



# ECS Southeast, LLP

Geotechnical Subsurface Data Report

Emergency Bridge Package 2020-1

SCDOT Project ID: P039639

York County, South Carolina

ECS Project Number 08:14113

March 24, 2020



**GEOTECHNICAL SUBSURFACE DATA REPORT**

Emergency Bridge Package 2020-1  
SCDOT Project ID: P039639  
York County, South Carolina

Prepared For:



Mr. Trapp Harris, P.E.  
955 Park Street  
Columbia, SC 29201

Prepared By:  
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Charlotte, NC 28217

ECS Project No:  
**08:14113**

Report Date:  
March 24, 2020



## ECS SOUTHEAST, LLP

Geotechnical • Construction Materials • Environmental • Facilities

"Setting the Standard for Service"

NC Registered Engineering Firm F-1078  
NC Registered Geologists Firm G-553  
SC Registered Engineering Firm 3239

March 24, 2020

Mr. Trapp Harris, P.E.  
Geotechnical Engineer  
South Carolina Department of Transportation  
955 Park Street  
Columbia, South Carolina 29201

ECS Project No. 08:14113

Reference: Geotechnical Subsurface Data Report  
**Emergency Bridge Package 2020-1**  
SCDOT Project ID: P039639  
York County, South Carolina

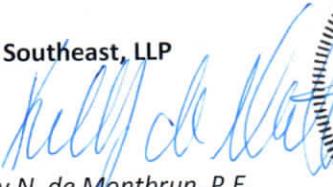
Dear Mr. Harris:

ECS Southeast, LLP (ECS) has completed the subsurface exploration and laboratory testing for the above referenced project. Our services were performed in general accordance with the scope provided in the SCDOT NTP dated February 28, 2019. This report presents our understanding of the geotechnical aspects of the project, along with the results of the field exploration and laboratory testing conducted.

It has been our pleasure to be of service to the South Carolina Department of Transportation (SCDOT) during this phase of this project. Should you have any questions concerning the information contained in this report, or if we can be of further assistance to you, please contact us.

Respectfully submitted,

ECS Southeast, LLP

  
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## **1.0 INTRODUCTION**

ECS is pleased to present this Geotechnical Subsurface Data Report for the S-46-816 Bridge over Mud Creek, as part of the Emergency Bridge Package 2020-1 project. The purpose of this report is to provide geotechnical information and laboratory testing results.

## **2.0 PROJECT LOCATION**

### **2.1 PROJECT LOCATION**

The project site is located along S-46-816 (Smith Ford Road) approximately 0.7 miles northwest of the intersection of Smith Ford Road and Huntington Road. The project site is approximately 3.2 miles west of the town of Hickory Grove in York County, South Carolina, as shown on the Site Vicinity Map in Appendix A.

### **2.2 PROJECT DESCRIPTION**

The S-46-816 (Smith Ford Road) bridge over Mud Creek is a currently in-service 2 lane bridge in York County, South Carolina. We understand plans are to demolish the existing bridge and replace with a new bridge.

## **3.0 SUBSURFACE EXPLORATION**

### **3.1 SOIL TEST BORINGS**

ECS completed a total of four (4) soil test borings (B-5, B-6, B-7, and B-8) at the subject bridge consisting of two (2) bridge end bent borings and two (2) bridge approach borings. The soil test borings were performed utilizing a CME 75 drill rig on March 10 through 13, 2019. Photographic documentation of the drill rig setup at each boring location is included in Appendix B. The borings were located in the field by an ECS representative at the approximate locations provided by the SCDOT. After completion, the test locations were obtained by a licensed surveyor. A Boring Location Diagram is included in Appendix A.

The soil test borings were drilled by a CME 75 drill rig using the rotary wash drilling method with a 6 inch bit. Standard Penetration Tests (SPTs) were generally conducted continuously within the top 10 feet and at 5-foot intervals thereafter until refusal was encountered. The SPT is used to provide an index for estimating soil strength and density. In conjunction with the penetration testing, split barrel soil samples were recovered for soil classification and laboratory testing at various intervals. The N-values presented in the boring logs are uncorrected, field N-values. Blow counts recorded at these intervals were produced from a standard penetration test hammer with an energy efficiency of 72.8%. The hammer calibration records are included in Appendix D.

An ECS Geotechnical Professional was on site and visually classified each sample during drilling. Samples from each split spoon were sealed in plastic bags and returned to the ECS office for laboratory testing. The boring logs are included in Appendix B. A summary of the borings is presented in Table 3.1.1.

**Table 3.1.1 Summary of Subsurface Exploration Boring Locations**

Boring ID	Boring Type	Northing (Int. ft.)	Easting (Int. ft.)	Ground Surface Elevation (ft.)	Water Table Depth (ft.)	Water Table Elevation (ft.)
B-5	SPT	1147460.25	1858716.40	445.0	17.3	427.7
B-6	SPT	1147559.13	1858703.52	445.1	19.8	425.3
B-7	SPT	1147714.04	1858684.04	444.9	16.8	428.1
B-8	SPT	1147769.63	1858676.98	443.9	19.6	424.3

### 3.2 ROCK CORING

Rock coring was performed within the soil test borings B-6 and B-7 located at the bridge end bents at the auger and spoon refusal depths. Boring B-6 was terminated in rock at a depth of approximately 80 feet below the existing ground surface. Boring B-7 encountered soil underlying rock cored in HQ-1, therefore, SPT sampling and drilling was resumed in Boring B-7 and the boring was terminated at drilling/spoon refusal at a depth of approximately 86 feet below the existing ground surface. A summary of the rock coring runs recovered from the Boring B-6 and B-7 is included in Table 3.2.1.

Rock coring was performed using a diamond-studded bit fastened to the end of a hollow double tube core barrel. A HQ core barrel was used to obtain rock cores 2½ inches in diameter. This device was rotated at high speed by the drill rig and the cuttings were brought to the surface by circulating water. Core samples of the materials penetrated were protected and retained in the swivel-mounted inner tube of the core barrel. Upon completion of each drill run, the core barrel was brought to the surface, removed and placed in core boxes, and returned to our laboratory for testing. An ECS Project Geologist was on site and visually classified each sample during coring. The rock coring results are presented on the boring logs and a Photo Log is included in Appendix B.

**Table 3.2.1 Summary of Rock Core Runs**

Boring ID	Run ID	Run Depth (ft)	Recovery (%)	Rock Quality Designation (%)	q <sub>u</sub> (psi)
B-6	HQ-1	65.0 – 70.0	78	57	9389.7
	HQ-2	70.0 – 75.0	100	90	7921.4
	HQ-3	75.0 – 80.0	100	100	3327.9
B-7	HQ-1	78.0 – 83.0	12	0	-

### 3.3 GROUNDWATER

Groundwater was measured between approximately 17.3 and 19.8 feet below the existing ground surface at around the 24-hr time interval within Borings B-5, B-6, B-7, and B-8. After a 24 hour measurement was obtained, the boring was backfilled and capped with bentonite. Groundwater elevations should be expected to vary depending on seasonal fluctuations in precipitation, surface water absorption characteristics, and other factors not readily apparent at the time of our exploration, and may be higher or lower than inferred from the recent test boring data.

### **3.4 LABORATORY TESTING**

The laboratory testing frequency was determined by the SCDOT and laboratory testing was performed in accordance with the respective ASTM and AASHTO standards. Individual laboratory test results and a Laboratory Testing Summary are presented in Appendix C. Table 3.3.1 provides a quantitative overview of the testing performed:

**Table 3.4.1 Laboratory Test Quantities**

Test Type	Quantity
Atterberg Limits	5
Sieve Analysis	8
Moisture Content	16
Hydrometer	8
Corrosion Testing	1
Unconfined Compressive Strength (Rock)	3

### **4.0 CLOSING**

Due to the prevailing geology, changes in the subsurface conditions can occur over relatively short distances that have not been disclosed by the results of the borings evaluated. Consequently, there may be undisclosed subsurface conditions that require special treatment or additional preparation once these conditions are revealed during construction. The assessment of site environmental conditions for the presence of pollutants in the soil, rock, and groundwater of the site was beyond the scope of services for this project.

## **APPENDIX A – Drawings & Reports**

Site Vicinity Map  
Boring Location Diagram



Mud  
sland

Smith Ford Rd

Huntington Rd

Mud Creek

0 600 1,200  
Feet



**Site Vicinity Map  
EMERGENCY BRIDGE PACKAGE 2020-1**

**S-816 BRIDGE OVER MUD CREEK, YORK COUNTY, SC**

**SCDOT**

ENGINEER  
MFP

SCALE  
1 " = 600 '

PROJECT NO.  
08:14113

SHEET  
1 OF 1

DATE  
3/19/2020



Boring ID	Latitude	Longitude
B-5	34.98603900	-81.47162200
B-6	34.98630800	-81.47166700
B-7	34.98673600	-81.47173600
B-8	34.98688900	-81.47175800

Source: Google Earth (2020)  
Scale: Not to Scale

Note: Borings B-1 through B-4 were performed as part of the Emergency Bridge Package 2020-1: S-174 (Timms Mills Road) Bridge over Six & Twenty Creek, Anderson County, SC.

#### LEGEND



Boring Location



Boring Number



**Boring Location Plan**  
Emergency Bridge Package 2020-1  
S-816 (Smith Ford Road) Bridge over Mud Creek  
York County, South Carolina  
ECS Project No.: 08:14113

## **APPENDIX B – Field Operations**

Reference Notes for Boring Logs  
Boring Logs (Borings B-5, B-6, B-7, B-8)  
Rock Core Photo Logs (Borings B-6 and B-7)  
Photo Log



ECS REFERENCE NOTES FOR SCDOT BORING LOGS - SOIL DESCRIPTIONS

The descriptions noted on the boring logs generally conform to the SCDOT GDM format.

## **DESCRIPTION FORMAT**

GEOLOGIC ORIGIN\* - Relative density/consistency, moisture condition, color, angularity, hcl reaction, cementation, secondary component (adj.), particle-size range, PRIMARY COMPONENT (noun), USCS, AASHTO, contains, other

\*Such as FILL, ALLUVIUM, RESIDUUM, PARTIALLY WEATHERED ROCK, etc. In Coastal Plain areas, name of formation may be used. Geologic origin is cited only for first sample of geologic type.

## **RELATIVE DENSITY/CONSISTENCY**

## SANDS AND GRAVELS

## SILTS AND CLAYS

SPT	Density description	SPT	Consistency Description
0 - 4	Very loose	0 - 2	Very Soft
5 - 10	Loose	3 - 4	Soft
11 - 30	Medium Dense	5 - 8	Firm
31 - 50	Dense	9 - 15	Stiff
> 50	Very Dense	16 - 30	Very Stiff
		>30	Hard

## MOISTURE CONDITION

Dry	Dusty, dry to touch
Moist	Moisture can be felt but not visible
Wet	Water is visible

## COLOR

Basic colors (when moist) using the Munsell color chart

Mottled, indicates splotches of various colors

Variegated, indicates thin layers of various colors

ANGULARITY

Angular	Particles have sharp edges and relatively plane sides with unpolished surfaces
Subangular	Particles are similar to angular description but have rounded edges
Subrounded	Particles have nearly plane sides but have well-rounded corners and edges
Rounded	Particles have smoothly curved sides and no edges

## HCL REACTION

None Reactive	No visible reaction
Weakly Reactive	Some reaction, with bubbles forming slowly
Strongly Reactive	Violent reaction, with bubbles forming immediately

## **CEMENTATION**

Weakly Cemented	Crumbles or breaks with handling or little finger pressure
Moderately Cemented	Crumbles or breaks with considerable finger pressure
Strongly Cemented	Will not crumble or break with finger pressure

## PARTICLE-SIZE RANGE

SIZE:	12"	3"	¾"	#4	#10	#40	#200	
DESCRIPTION:	BOULDER	COBBLE	GRAVEL		SAND			SILT to CLAY
RANGE:		Coarse golf ball	Fine marble	Coarse pea	Medium sugar	Fine beach sand		
EXAMPLE:	basketball	softball						flour



#### **USCS SOIL DESIGNATION**

USCS classification per ASTM D 2487 and D 2488

#### **AASHTO SOIL DESIGNATION**

AASHTO classification per AASHTO M 145 and ASTM D 3282

#### **CONTAINS**

Contains is used to describe non-ASTM components such as roots, construction debris, asphalt concrete, etc. "contains slight" is used for occasional particles, "contains" is used for about 10% to 30% particles, "contains significant" is used for > 30% particles



## ECS REFERENCE NOTES FOR SCDOT BORING LOGS - ROCK DESCRIPTIONS

The descriptions noted on the boring logs generally conform to the SCDOT GDM format.

### DESCRIPTION FORMAT

Rock origin, TYPE, color, texture, grain size and shape, weathering / alteration, strength, hardness, strike and dip, discontinuity type, discontinuity width, amount of infilling, type of infilling, surface shape of joint, discontinuity spacing, roughness of surface, other

Descriptions are typically provided for each run. When portions of an individual run are notably different, the run may be subdivided into sub-runs with appropriate descriptions provided.

### ROCK ORIGIN AND TYPE

Sedimentary: Breccia, sandstone, siltstone, mudstone, shale, coal, conglomerate, limestone, chert, dolomite, etc.  
Metamorphic: Schist, phyllite, gneiss, marble, metaquartzite, slate, amphibolite, hornfels, serpentine, metatuff, etc.  
Igneous: Granite, syenite, diorite, gabbro, peridotite, diabase, basalt, pegmatite, etc.

### COLOR

Basic colors (when moist) using the Munsell color chart

Mottled, indicates splotches of various colors

Variegated, indicates thin layers of various colors

### TEXTURE

Very Thickly Bedded	> 1.0 m
Thickly Bedded	0.5 to 1.0 m
Thinly Bedded	50 to 500 mm
Very Thinly Bedded	10 to 50 mm
Laminated	2.5 to 10 mm
Thinly Laminated	< 2.5 mm

### GRAIN SIZE AND SHAPE

#### Size

Very coarse grained	> 4.75	Grain sizes greater than popcorn kernels
Coarse grained	2.00 – 4.75	Individual grains easy to distinguish by eye
Medium grained	0.425 – 2.00	Individual grains distinguished by eye
Fine grained	0.075 – 0.425	Individual grains distinguished with difficulty
Very fine grained	< 0.075	Individual grains cannot be distinguished by unaided eye

#### Shape

Angular	Shows little wear; edges and corners are sharp
Subangular	Shows definite effects of wear; edges and corners are slightly rounded off
Subrounded	Shows considerable wear; edges and corners are rounded to smooth curves
Rounded	Shows extreme wear; edges and corners are smoother to broad curves
Well-rounded	Completely worn; edges and corners are not present

### WEATHERING / ALTERATION

Residual Soil	Original minerals of rock have been entirely decomposed to secondary minerals, and original rock fabric is not apparent; material can be easily broken by hand
Completely Weather / Altered	Original minerals of rock have been almost entirely decomposed to secondary minerals, although the original fabric may be intact; material can be granulated by hand
Highly Weathered / Altered	More than half of the rock is decomposed; rock is weakened so that a minimum 1-7/8 inch diameter sample can be easily broken readily by hand across rock fabric
Moderately Weathered / Altered	Rock is discolored and noticeably weakened, but less than half is decomposed; a minimum 1-7/8 inch diameter sample cannot be broken readily by hand across rock fabric



Slightly Weathered / Altered  
Fresh

Rock is slightly discolored, but not noticeably lower in strength than fresh rock  
Rock shows no discoloration, loss of strength, or other effect of weathering / alteration

## STRENGTH

Extremely Weak Rock  
Very Weak Rock  
Weak Rock  
Medium Strong Rock  
Strong Rock  
Very Strong Rock  
Extremely Strong Rock

Can be indented by thumbnail  
Can be peeled by pocket knife  
Can be peeled with difficulty by pocket knife  
Can be indented 3/16 inch with sharp end of pick  
Requires one hammer blow to fracture  
Requires many hammer blows to fracture  
Can only be chipped with hammer blows

## HARDNESS

Very Soft  
Soft  
Moderately Hard  
Hard  
Very Hard

Can be deformed by hand  
Can be scratched with a fingernail  
Can be scratched easily by a knife  
Can be scratched with difficulty by a knife  
Can not be scratched with a knife

## STRIKE AND DIP

Dip of fracture surface measured relative to horizontal with bearing and direction.

## DISCONTINUITY TYPE

F - Fault  
J - Joint  
Sh - Shear  
Fo - Foliation  
V - Vein  
B - Bedding

## DISCONTINUITY WIDTH (MM)

W - Wide (12.5 – 50)  
MW - Moderately Wide (2.5 – 12.5)  
N - Narrow (1.25 – 2.5)  
VN - Very Narrow (<1.25)  
T - Tight (0)

## AMOUNT OF INFILLING

Su - Surface Stain  
Sp - Spotty  
Pa - Partially Filled  
Fi - Filled  
No - None

## TYPE OF INFILLING

Cl - Clay  
Ca - Calcite  
Ch - Chloride  
Fe - Iron Oxide  
Gy - Gypsum/Talc  
H - Healed  
No - None  
Py - Pyrite  
Qz - Quartz  
Sd - Sand



#### SURFACE SHAPE OF JOINT

- Wa - Wavy
- Pl - Planar
- St - Stepped
- Ir - Irregular

#### DISCONTINUITY SPACING (FT)

- Ew - Extremely Wide (>65)
- W - Wide (22 – 65)
- M - Moderate (7.5 – 22)
- C - Close (2 – 7.5)
- VC - Very Close (<2)

#### ROUGHNESS OF SURFACE

- Slk - Slickensided (surface has smooth, glassy finish with visual evidence of striations)
- S - Smooth (surface appears smooth and feels so to the touch)
- SR - Slightly Rough (asperities on the discontinuity surfaces are distinguishable and can be felt)
- R - Rough (some ridges and side-angle steps are evident; asperities are clearly visible, and discontinuity surface feels very abrasive)
- VR - Very Rough (near-vertical steps and ridges occur on the discontinuity surface)

#### REC and RQD

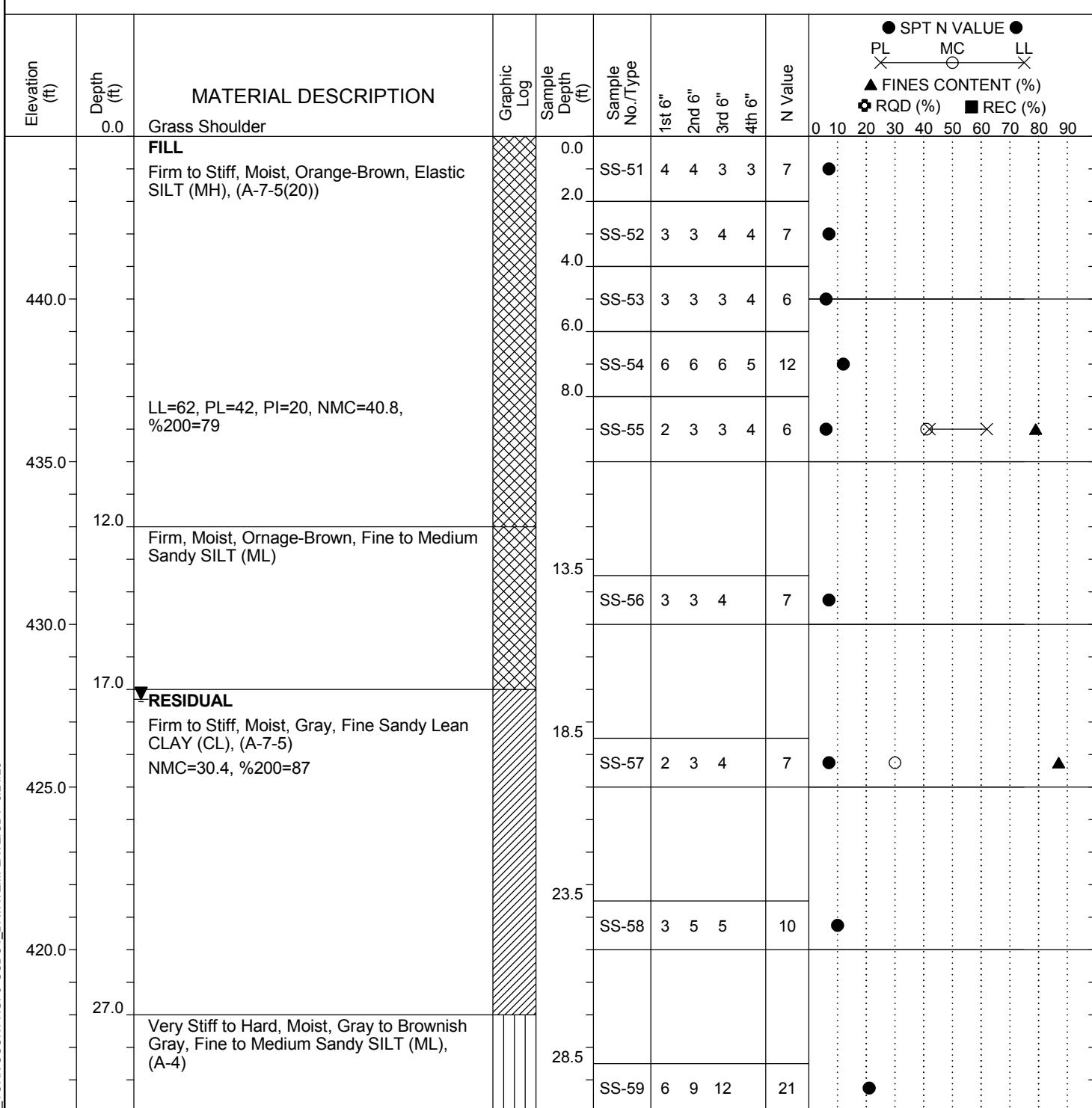
Rock Recovery, expressed as REC, is the percentage of the total length or rock recovered divided by the length of the core run. The Rock Quality Designation, expressed as RQD is the percentage of the total length of the rock pieces 4 inches in length or greater divided the length of the rock core run. Mechanical breaks are neglected in determining the RQD.

# SOIL CLASSIFICATION CHART

MAJOR DIVISIONS			SYMBOLS		TYPICAL DESCRIPTIONS	
			GRAPH	LETTER		
COARSE GRAINED SOILS  MORE THAN 50% OF MATERIAL IS LARGER THAN NO. 200 SIEVE SIZE	GRAVEL AND GRAVELLY SOILS  MORE THAN 50% OF COARSE FRACTION RETAINED ON NO. 4 SIEVE	CLEAN GRAVELS (LITTLE OR NO FINES)		GW	WELL-GRADED GRAVELS, GRAVEL - SAND MIXTURES, LITTLE OR NO FINES	
		GRAVELS WITH FINES (APPRECIABLE AMOUNT OF FINES)		GP	Poorly-graded gravels, gravel - sand mixtures, little or no fines	
				GM	SILTY GRAVELS, GRAVEL - SAND - SILT MIXTURES	
	SAND AND SANDY SOILS  MORE THAN 50% OF COARSE FRACTION PASSING ON NO. 4 SIEVE	CLEAN SANDS (LITTLE OR NO FINES)		GC	CLAYEY GRAVELS, GRAVEL - SAND - CLAY MIXTURES	
				SW	WELL-GRADED SANDS, GRAVELLY SANDS, LITTLE OR NO FINES	
		SANDS WITH FINES (APPRECIABLE AMOUNT OF FINES)		SP	Poorly-graded sands, gravelly sand, little or no fines	
FINE GRAINED SOILS  MORE THAN 50% OF MATERIAL IS SMALLER THAN NO. 200 SIEVE SIZE	SILTS AND CLAYS  LIQUID LIMIT LESS THAN 50			SM	SILTY SANDS, SAND - SILT MIXTURES	
				SC	CLAYEY SANDS, SAND - CLAY MIXTURES	
				ML	INORGANIC SILTS AND VERY FINE SANDS, ROCK FLOUR, SILTY OR CLAYEY FINE SANDS OR CLAYEY SILTS WITH SLIGHT PLASTICITY	
	SILTS AND CLAYS  LIQUID LIMIT GREATER THAN 50			CL	INORGANIC CLAYS OF LOW TO MEDIUM PLASTICITY, GRAVELLY CLAYS, SANDY CLAYS, SILTY CLAYS, LEAN CLAYS	
				OL	ORGANIC SILTS AND ORGANIC SILTY CLAYS OF LOW PLASTICITY	
				MH	INORGANIC SILTS, MICACEOUS OR DIATOMACEOUS FINE SAND OR SILTY SOILS	
				CH	INORGANIC CLAYS OF HIGH PLASTICITY	
				OH	ORGANIC CLAYS OF MEDIUM TO HIGH PLASTICITY, ORGANIC SILTS	
HIGHLY ORGANIC SOILS				PT	PEAT, HUMUS, SWAMP SOILS WITH HIGH ORGANIC CONTENTS	

NOTE: DUAL SYMBOLS ARE USED TO INDICATE BORDERLINE SOIL CLASSIFICATIONS

<b>Project ID:</b>	P039639			<b>County:</b>	York		<b>Boring No.:</b>	B-5		
<b>Site Description:</b>	Emergency Bridge Package 2020-1					<b>Route:</b>	S-46-816			
<b>Eng./Geo.:</b>	J. Garrick		<b>Boring Location:</b>			<b>Offset:</b>				
Elev.:	445.0 ft	<b>Latitude:</b>	34.986039	<b>Longitude:</b>	-81.471622	<b>Date Started:</b>	3/11/2020			
<b>Total Depth:</b>	49.8 ft	<b>Soil Depth:</b>	49.8 ft	<b>Core Depth:</b>	N/A ft	<b>Date Completed:</b>	3/11/2020			
<b>Bore Hole Diameter (in):</b>		6	<b>Sampler Configuration</b>		<b>Liner Required:</b>	Y <input checked="" type="checkbox"/>	<b>Liner Used:</b>	Y <input type="checkbox"/>		
<b>Drill Machine:</b>		CME 75	<b>Drill Method:</b>	Wash Rotary	<b>Hammer Type:</b>	Automatic	<b>Energy Ratio:</b>	73%		
<b>Core Size:</b>	N/A		<b>Driller:</b>	Betts		<b>Groundwater:</b>	TOB	N/A	24HR	17.3 ft



## LEGEND

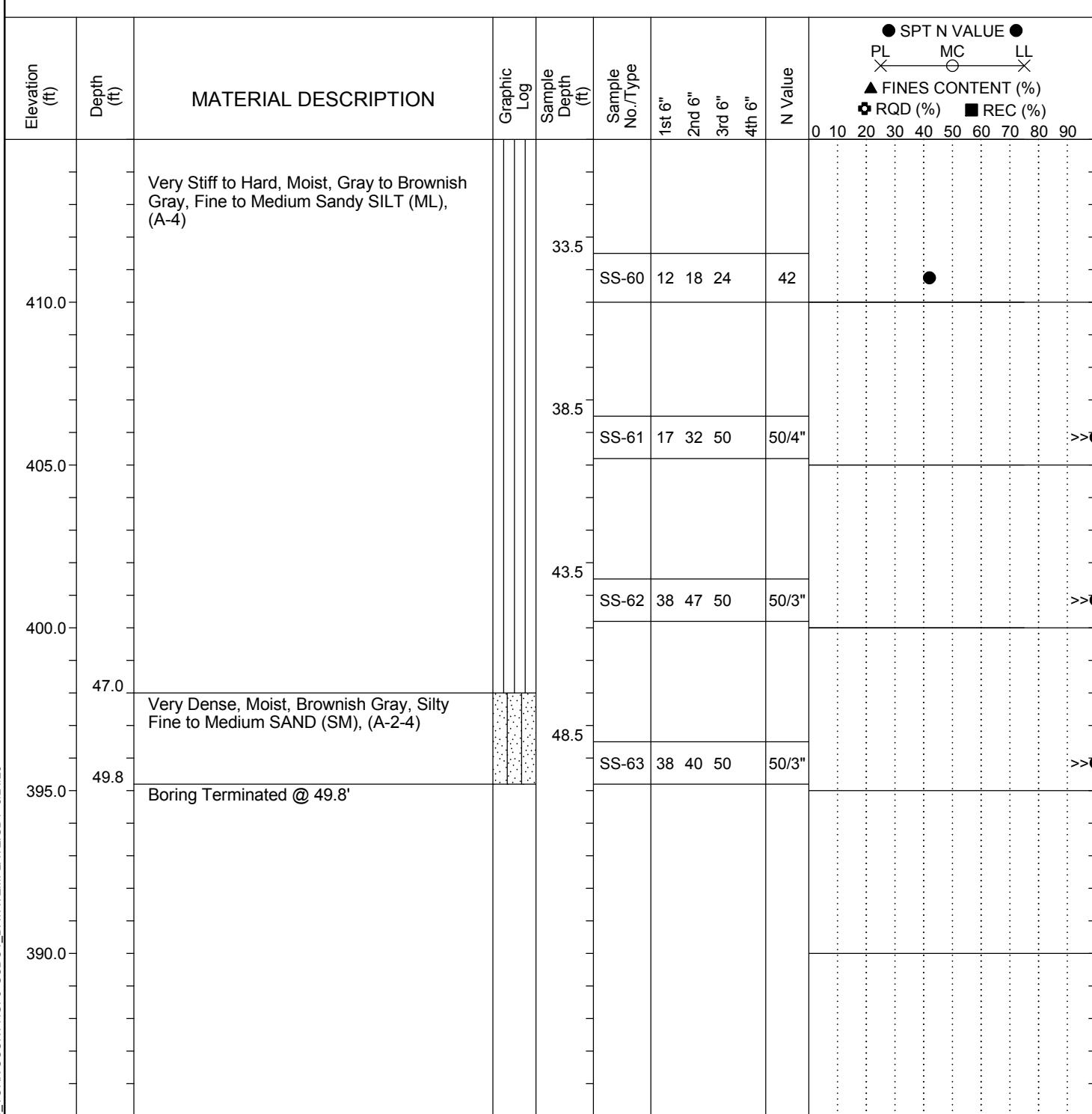
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SAMPLER TYPE		DRILLING METHOD	
SS - Split Spoon	NQ - Rock Core, 1-7/8"	HSA - Hollow Stem Auger	RW - Rotary Wash
UD - Undisturbed Sample	CU - Cuttings	CFA - Continuous Flight Augers	RC - Rock Core
AWG - Rock Core, 1-1/8"	CT - Continuous Tube	DC - Driving Casing	



## Soil Test Log

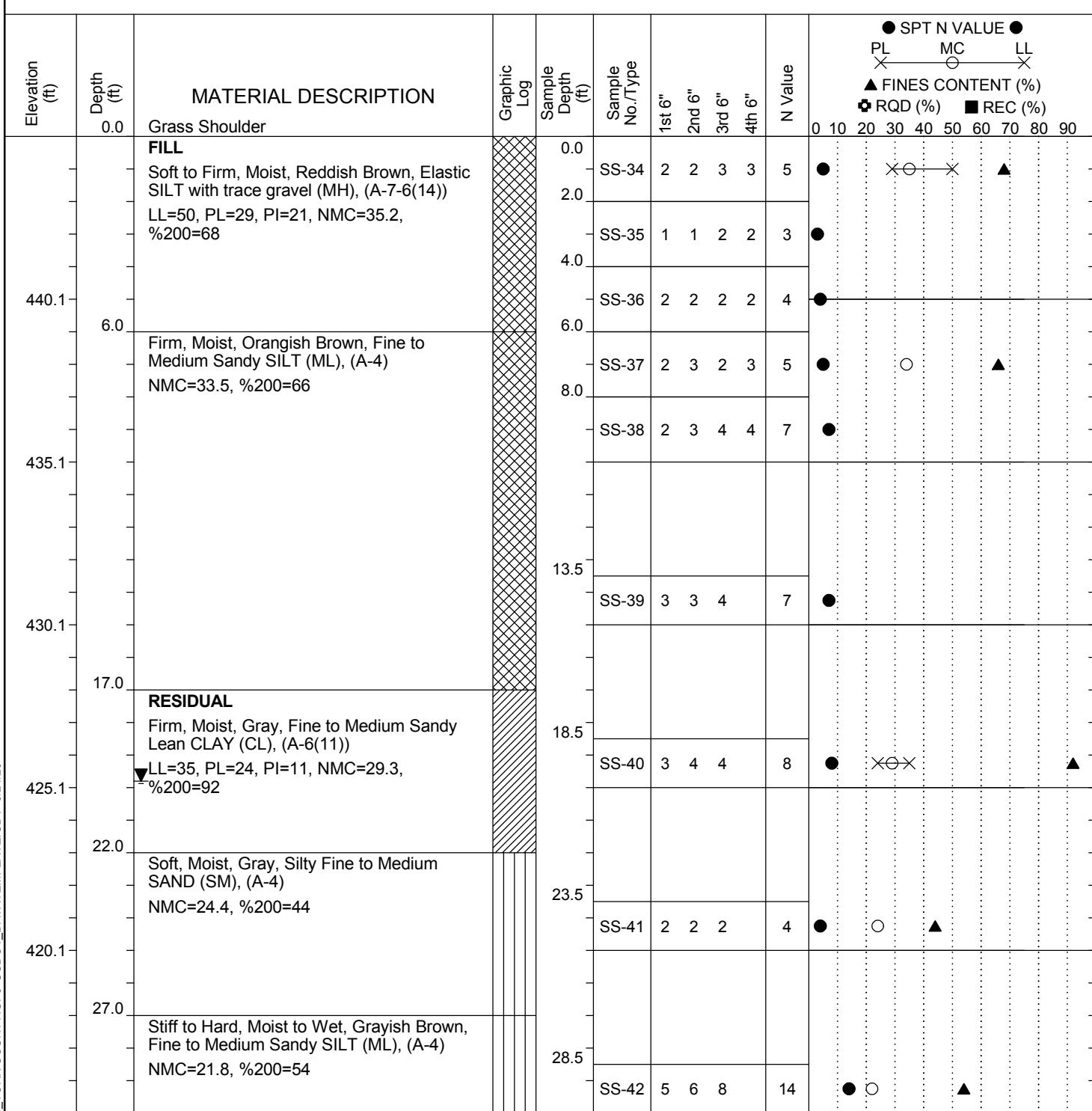
Project ID:	P039639			County:	York		Boring No.:	B-5		
Site Description:	Emergency Bridge Package 2020-1				Route:		S-46-816			
Eng./Geo.:	J. Garrick		Boring Location:			Offset:				
Elev.:	445.0 ft		Latitude:	34.986039		Longitude:	-81.471622			
Total Depth:	49.8 ft		Soil Depth:	49.8 ft		Core Depth:	N/A ft			
Bore Hole Diameter (in):	6		Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)		
Drill Machine:	CME 75		Drill Method:	Wash Rotary		Hammer Type:	Automatic	Energy Ratio:	73%	
Core Size:	N/A		Driller:	Betts		Groundwater:	TOB	N/A	24HR	17.3 ft



## LEGEND

SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

Project ID:	P039639			County:	York		Boring No.:	B-6
Site Description:	Emergency Bridge Package 2020-1						Route:	S-46-816
Eng./Geo.:	J. Garrick		Boring Location:			Offset:		
Elev.:	445.1 ft		Latitude:	34.986308		Longitude:	-81.471667	
Total Depth:	80 ft		Soil Depth:	65 ft		Core Depth:	80 ft	
Bore Hole Diameter (in):	6		Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)
Drill Machine:	CME 75		Drill Method:	Wash Rotary		Hammer Type:	Automatic	
Core Size:	HQ		Driller:	Betts		Groundwater:	TOB	N/A
							24HR	19.8 ft

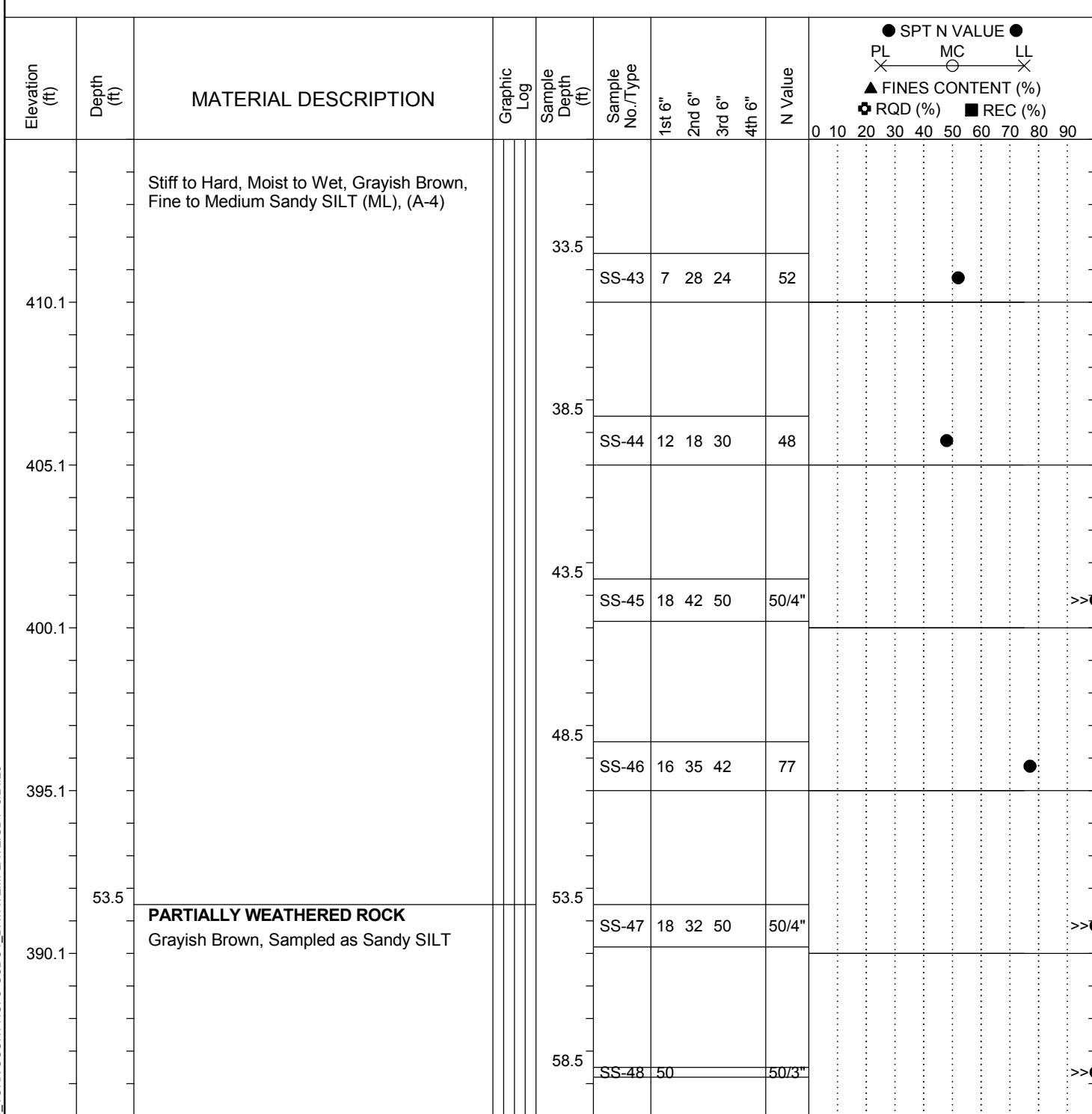


## LEGEND

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SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	NQ - Rock Core, 1-7/8"	CU - Cuttings	HSA - Hollow Stem Auger	RW - Rotary Wash	CFA - Continuous Flight Augers	DC - Driving Casing	RC - Rock Core
UD - Undisturbed Sample							
AWG - Rock Core, 1-1/8"		CT - Continuous Tube					

Project ID:	P039639			County:	York		Boring No.:	B-6
Site Description:	Emergency Bridge Package 2020-1				Route:		S-46-816	
Eng./Geo.:	J. Garrick		Boring Location:			Offset:		
Elev.:	445.1 ft		Latitude:	34.986308		Longitude:	-81.471667	
Total Depth:	80 ft		Soil Depth:	65 ft		Core Depth:	80 ft	
Bore Hole Diameter (in):	6		Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)
Drill Machine:	CME 75		Drill Method:	Wash Rotary		Hammer Type:	Automatic	Energy Ratio: 73%
Core Size:	HQ		Driller:	Betts		Groundwater:	TOB	N/A
							24HR	19.8 ft



LEGEND

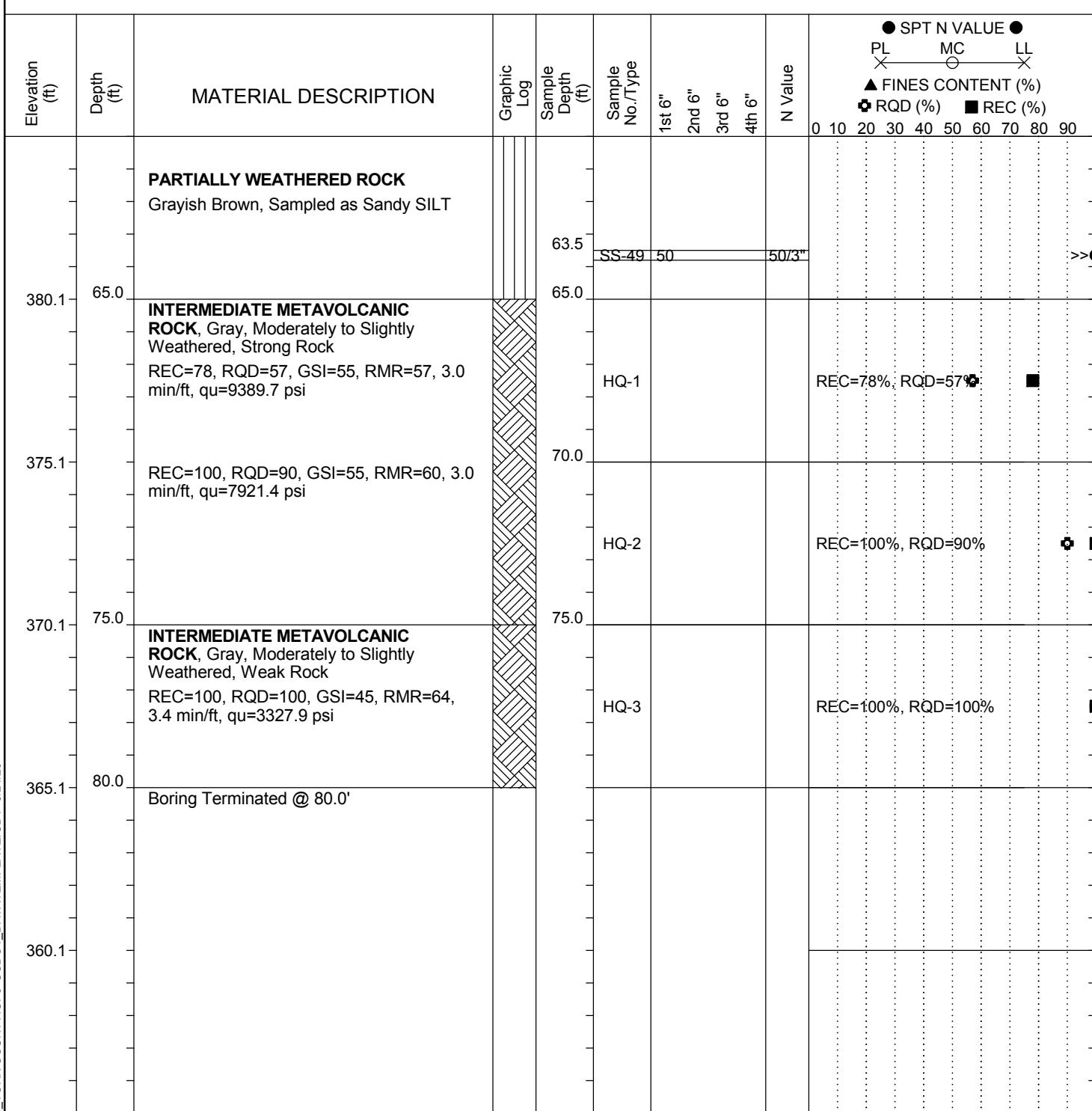
Continued Next Page

SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

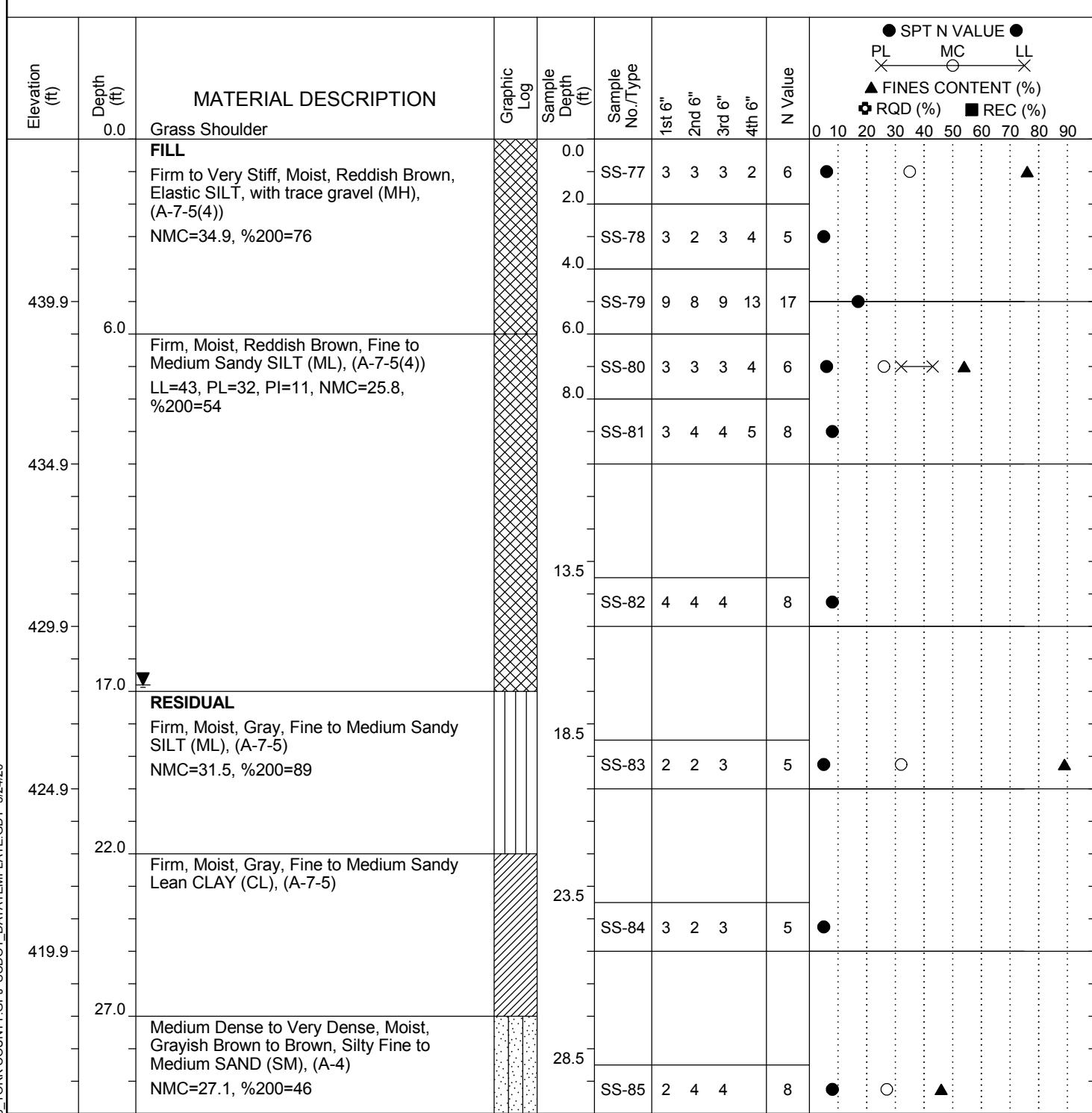


## Soil Test Log

Project ID:	P039639			County:	York		Boring No.:	B-6		
Site Description:	Emergency Bridge Package 2020-1				Route:		S-46-816			
Eng./Geo.:	J. Garrick		Boring Location:			Offset:				
Elev.:	445.1 ft		Latitude:	34.986308		Longitude:	-81.471667			
Total Depth:	80 ft		Soil Depth:	65 ft		Core Depth:	80 ft			
Bore Hole Diameter (in):	6		Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)		
Drill Machine:	CME 75		Drill Method:	Wash Rotary		Hammer Type:	Automatic	Energy Ratio:	73%	
Core Size:	HQ		Driller:	Betts		Groundwater:	TOB	N/A	24HR	19.8 ft



Project ID:	P039639	County:	York	Boring No.:	B-7
Site Description:	Emergency Bridge Package 2020-1			Route:	S-46-816
Eng./Geo.:	J. Garrick	Boring Location:		Offset:	
Elev.:	444.9 ft	Latitude:	34.986736	Longitude:	-81.471736
Total Depth:	86 ft	Soil Depth:	86 ft	Core Depth:	N/A ft
Bore Hole Diameter (in):	6	Sampler Configuration		Liner Required:	Y (N)
Drill Machine:	CME 75	Drill Method:	Wash Rotary	Hammer Type:	Automatic
Core Size:	N/A	Driller:	Betts	Groundwater:	TOB
				N/A	24HR
					16.8 ft

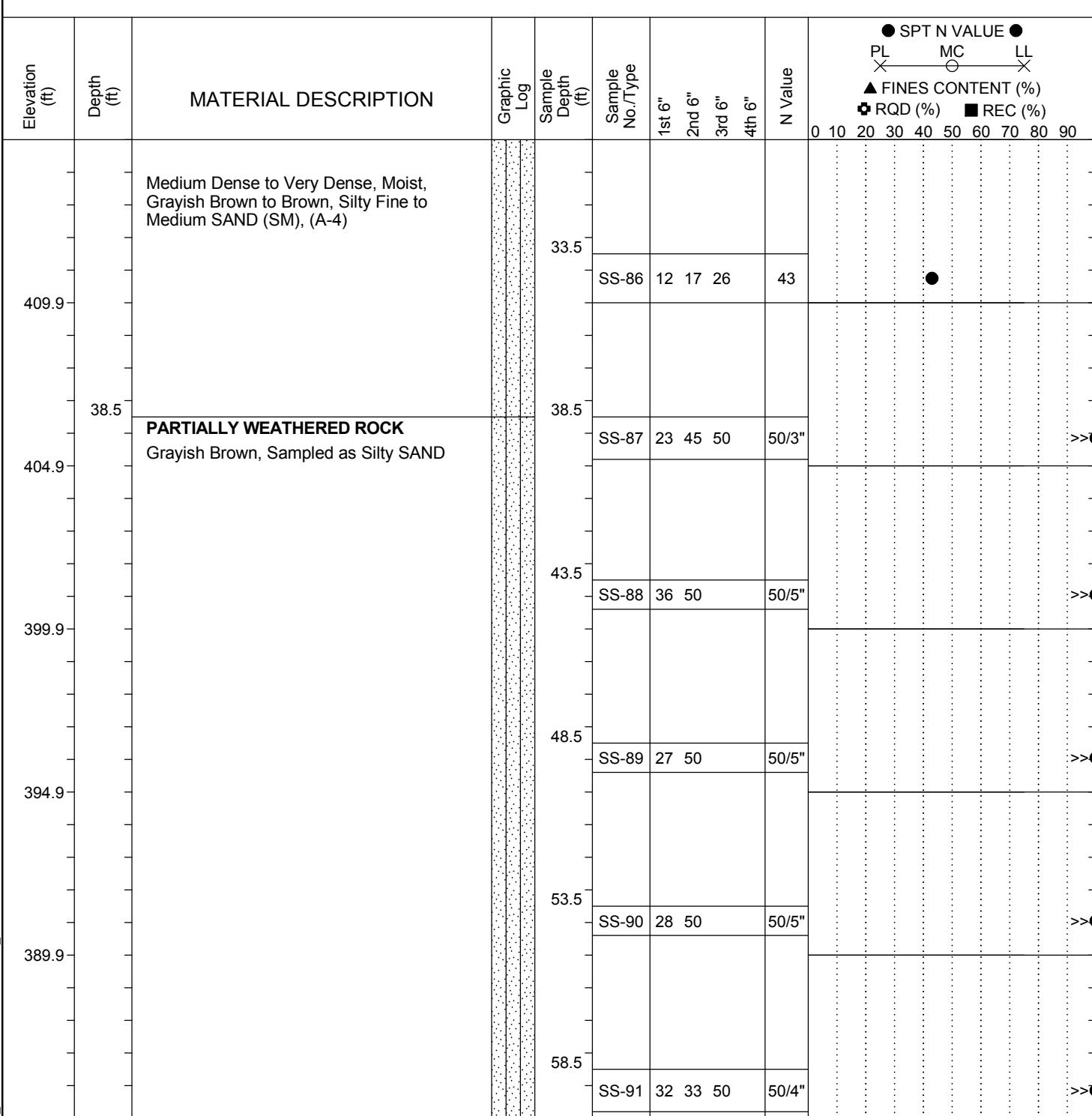


## LEGEND

Continued Next Page

SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	NQ - Rock Core, 1-7/8"			HSA - Hollow Stem Auger	RW - Rotary Wash		
UD - Undisturbed Sample	CU - Cuttings			CFA - Continuous Flight Augers	RC - Rock Core		
AWG - Rock Core, 1-1/8"	CT - Continuous Tube			DC - Driving Casing			

Project ID:	P039639			County:	York		Boring No.:	B-7
Site Description:	Emergency Bridge Package 2020-1						Route:	S-46-816
Eng./Geo.:	J. Garrick		Boring Location:			Offset:		
Elev.:	444.9 ft		Latitude:	34.986736		Longitude:	-81.471736	
Total Depth:	86 ft		Soil Depth:	86 ft		Core Depth:	N/A ft	
Bore Hole Diameter (in):	6		Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)
Drill Machine:	CME 75		Drill Method:	Wash Rotary		Hammer Type:	Automatic	Energy Ratio: 73%
Core Size:	N/A		Driller:	Betts		Groundwater:	TOB	N/A
							24HR	16.8 ft

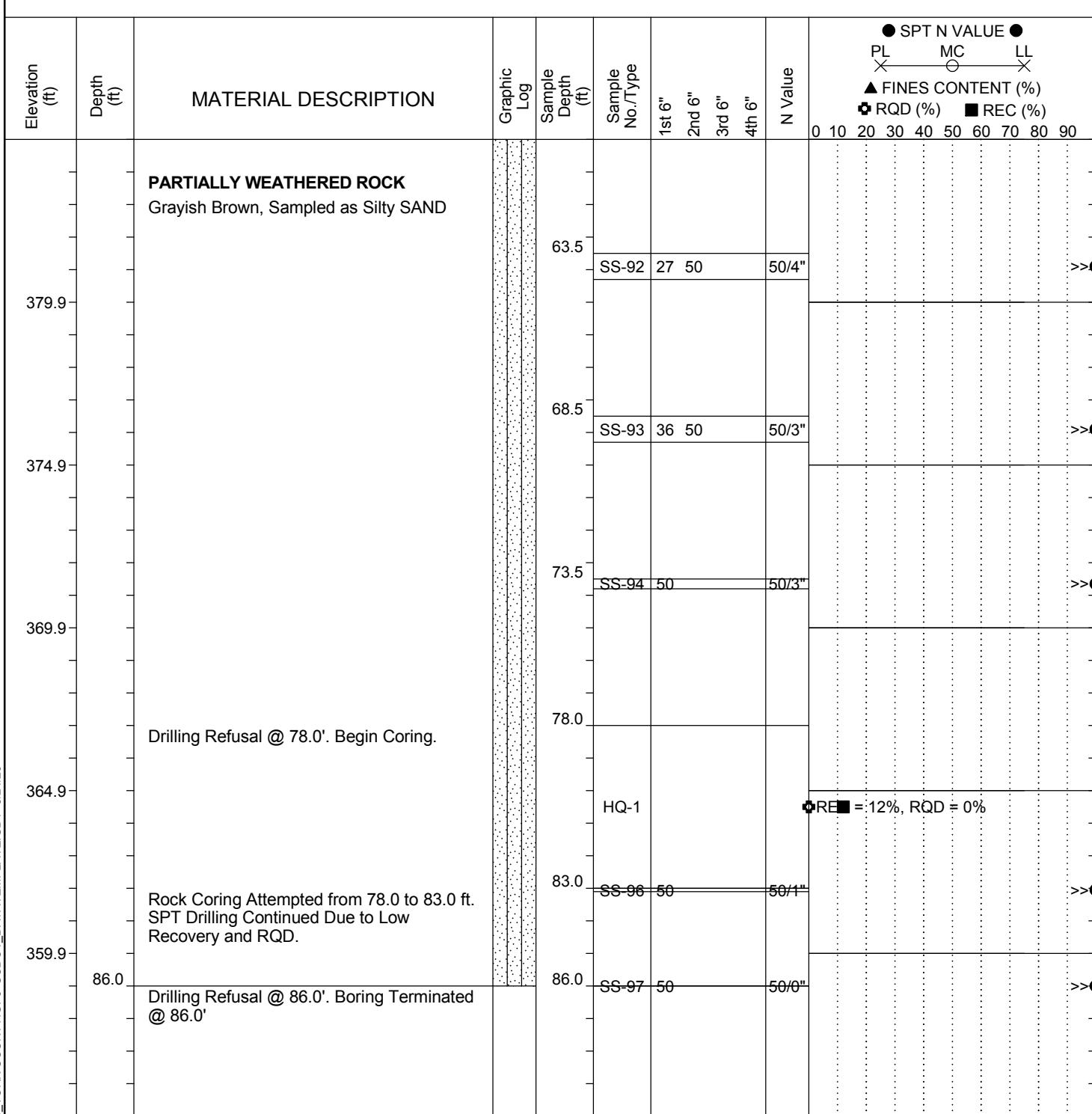


## LEGEND

Continued Next Page

SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		

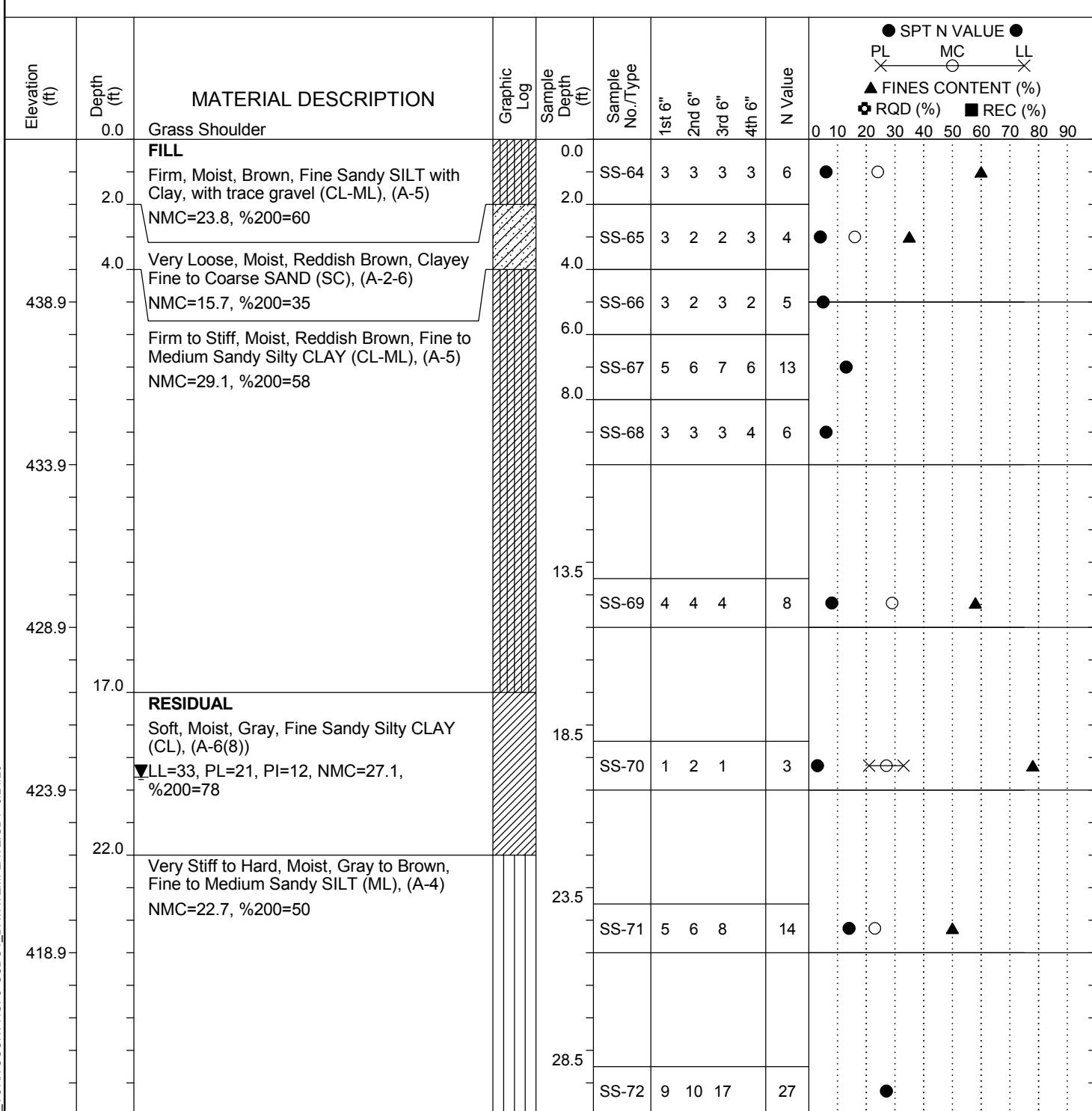
<b>Project ID:</b>	P039639			<b>County:</b>	York		<b>Boring No.:</b>	B-7		
<b>Site Description:</b>	Emergency Bridge Package 2020-1					<b>Route:</b>	S-46-816			
<b>Eng./Geo.:</b>	J. Garrick		<b>Boring Location:</b>			<b>Offset:</b>				
<b>Elev.:</b>	444.9 ft		<b>Latitude:</b>	34.986736		<b>Longitude:</b>	-81.471736			
<b>Total Depth:</b>	86 ft		<b>Soil Depth:</b>	86 ft		<b>Core Depth:</b>	N/A ft			
<b>Bore Hole Diameter (in):</b>	6		<b>Sampler Configuration</b>			<b>Liner Required:</b>	Y <input checked="" type="checkbox"/>	<b>Liner Used:</b> Y <input type="checkbox"/>		
<b>Drill Machine:</b>	CME 75		<b>Drill Method:</b>	Wash Rotary		<b>Hammer Type:</b>	Automatic		<b>Energy Ratio:</b> 73%	
<b>Core Size:</b>	N/A		<b>Driller:</b>	Betts		<b>Groundwater:</b>	TOB	N/A	24HR	16.8 ft



## LEGEND

SAMPLER TYPE		DRILLING METHOD	
SS - Split Spoon	NQ - Rock Core, 1-7/8"	HSA - Hollow Stem Auger	RW - Rotary Wash
UD - Undisturbed Sample	CU - Cuttings	CFA - Continuous Flight Augers	RC - Rock Core
AWG - Rock Core, 1-1/8"	CT - Continuous Tube	DC - Driving Casing	

Project ID:	P039639	County:	York	Boring No.:	B-8
Site Description:	Emergency Bridge Package 2020-1			Route:	S-46-816
Eng./Geo.:	J. Garrick	Boring Location:		Offset:	
Elev.:	443.9 ft	Latitude:	34.986889	Longitude:	-81.471758
Total Depth:	49.2 ft	Soil Depth:	49.2 ft	Core Depth:	N/A ft
Bore Hole Diameter (in):	6	Sampler Configuration		Liner Required:	Y (N)
Drill Machine:	CME 75	Drill Method:	Wash Rotary	Hammer Type:	Automatic
Core Size:	N/A	Driller:	Betts	Groundwater:	TOB N/A
					24HR 19.6 ft



## LEGEND

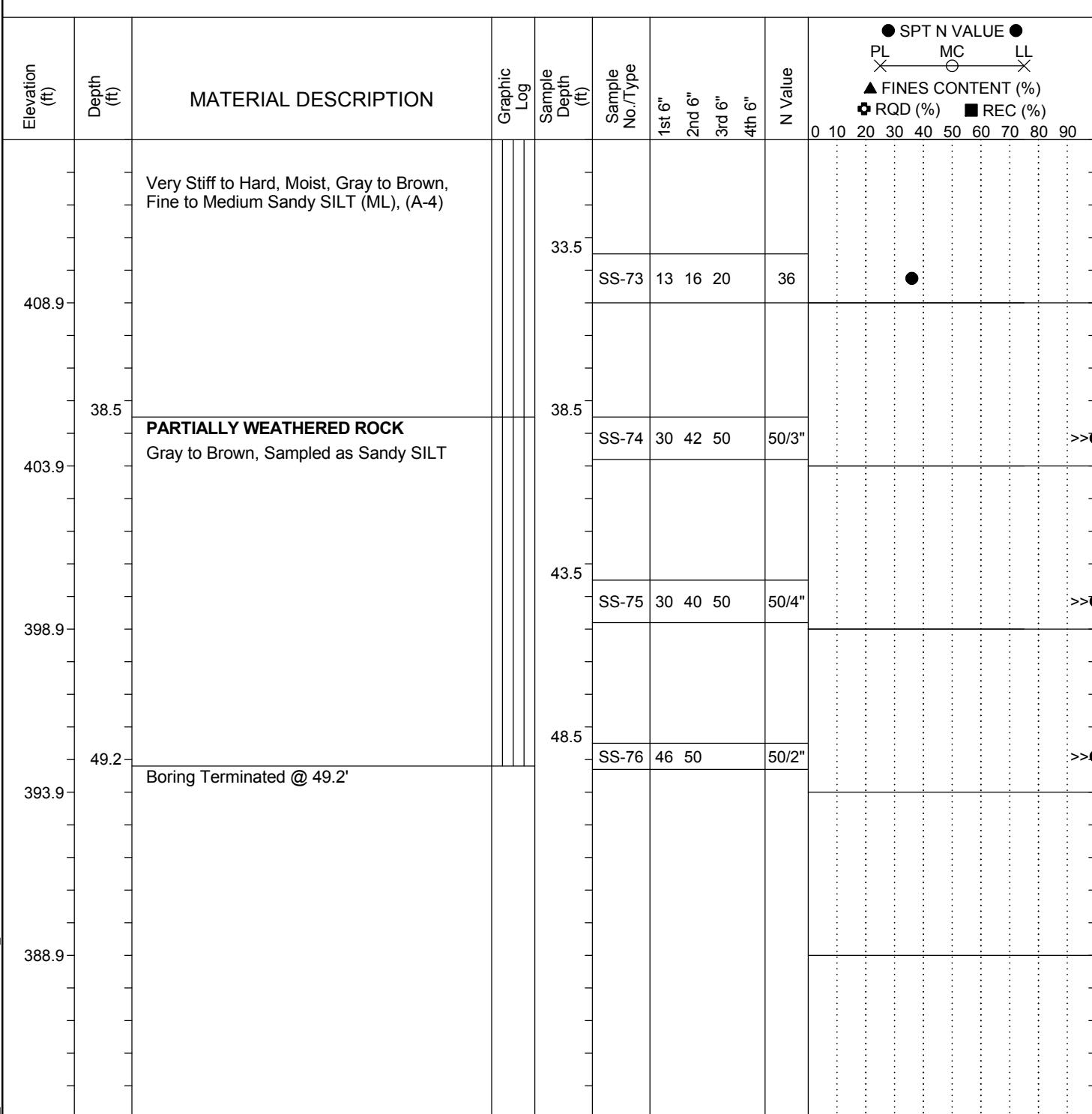
Continued Next Page

SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		



## Soil Test Log

Project ID:	P039639			County:	York		Boring No.:	B-8		
Site Description:	Emergency Bridge Package 2020-1						Route:	S-46-816		
Eng./Geo.:	J. Garrick		Boring Location:			Offset:				
Elev.:	443.9 ft		Latitude:	34.986889		Longitude:	-81.471758			
Total Depth:	49.2 ft		Soil Depth:	49.2 ft		Core Depth:	N/A ft			
Bore Hole Diameter (in):	6		Sampler Configuration		Liner Required:	Y (N)	Liner Used:	Y (N)		
Drill Machine:	CME 75		Drill Method:	Wash Rotary		Hammer Type:	Automatic	Energy Ratio:	73%	
Core Size:	N/A		Driller:	Betts		Groundwater:	TOB	N/A	24HR	19.6 ft



SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	NQ - Rock Core, 1-7/8"		HSA - Hollow Stem Auger	RW - Rotary Wash	
UD - Undisturbed Sample	CU - Cuttings		CFA - Continuous Flight Augers	RC - Rock Core	
AWG - Rock Core, 1-1/8"	CT - Continuous Tube		DC - Driving Casing		



ECS Southeast, LLP  
1812 Center Park Drive, Ste D  
Charlotte, NC 28217  
Phone: 704-525-5152

## ROCK CORE PHOTO LOG

Boring B-6

Project Name: 2020-1 SCDOT Emergency Bridge Package  
Bridge Replacement over Mud Creek on Smith Ford Road

Project Number:  
08:14113

Project Location: York County, South Carolina

Date: 3/18/2020

Begin HQ-1  
65.0 ft

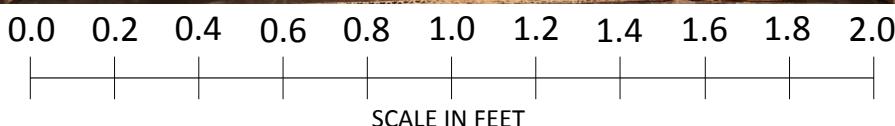


End HQ-1  
70.0 ft

Begin HQ-2  
70.0 ft



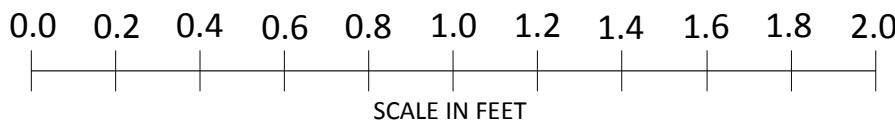
End HQ-2  
75.0 ft



Begin HQ-3  
75.0 ft



End HQ-3  
80.0 ft





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Charlotte, NC 28217  
Phone: 704-525-5152

## ROCK CORE PHOTO LOG

Boring B-7

Project Name: 2020-1 SCDOT Emergency Bridge Package  
Bridge Replacement over Mud Creek on Smith Ford Road

Project Number:  
08:14113

Project Location: York County, South Carolina

Date: 3/18/2020

Begin HQ-1  
78.0 ft

End HQ-1  
83.0 ft





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Charlotte, North Carolina 28217  
(704)525-5152

## PHOTO LOG

Project Name: Emergency Bridge Package 2020-1 S-816 Bridge on Smith Ford Road over Mud Creek	Project Number: 08:14113
Project Location: York County, South Carolina	Date: 03/20/2020



Photo 1: Drill Rig at Boring B-5



Photo 2: Drill Rig at Boring B-6



ECS Southeast, LLP  
1812 Center Park Drive, STE D  
Charlotte, North Carolina 28217  
(704)525-5152

## PHOTO LOG

Project Name: Emergency Bridge Package 2020-1 S-816 Bridge on Smith Ford Road over Mud Creek	Project Number: 08:14113
Project Location: York County, South Carolina	Date: 03/20/2020



Photo 3: Drill Rig at Boring B-7



Photo 4: Drill Rig at Boring B-7

## **APPENDIX C – Laboratory Testing**

Summary of Laboratory Results  
Laboratory Data Sheets  
Rock Coring Summary  
Uniaxial Compressive Strength Reports (3 sheets)

# SUMMARY OF LABORATORY RESULTS

PAGE 1 OF 1

PROJECT ID		PROJECT NAME									
		Emergency Bridge Package 2020-1									
Borehole	Depth	Liquid Limit	Plastic Limit	Plasticity Index	Maximum Size (mm)	%<#200 Sieve	Classification	Water Content (%)	Dry Density (pcf)	Saturation (%)	Void Ratio
B-5	8.0	62	42	20	4.76	79	MH	40.8			
B-5	18.5				2	87	CL	30.4			
B-6	0.0	50	29	21	4.76	68	MH	35.2			
B-6	6.0				2	66	ML	33.5			
B-6	18.5	35	24	11	0.841	92	CL	29.3			
B-6	23.5				2	44	SM	24.4			
B-6	28.5				2	54	ML	21.8			
B-7	0.0				2	76	MH	34.9			
B-7	6.0	43	32	11	2	54	ML	25.8			
B-7	18.5				2	89	ML	31.5			
B-7	28.5				2	46	SM	27.1			
B-8	0.0				4.76	60	CL-ML	23.8			
B-8	2.0				2	35	SC	15.7			
B-8	13.5				4.76	78	CL-ML	29.1			
B-8	18.5	33	21	12	4.76	78	CL	27.1			
B-8	23.5				4.76	50	ML	22.7			

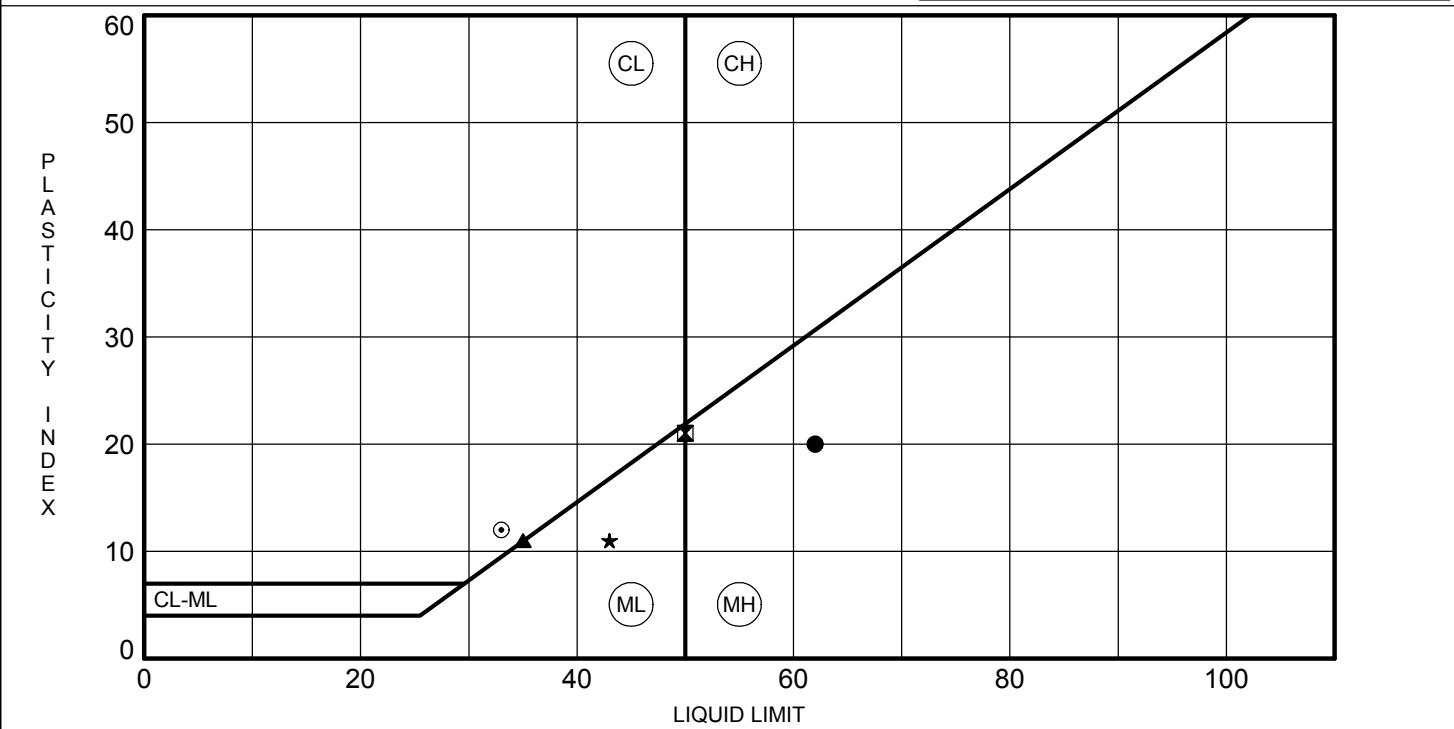


## ATTERBERG LIMITS' RESULTS

PROJECT ID N/A

PROJECT NAME Emergency Bridge Package 2020-1

PROJECT COUNTY York



BOREHOLE	DEPTH	LL	PL	PI	Fines	Classification
● B-5	8.0	62	42	20		Orangish Brown Elastic SILT
■ B-6	0.0	50	29	21		Reddish Brown Elastic SILT
▲ B-6	18.5	35	24	11		Gray Fine to Medium Sandy Lean CLAY
★ B-7	6.0	43	32	11		Reddish Brown Fine to Medium Sandy SILT
◎ B-8	18.5	33	21	12		Gray Fine Sandy Silty CLAY



**TIMELY  
ENGINEERING  
SOIL  
TESTS, LLC**

1874 Forge Street Tucker, GA 30084

Phone: 770-938-8233

Fax: 770-923-8973

Web: [www.test-llc.com](http://www.test-llc.com)



Tested By	EB
Date	03/19/20
Checked By	LB

Client Pr. #	08:14113
Pr. Name	Emergency Bridge Package 2020-1
Sample ID	33521/SS-34 & SS-38
Location	B-6

Lab. PR. #	2020B-03-1
S. Type	Bulk (Composite)
Depth/Elev.	0-10'
Add. Info	-

### ASTM G 57/G187/AASHTO T 288

#### Standard Test Method for Determining Minimum Laboratory Soil Resistivity

##### Determination of Resistivity at as-received moisture content

###### As-received Moisture Content

Mass of Wet Sample & Tare, g  
Mass of Dry Sample & Tare, g  
Mass of Tare, g  
Moisture Content, %

NA

###### Remarks

--

###### TEST DATA

Mass of Soil Box, g  
Mass of Soil Box + Soil, g  
Mass of Soil, g  
Calibrated Volume of Soil Box, ft<sup>3</sup>  
Wet Density of as-placed Soil,pcf  
Dry Density of as-placed Soil,pcf

-
-
-
0.0027
-
-

Meter Dial Reading, ohms  
Reading of Meter Range Multiplier  
Measured Resistance, ohms  
Calibrated Soil Box Multiplier, cm

-
-
NA
1.0

Reported Soil Resistivity, ohms-cm

NA
----

##### Determination of Minimum Soil Resistivity

###### TEST DATA

###### Trials at Various Moisture Content

###### TRIAL #

1	2	3	4	5	6	7	8	9
11.6	10.8	10.1	9.8	9.8				
K	K	K	K	K				
11600	10800	10100	9800	9800				
1.0	1.0	1.0	1.0	1.0				
11600	10800	10100	9800	9800				

Reported Soil Minimum Resistivity, ohms-cm

9800
------

Note: Material passed # 10 sieve used for testing

Oven ID #

496/610

Balance ID #

563/700

Soil Box ID #

612/613/707

Resistivity Meter ID #

706

Description

NA
----

USCS (D2487; D2488)

NA
----

AASHTO (M145)

NA
----



# TIMELESS ENGINEERING SOIL TESTS, LLC

1874 Forge Street Tucker, GA 30084

Phone: 770-938-8233

Fax: 770-923-8973

Web: [www.test-llc.com](http://www.test-llc.com)



Tested By

EB

Da

03/19/20

Checked By

1

Client Pr. #	14:9922
Pr. Name	Emergency Bridge Package 2020-1
Sample ID	33521/SS-34 & SS-38
Location	B-6

Lab. PR. #	2020B-03-1
S. Type	Bulk (Composite)
Depth/Elev.	0-10'
Add. Info	-

ASTM G51

## **Standard Test Method for Determining pH of Soil for Use in Corrosion Testing**

## SAMPLE PREPARATION

Roots, Stones, Gravel and other deleterious material was removed prior to testing

Measurements performed at room temperature condition:

20.9 °C

## TEST DATA

## REMARKS

NIST TRACEABLE BUFFER SOLUTIONS (4.0; 7.0; 10.0 pH) were used for CALIBRATION of pH METER prior to testing.

pH Meter ID 375/732/733



# TIMELY ENGINEERING SOIL TESTS, LLC

1874 Forge Street Tucker, GA 30084

Phone: 770-938-8233

Fax: 770-923-8973

Web: [www.test-llc.com](http://www.test-llc.com)



### Tested By

KF

1

03/18/20

Checked By

4

Client Pr. #	14:9922 & 08:14113
Pr. Name	Emergency Bridge Package 2020-1
Sample ID	Various (see below)
Location	-

Lab. PR. #	2020B-03-1
S. Type	Bag
Depth/Elev.	Various (see below)
Add. Info	-

## Analytical Testing Results for Water Soluble Chloride Ion Content in Soil (Method AASHTO T291)





# INDEX PROPERTIES VERSUS DEPTH

PROJECT ID N/A

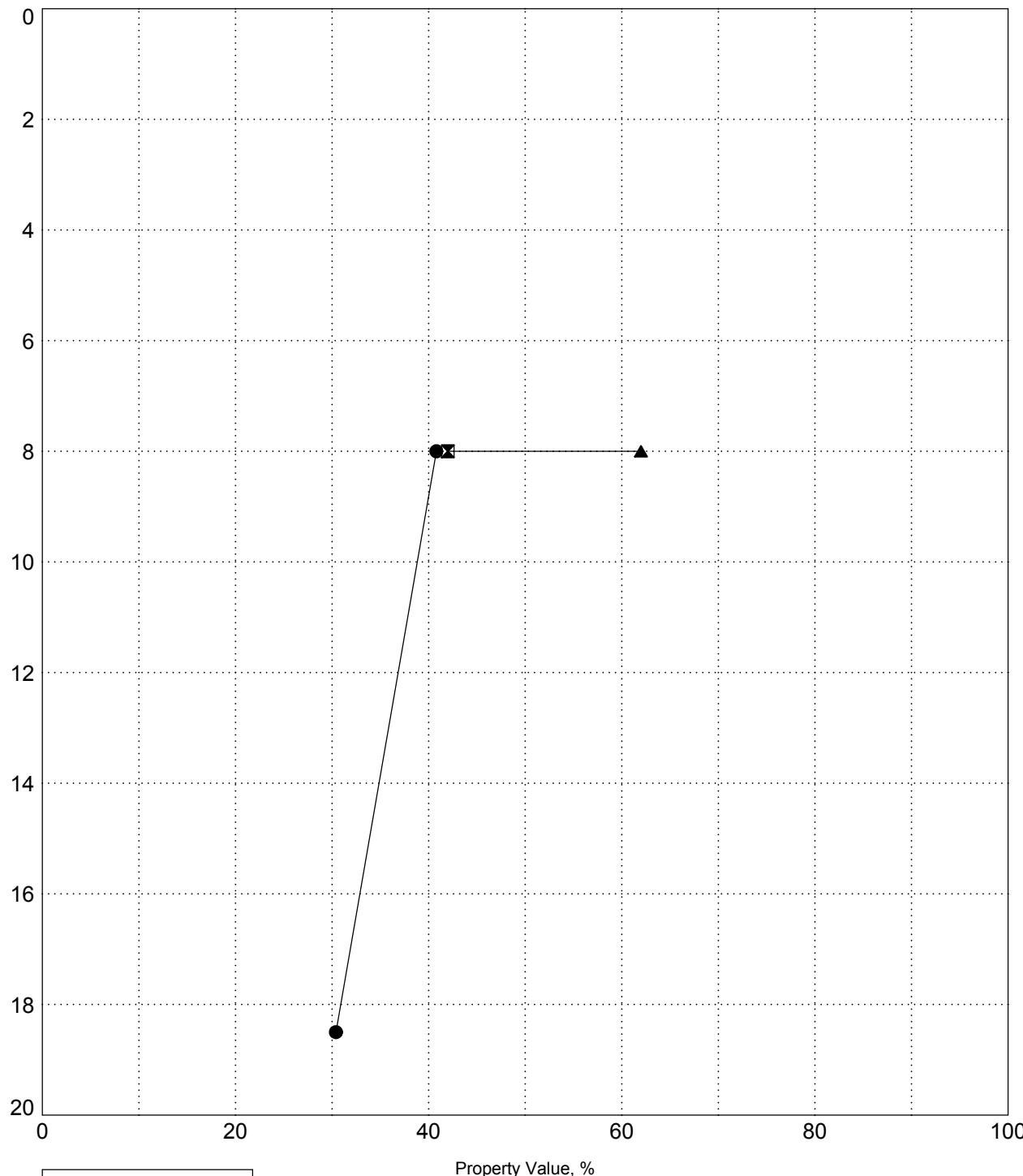
PROJECT NAME Emergency Bridge Package 2020-1

PROJECT COUNTY York

## BORING B-5

SURFACE ELEVATION: 445.0

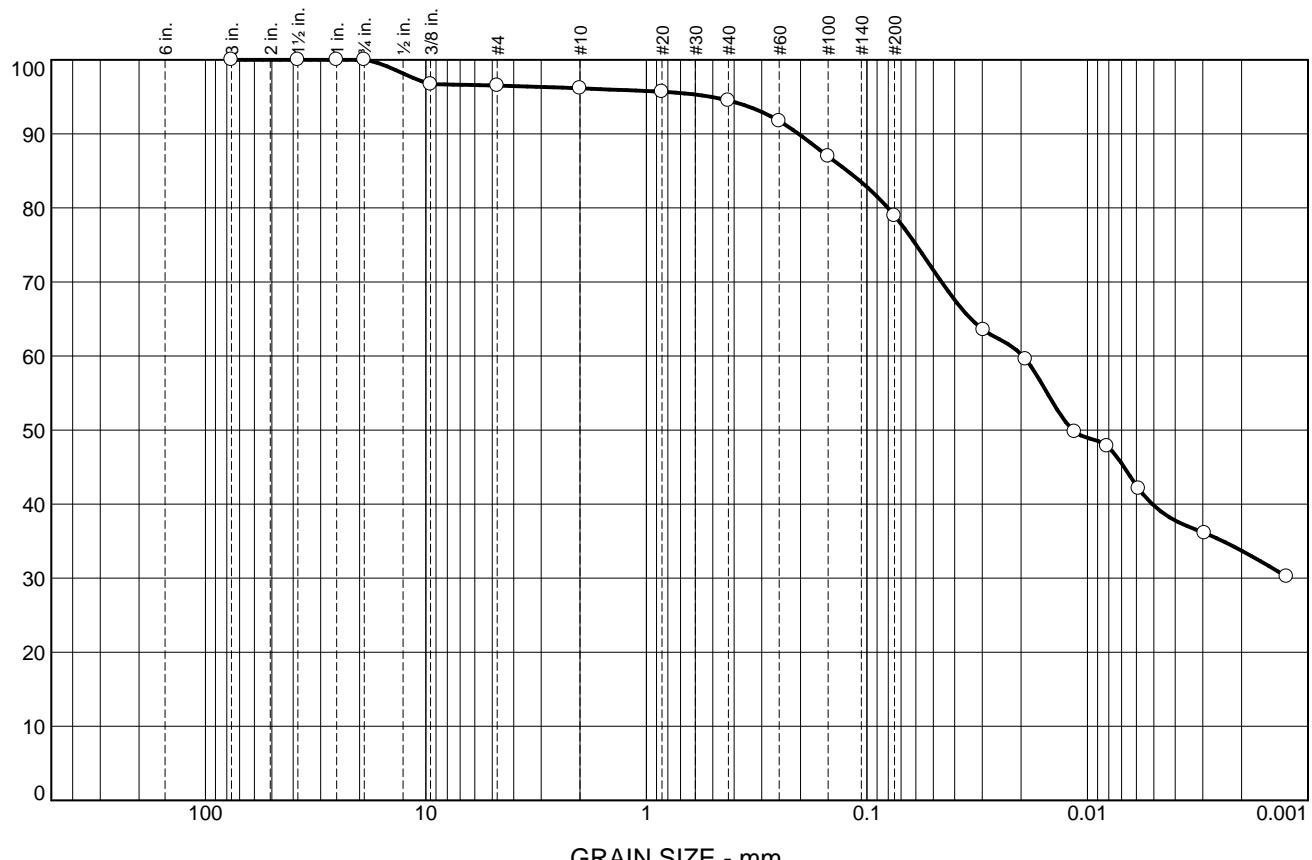
DEPTH, feet



LEGEND	
●	Water Content
☒	Plastic Limit
▲	Liquid Limit
★	Fines

These results are for the exclusive use of the client for whom they were obtained. They apply only to the samples tested and are not indicative of apparently identical soils.

# Particle Size Distribution Report



% +3"	% Gravel	% Sand		% Fines	
		Coarse	Fine	Silt	Clay
0	4	1	16	45	34

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
3	100		
1.5	100		
1	100		
.75	100		
.375	97		
#4	97		
#10	96		
#20	96		
#40	95		
#60	92		
#100	87		
#200	79		
0.0296 mm.	64		
0.0191 mm.	60		
0.0114 mm.	50		
0.0081 mm.	48		
0.0059 mm.	42		
0.0029 mm.	36		
0.0013 mm.	30		

\* (no specification provided)

## Soil Description

Orange Silty Clay (A-7-5(20))

PL= 42

Atterberg Limits

LL= 62

PI= 20

## Coefficients

D<sub>90</sub>= 0.2043

D<sub>85</sub>= 0.1227

D<sub>60</sub>= 0.0196

D<sub>50</sub>= 0.0117

D<sub>30</sub>=

D<sub>15</sub>=

D<sub>10</sub>=

C<sub>u</sub>=

C<sub>c</sub>=

USCS=

## Classification

AASHTO= A-7-5(20)

F.M.=0.39

## Remarks

Sample Number: B-5

Depth: 8.0-10.0'

Date: 3.19



ECS SOUTHEAST, LLP

1812 Center Park Drive, Suite D  
Charlotte, NC 28217  
Phone: (704) 525-5152  
Fax: (704) 357-0023

Client: SCDDOT

Project: Emergency Bridge Package 2020-1 - York County

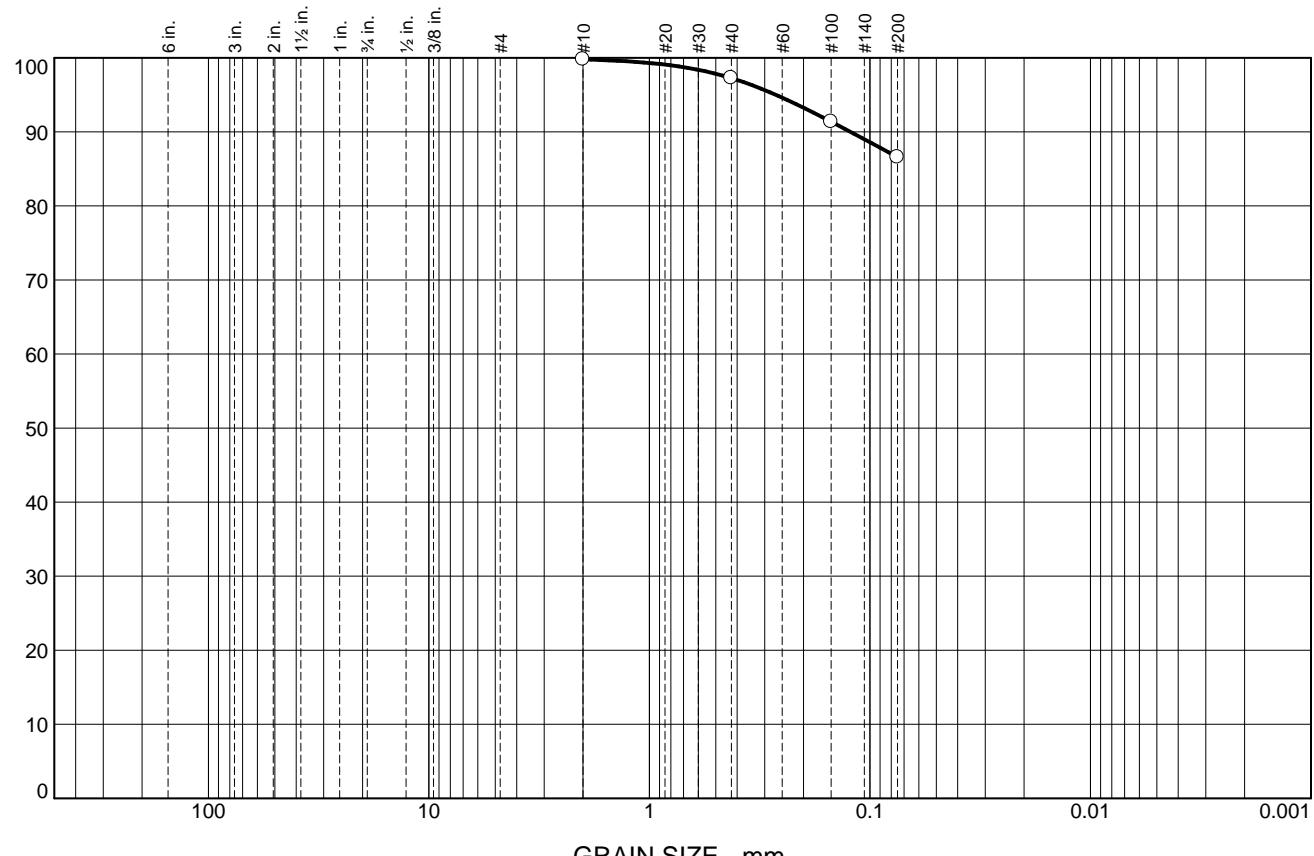
Project No: 14113

Figure

Tested By: CER

These results are for the exclusive use of the client for whom they were obtained. They apply only to the samples tested and are not indicative of apparently identical soils.

# Particle Size Distribution Report



% +3"	% Gravel	% Sand		% Fines	
		Coarse	Fine	Silt	Clay
		3	10	87	

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#10	100		
#40	97		
#100	91		
#200	87		

\* (no specification provided)

<u>Soil Description</u>		
PL=	<u>Atterberg Limits</u>	PI=
LL=	D <sub>90</sub> = 0.1225	D <sub>60</sub> =
D <sub>50</sub> =	D <sub>85</sub> =	D <sub>15</sub> =
D <sub>10</sub> =	C <sub>u</sub> =	C <sub>c</sub> =
USCS=	<u>Coefficients</u>	AASHTO=
	D <sub>30</sub> =	
	C <sub>c</sub> =	
<u>Classification</u>		
USCS=	AASHTO=	
<u>Remarks</u>		
Natural Moisture: 30.4%		
F.M.=0.15		

**Sample Number:** B-5

**Depth:** 18.5-20.0'

**Date:** 3.20.2020



**ECS SOUTHEAST, LLP**  
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Charlotte, NC 28217  
Phone: (704) 525-5152  
Fax: (704) 357-0023

**Client:** SCDDOT

**Project:** Emergency Bridge Package 2020-1 - York County

**Project No:** 14113

**Figure**

**Tested By:** CER



# INDEX PROPERTIES VERSUS DEPTH

PROJECT ID N/A

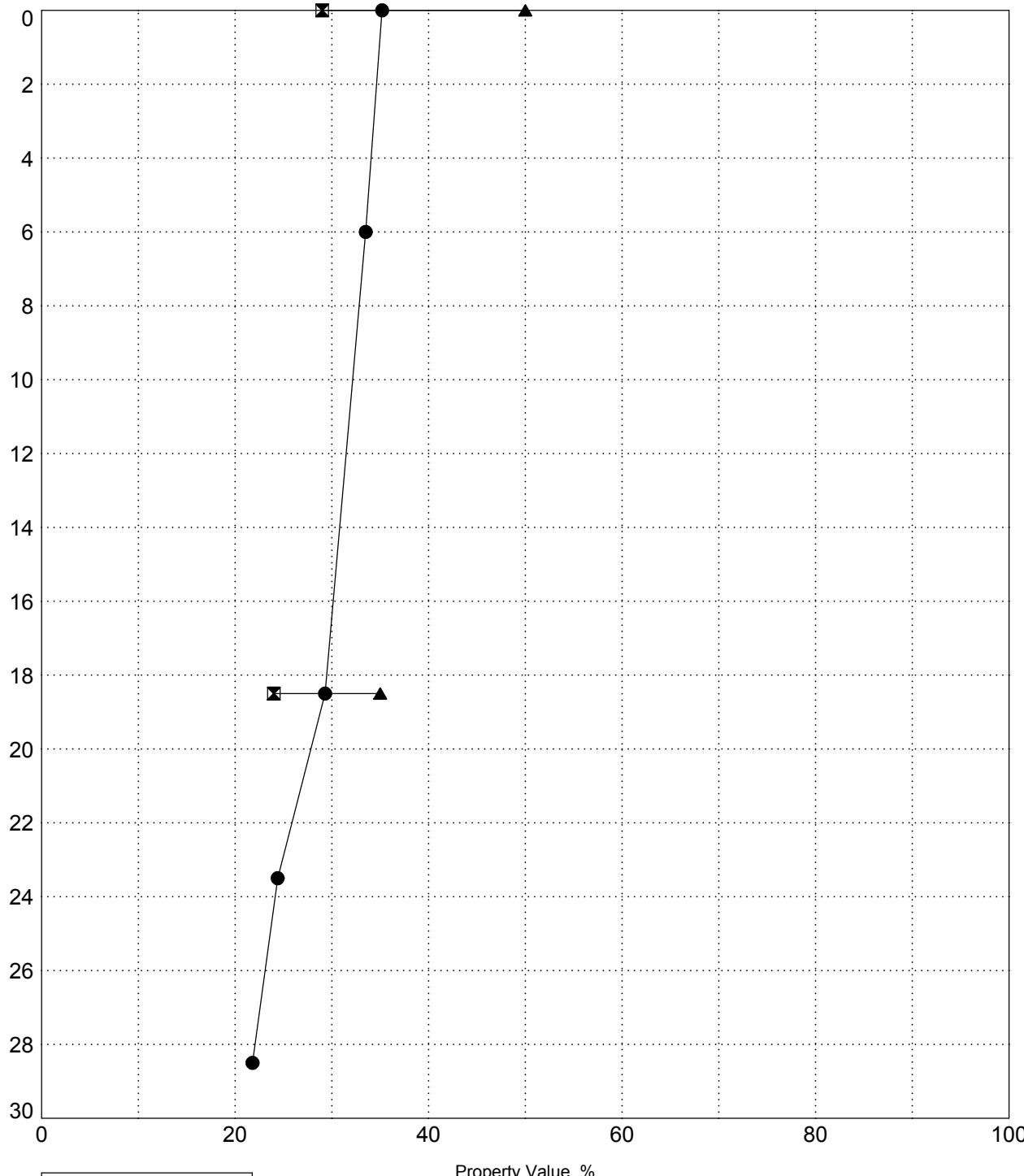
PROJECT NAME Emergency Bridge Package 2020-1

PROJECT COUNTY York

SURFACE ELEVATION: 445.1

## BORING B-6

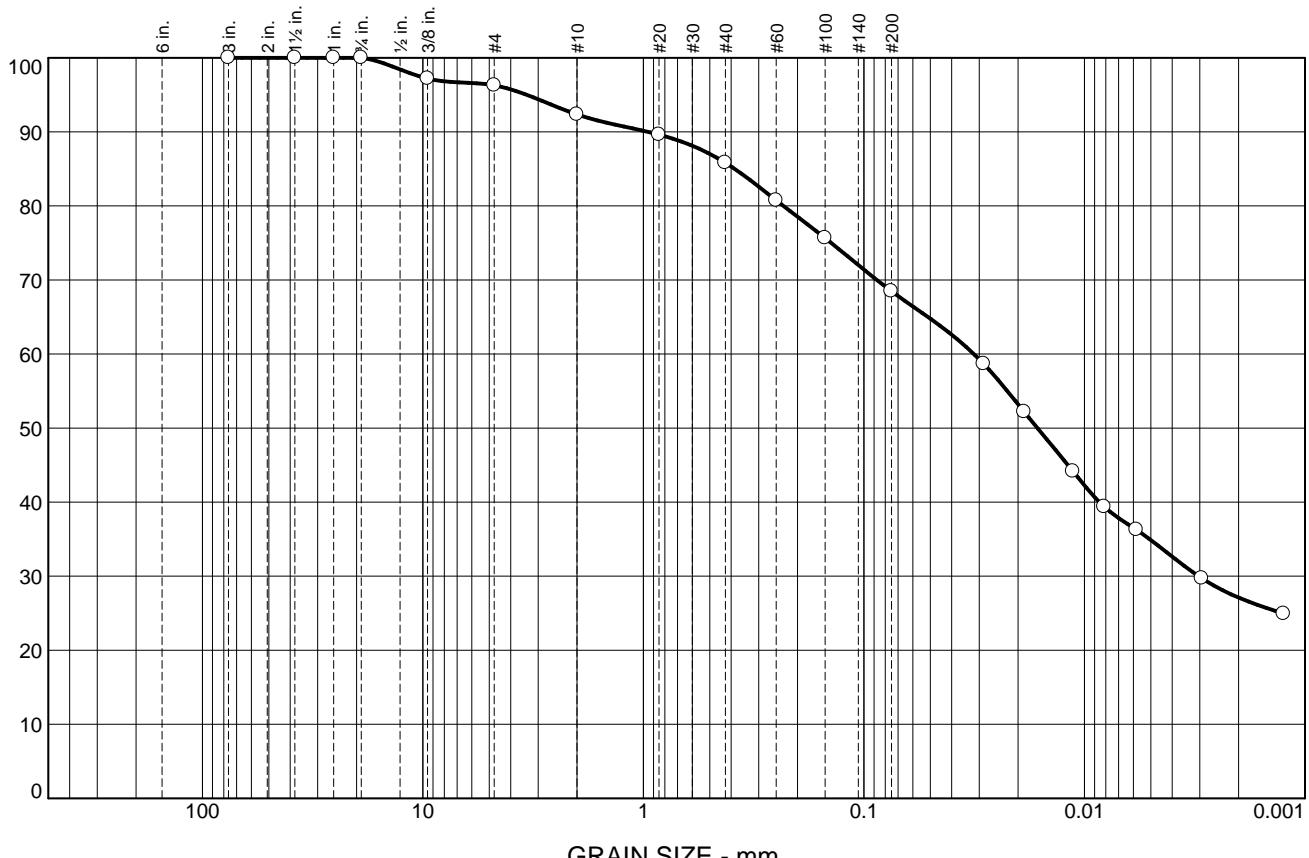
DEPTH, feet



LEGEND	
●	Water Content
☒	Plastic Limit
▲	Liquid Limit
★	Fines

These results are for the exclusive use of the client for whom they were obtained. They apply only to the samples tested and are not indicative of apparently identical soils.

# Particle Size Distribution Report



% +3"	% Gravel	% Sand		% Fines	
		Coarse	Fine	Silt	Clay
		0	8	6	18

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
3	100		
1.5	100		
1	100		
.75	100		
.375	97		
#4	96		
#10	92		
#20	90		
#40	86		
#60	81		
#100	76		
#200	68		
0.0286 mm.	59		
0.0188 mm.	52		
0.0113 mm.	44		
0.0081 mm.	39		
0.0058 mm.	36		
0.0029 mm.	30		
0.0012 mm.	25		

\* (no specification provided)

Soil Description			
Dark red/brown Silty Clay (A-7-6(14))			
PL= 29	Atterberg Limits LL= 50	PI= 21	
D <sub>90</sub> = 0.9548	Coefficients D <sub>85</sub> = 0.3855	D <sub>60</sub> = 0.0317	
D <sub>50</sub> = 0.0163	D <sub>30</sub> = 0.0030	D <sub>15</sub> =	
D <sub>10</sub> =	C <sub>u</sub> =	C <sub>c</sub> =	
USCS=	Classification AASHTO= A-7-6(14)		
	Remarks		
	Natural Moisture: 35.2%		
	F.M.=0.76		

Sample Number: B-6      Depth: 0-2.0'

Date: 3.20.2020



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Phone: (704) 525-5152  
Fax: (704) 357-0023

Client: SCDDOT

Project: Emergency Bridge Package 2020-1 - York County

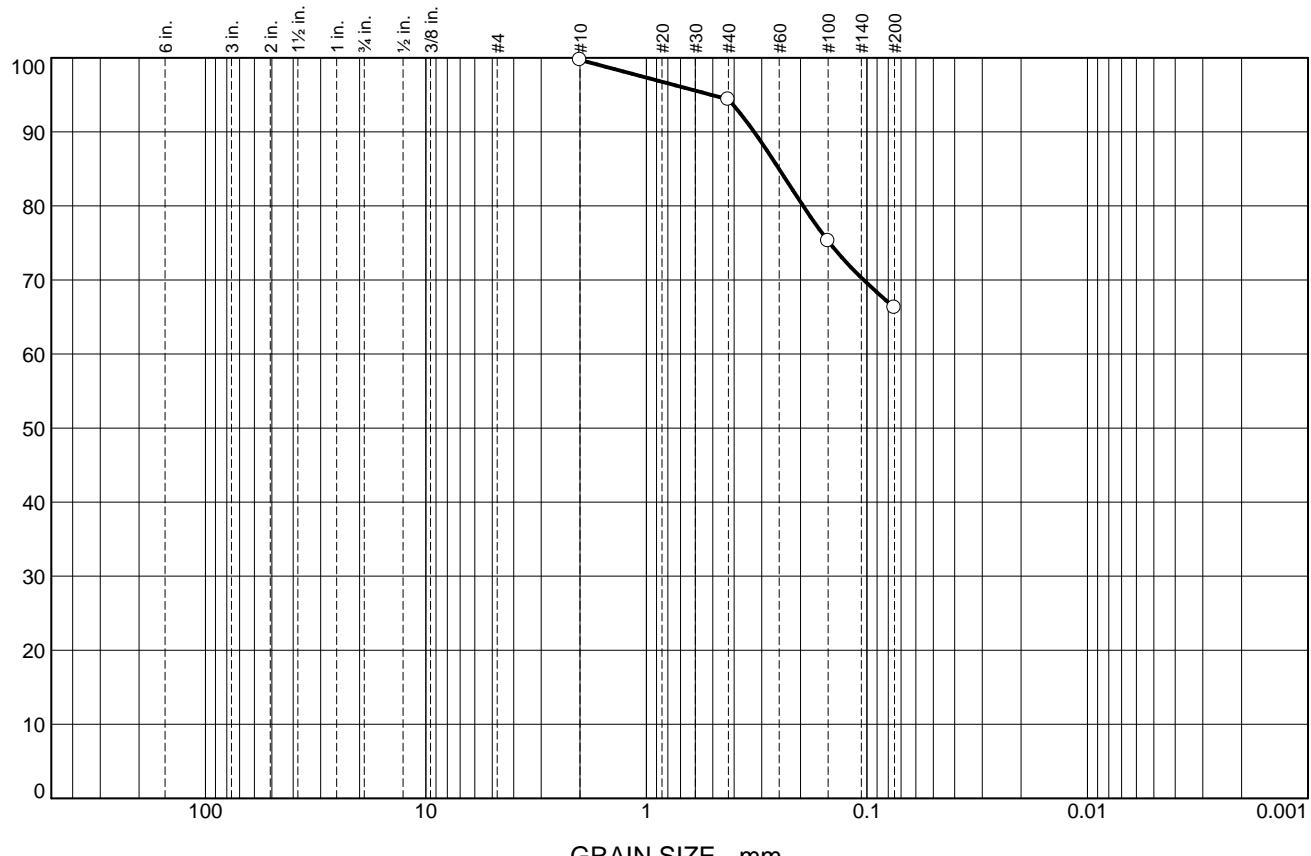
Project No: 14113

Figure

Tested By: CER

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# Particle Size Distribution Report



% +3"	% Gravel	% Sand		% Fines	
		Coarse	Fine	Silt	Clay
		6	28	66	

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#10	100		
#40	94		
#100	75		
#200	66		

\* (no specification provided)

<u>Soil Description</u>		
Firm, moist, orange/brown, fine to medium Sandy Silt		
PL=	<u>Atterberg Limits</u>	PI=
LL=	D <sub>90</sub> = 0.3248	D <sub>60</sub> =
D <sub>50</sub> =	D <sub>85</sub> = 0.2505	D <sub>30</sub> =
D <sub>10</sub> =	C <sub>u</sub> =	C <sub>c</sub> =
USCS=	<u>Coefficients</u>	AASHTO=
	D <sub>50</sub> =	
	C <sub>u</sub> =	
	C <sub>c</sub> =	
<u>Classification</u>		
USCS=	AASHTO=	
<u>Remarks</u>		
Natural Moisture: 33.5 F.M.=0.43		

**Sample Number:** B-6      **Depth:** 6.0-8.0'

**Date:** 3.20.020



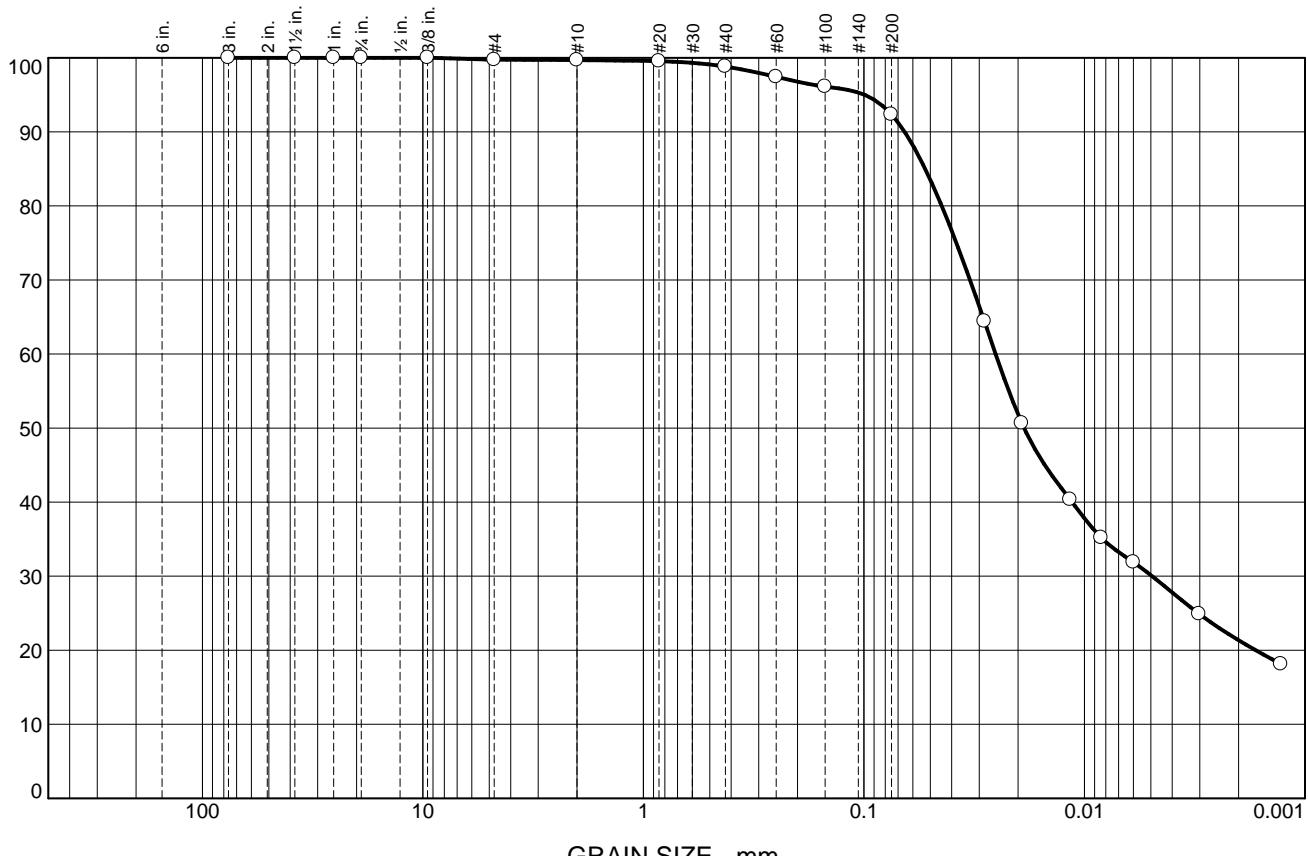
**ECS SOUTHEAST, LLP**  
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**Client:** SCDDOT  
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**Project No:** 14113      **Figure**

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# Particle Size Distribution Report



% +3"	% Gravel	% Sand		% Fines	
		Coarse	Fine	Silt	Clay
0	0	1	7	71	21

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
3	100		
1.5	100		
1	100		
.75	100		
.375	100		
#4	100		
#10	100		
#20	100		
#40	99		
#60	97		
#100	96		
#200	92		
0.0284 mm.	64		
0.0192 mm.	51		
0.0116 mm.	40		
0.0084 mm.	35		
0.0060 mm.	32		
0.0030 mm.	25		
0.0013 mm.	18		

\* (no specification provided)

## Soil Description

Light brown/green Sandy Clay (A-6(11))

## Atterberg Limits

PL= 24 LL= 35 PI= 11

## Coefficients

D<sub>90</sub>= 0.0654 D<sub>85</sub>= 0.0528 D<sub>60</sub>= 0.0253  
D<sub>50</sub>= 0.0188 D<sub>30</sub>= 0.0049 D<sub>15</sub>=  
D<sub>10</sub>= C<sub>u</sub>= C<sub>c</sub>=

## Classification

USCS= AASHTO= A-6(11)

## Remarks

Natural Moisture: 29.3%

F.M.=0.08

Sample Number: B-6

Depth: 18.5-20.0'

Date: 3.20.2020



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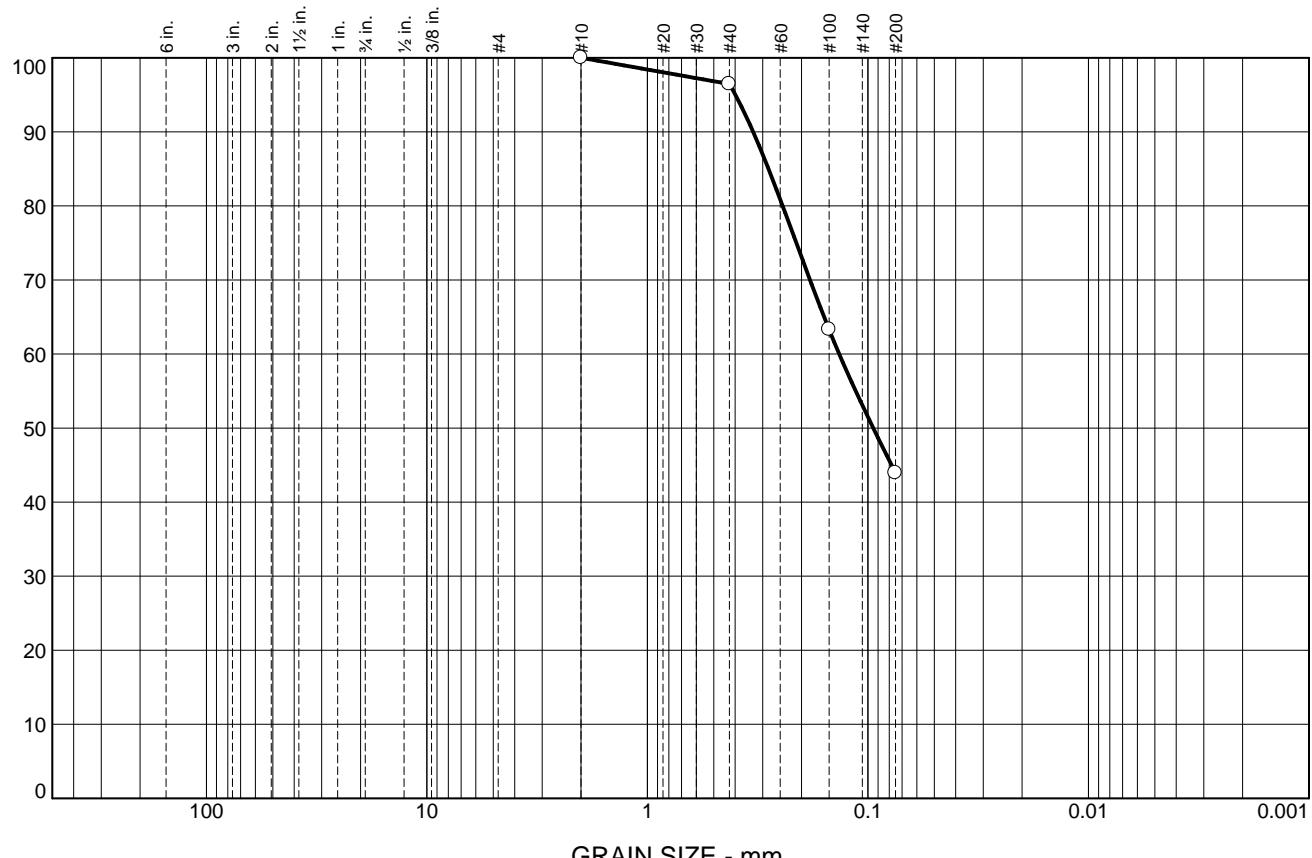
Project No: 14113

Figure

Tested By: CER

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# Particle Size Distribution Report



% +3"	% Gravel	% Sand		% Fines	
		Coarse	Fine	Silt	Clay
0	0	4	52	44	

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#10	100		
#40	96		
#100	63		
#200	44		

\* (no specification provided)

### Soil Description

Soft, moist, gray fine to medium Sandy Silt

### Atterberg Limits

PL= LL= PI=

### Coefficients

D<sub>90</sub>= 0.3314 D<sub>85</sub>= 0.2825 D<sub>60</sub>= 0.1349  
D<sub>50</sub>= 0.0946 D<sub>30</sub>= D<sub>15</sub>=  
D<sub>10</sub>= C<sub>u</sub>= C<sub>c</sub>=

### Classification

USCS= AASHTO=

### Remarks

Natural Moisture: 24.4%

F.M.=0.54

**Sample Number:** B-6      **Depth:** 23.5-25.0'

**Date:** 3.20.2020



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**Client:** SCDDOT

**Project:** Emergency Bridge Package 2020-1 - York County

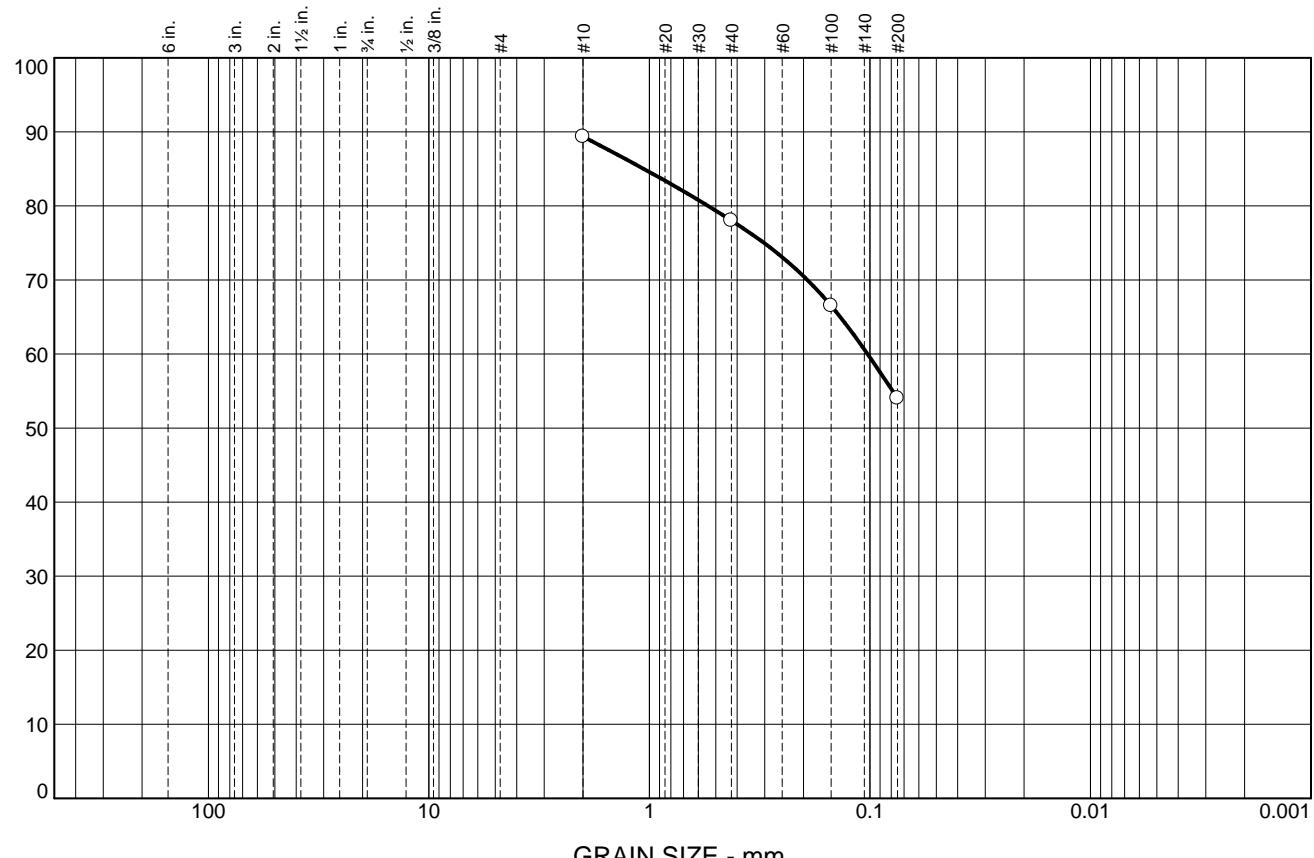
**Project No:** 14113

**Figure**

**Tested By:** CER

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# Particle Size Distribution Report



% +3"	% Gravel	% Sand		% Fines	
		Coarse	Fine	Silt	Clay
		11	24	54	

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#10	89		
#40	78		
#100	67		
#200	54		

\* (no specification provided)

<u>Soil Description</u>				
Gray/brown fine to medium Sandy Silt				
PL=	<u>Atterberg Limits</u>	PI=		
LL=	D <sub>85</sub> = 1.0614	D <sub>60</sub> = 0.1025		
D <sub>50</sub> =	D <sub>30</sub> =	D <sub>15</sub> =		
D <sub>10</sub> =	C <sub>u</sub> =	C <sub>c</sub> =		
USCS=	<u>Classification</u>			
	AASHTO=			
<u>Remarks</u>				
Natural Moisture: 21.8% F.M.=0.92				

**Sample Number:** B-6      **Depth:** 28.5-30.0'

**Date:** 3.20.2020



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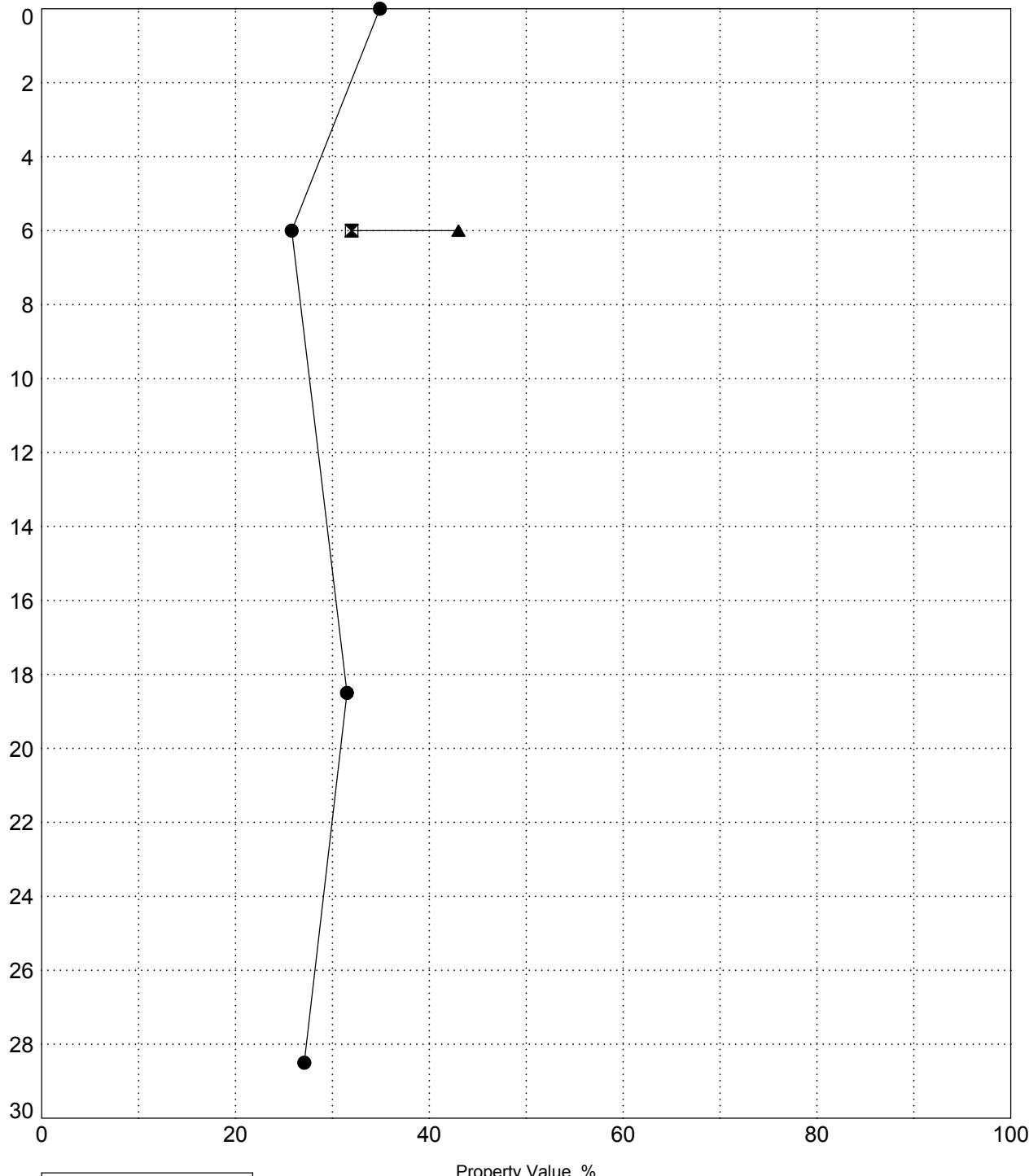
**Client:** SCDDOT  
**Project:** Emergency Bridge Package 2020-1 - York County  
**Project No:** 14113      **Figure**

**Tested By:** CER

PROJECT ID N/APROJECT NAME Emergency Bridge Package 2020-1PROJECT COUNTY York**BORING B-7**

SURFACE ELEVATION: 444.9

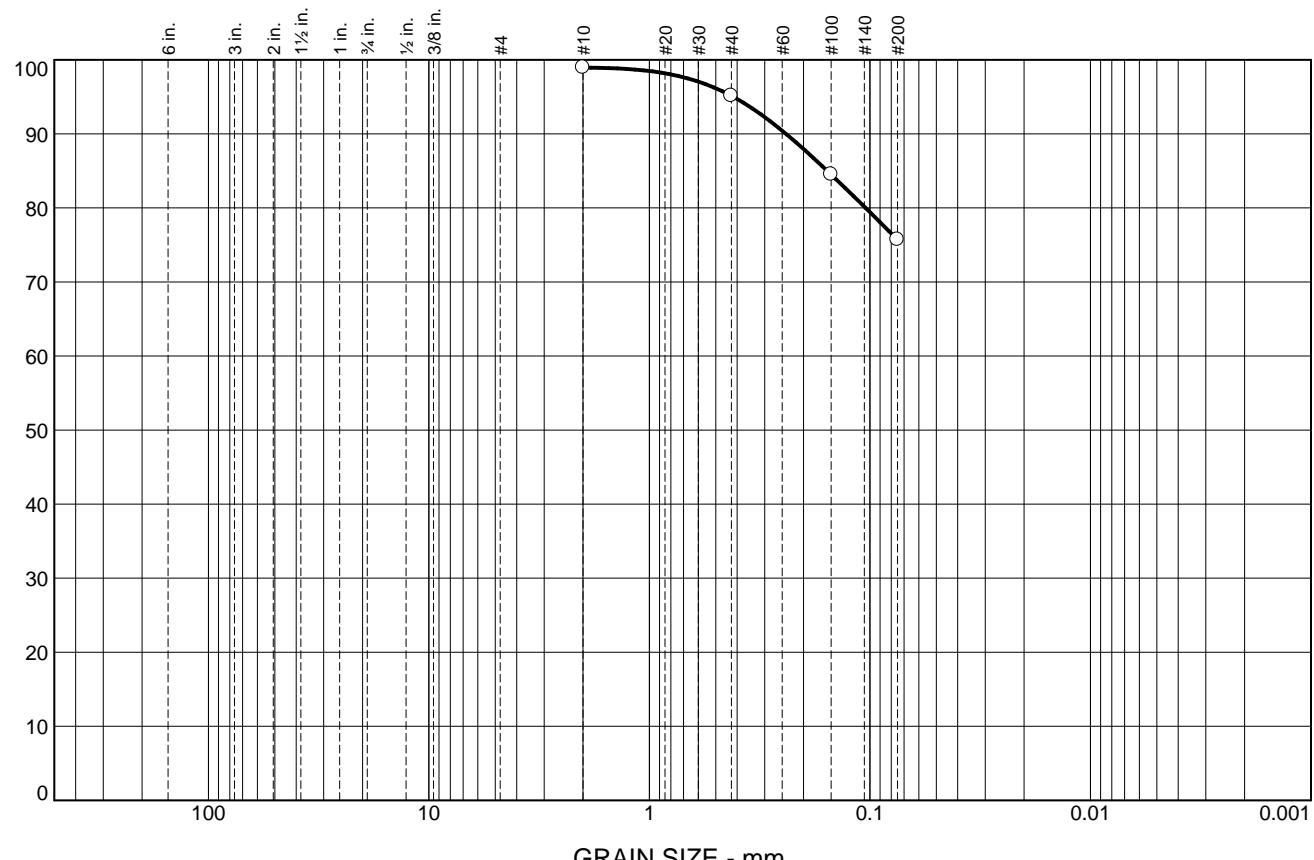
DEPTH, feet



LEGEND	
●	Water Content
■	Plastic Limit
▲	Liquid Limit
★	Fines

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# Particle Size Distribution Report



% +3"	% Gravel	% Sand		% Fines	
		Coarse	Fine	Silt	Clay
		4	19	76	

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#10	99		
#40	95		
#100	85		
#200	76		

\* (no specification provided)

Soil Description		
Red/brown Elastic Silt		
PL=	Atterberg Limits	PI=
LL=	D <sub>85</sub> = 0.1561	D <sub>60</sub> =
D <sub>50</sub> =	D <sub>30</sub> =	D <sub>15</sub> =
D <sub>10</sub> =	C <sub>u</sub> =	C <sub>c</sub> =
USCS=	Classification	AASHTO=
	Natural Moisture: 34.9%	
	F.M.=0.27	
	<u>Remarks</u>	

Sample Number: B-7

Depth: 0.0-2.0'

Date: 3.20.2020



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Client: SCDDOT

Project: Emergency Bridge Package 2020-1 - York County

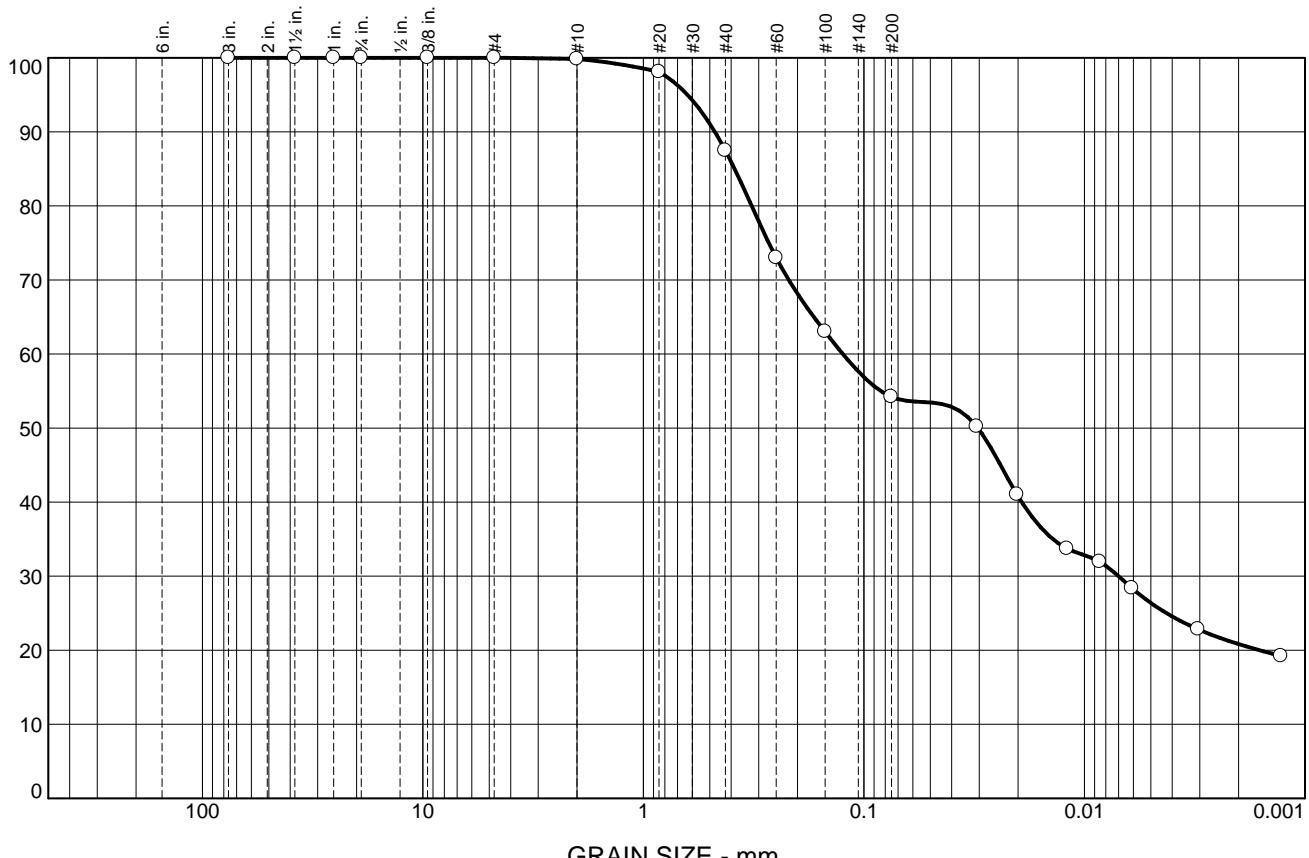
Project No: 14113

Figure

Tested By: CER

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# Particle Size Distribution Report



% +3"	% Gravel	% Sand		% Fines	
		Coarse	Fine	Silt	Clay
0	0	13	33	33	21

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
3	100		
1.5	100		
1	100		
.75	100		
.375	100		
#4	100		
#10	100		
#20	98		
#40	87		
#60	73		
#100	63		
#200	54		
0.0308 mm.	50		
0.0202 mm.	41		
0.0120 mm.	34		
0.0085 mm.	32		
0.0061 mm.	28		
0.0031 mm.	23		
0.0013 mm.	19		

\* (no specification provided)

## Soil Description

Orange/brown Silty Clay (a-7-5(4))

PL= 32

Atterberg Limits

LL= 43

PI= 11

## Coefficients

D<sub>90</sub>= 0.4741

D<sub>85</sub>= 0.3859

D<sub>60</sub>= 0.1246

D<sub>50</sub>= 0.0304

D<sub>30</sub>= 0.0070

D<sub>15</sub>=

D<sub>10</sub>=

C<sub>u</sub>=

C<sub>c</sub>=

USCS= ML

## Classification

AASHTO= A-7-5(4)

## Remarks

Natural Moisture: 25.8%

F.M.=0.66

Sample Number: B-7

Depth: 6.0-8.0'

Date: 3.20.2020



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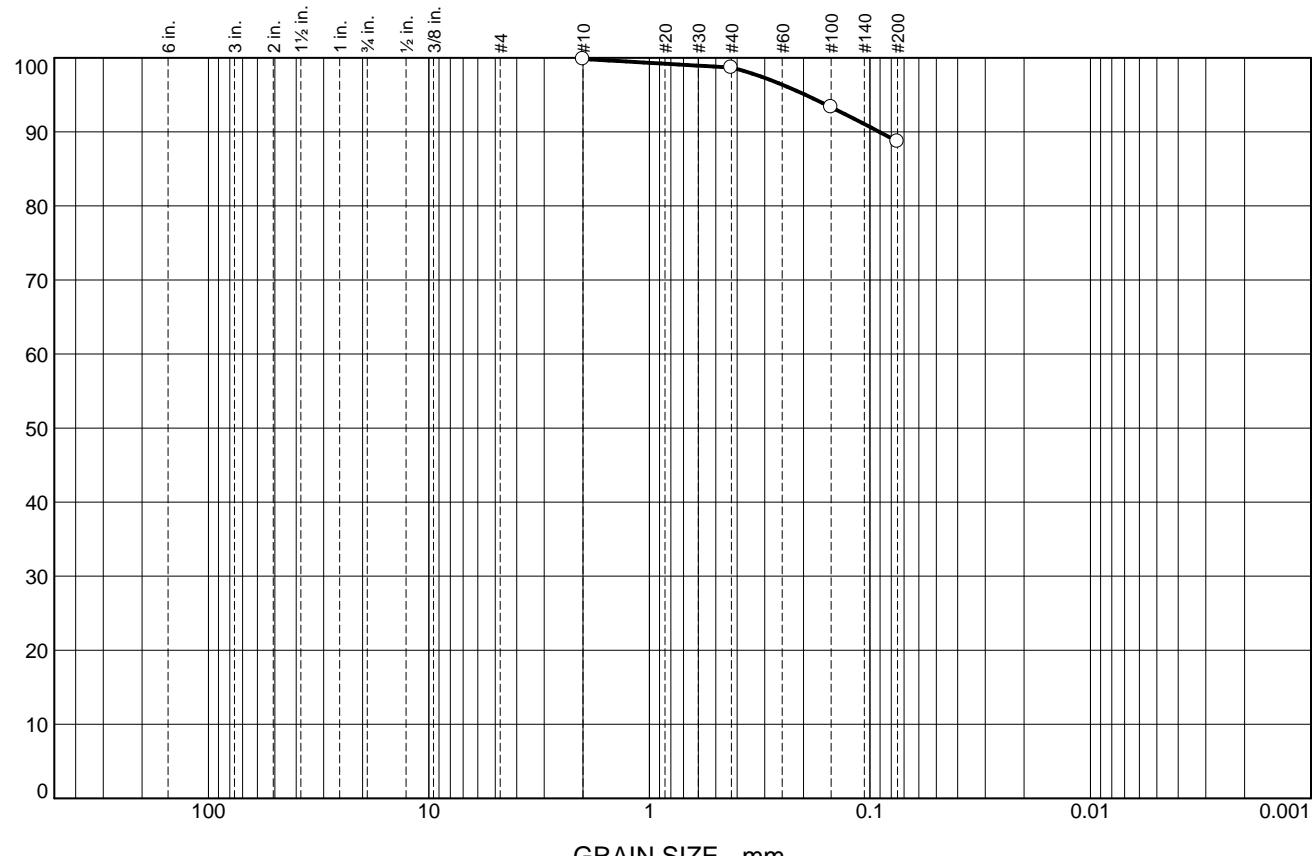
Project No: 14113

Figure

Tested By: CER

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# Particle Size Distribution Report



% +3"	% Gravel	% Sand		% Fines	
		Coarse	Fine	Silt	Clay
		1	10	89	

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#10	100		
#40	99		
#100	93		
#200	89		

\* (no specification provided)

<u>Soil Description</u>		
Gray/brown, fine to medium Sandy Silt		
PL=	<u>Atterberg Limits</u>	PI=
LL=	D <sub>85</sub> =	D <sub>60</sub> =
D <sub>90</sub> = 0.0908	D <sub>50</sub> =	D <sub>15</sub> =
D <sub>50</sub> =	C <sub>u</sub> =	C <sub>c</sub> =
D <sub>10</sub> =		
USCS=	<u>Coefficients</u>	AASHTO=
	D <sub>85</sub> =	
	D <sub>50</sub> =	
	C <sub>u</sub> =	
	C <sub>c</sub> =	
<u>Classification</u>		
USCS= AASHTO=		
<u>Remarks</u>		
Natural Moisture: 31.5% F.M.=0.11		

**Sample Number:** B-7      **Depth:** 18.5-20.0'

**Date:** 3.20.2020



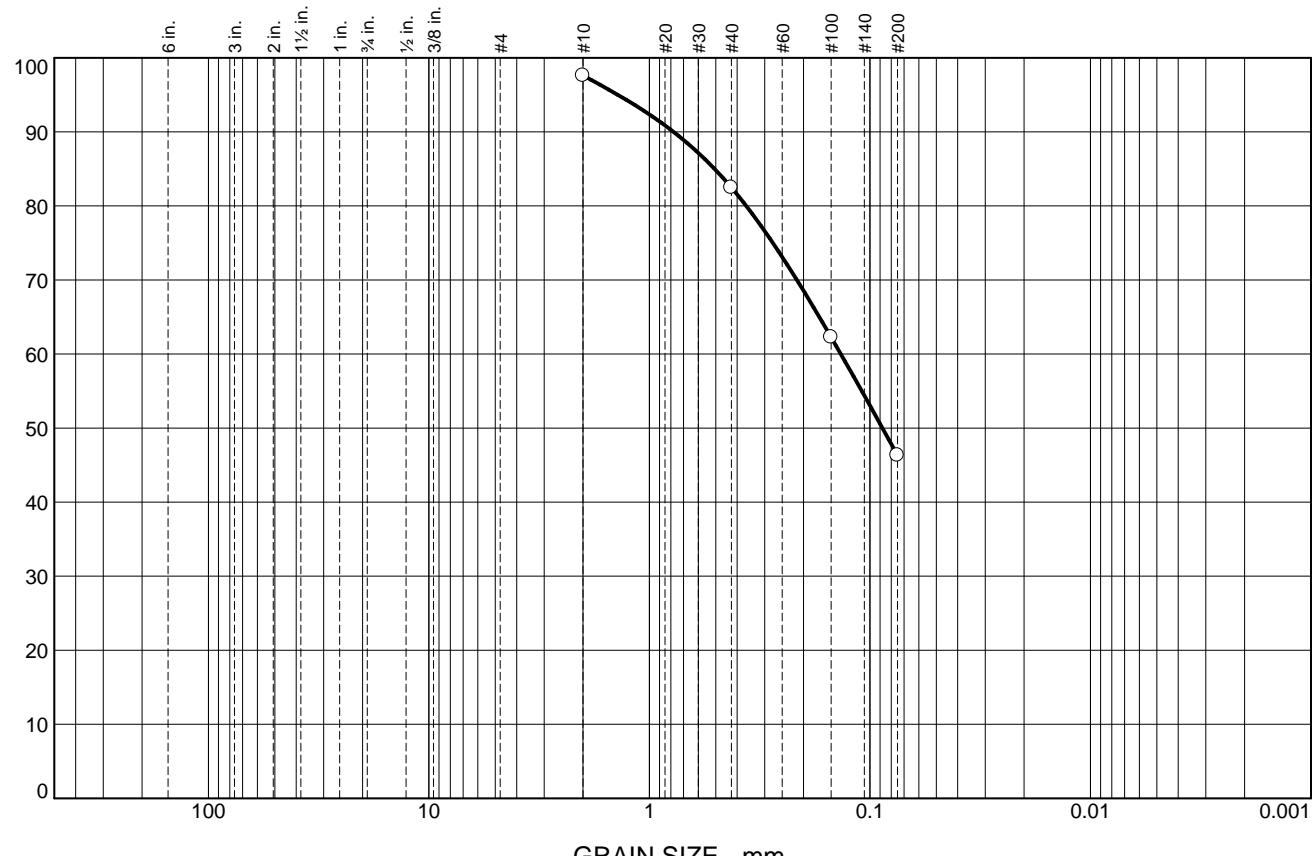
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**Client:** SCDDOT  
**Project:** Emergency Bridge Package 2020-1 - York County  
**Project No:** 14113      **Figure**

**Tested By:** CER

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# Particle Size Distribution Report



% +3"	% Gravel	% Sand		% Fines	
		Coarse	Fine	Silt	Clay
		16	36	46	

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#10	98		
#40	82		
#100	62		
#200	46		

\* (no specification provided)

<u>Soil Description</u>				
Gray/brown, fine to medium Silty Sand				
PL=	<u>Atterberg Limits</u>	PI=		
LL=	D <sub>85</sub> = 0.5066	D <sub>60</sub> = 0.1355		
D <sub>50</sub> = 0.0878	D <sub>30</sub> =	D <sub>15</sub> =		
D <sub>10</sub> =	C <sub>u</sub> =	C <sub>c</sub> =		
USCS=	<u>Coefficients</u>			
AASHTO=	D <sub>90</sub> = 0.7777	D <sub>60</sub> = 0.1355		
	D <sub>50</sub> = 0.0878	D <sub>15</sub> =		
	C <sub>u</sub> =	C <sub>c</sub> =		
<u>Classification</u>				
USCS=	AASHTO=			
<u>Remarks</u>				
Natural Moisture: 27.1% F.M.=0.80				

**Sample Number:** B-7      **Depth:** 28.5-30

**Date:** 3.20.2020



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**Client:** SCDDOT  
**Project:** Emergency Bridge Package 2020-1 - York County  
**Project No:** 14113      **Figure**

**Tested By:** CER



# INDEX PROPERTIES VERSUS DEPTH

PROJECT ID N/A

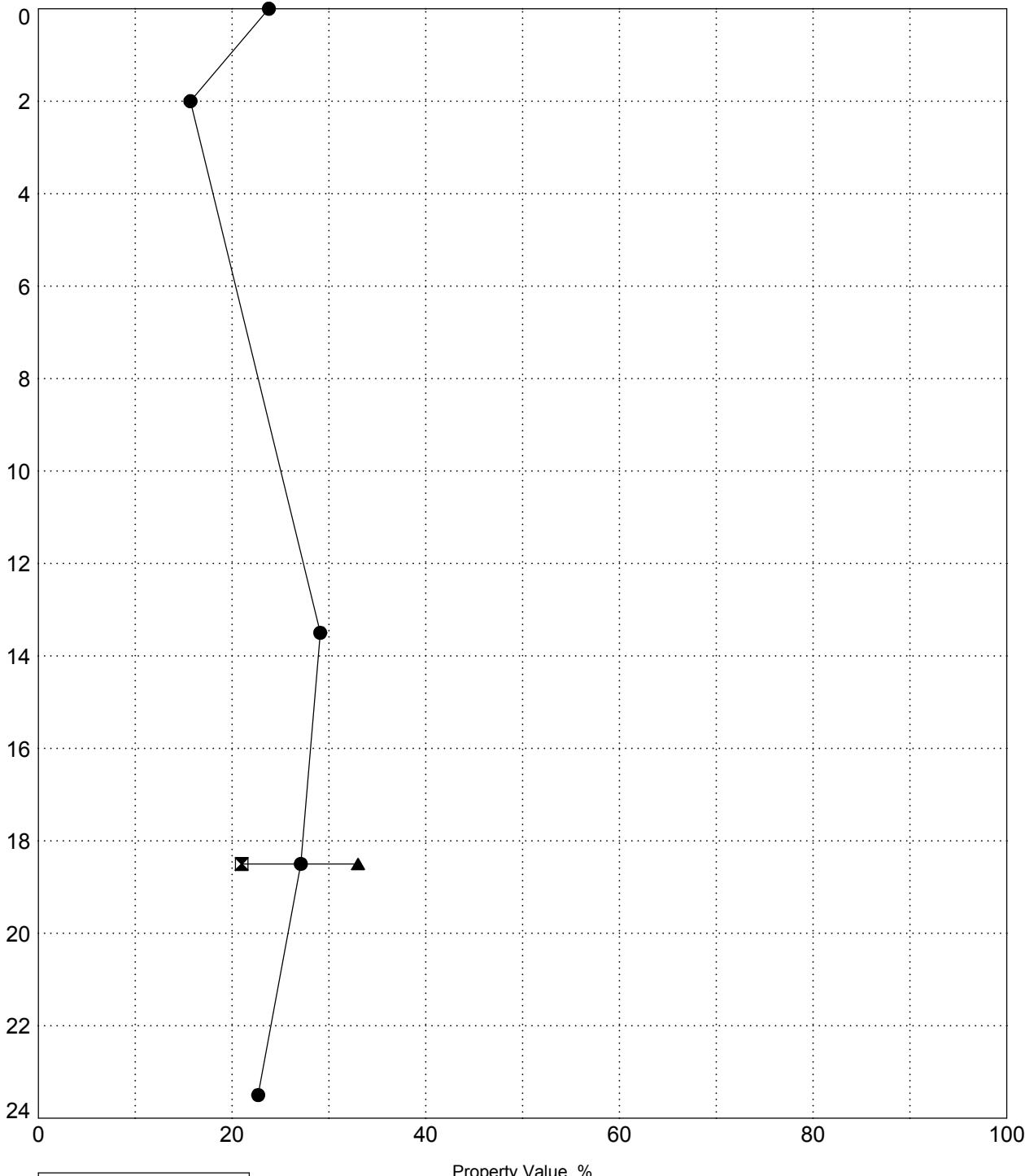
PROJECT NAME Emergency Bridge Package 2020-1

PROJECT COUNTY York

SURFACE ELEVATION: 443.9

## BORING B-8

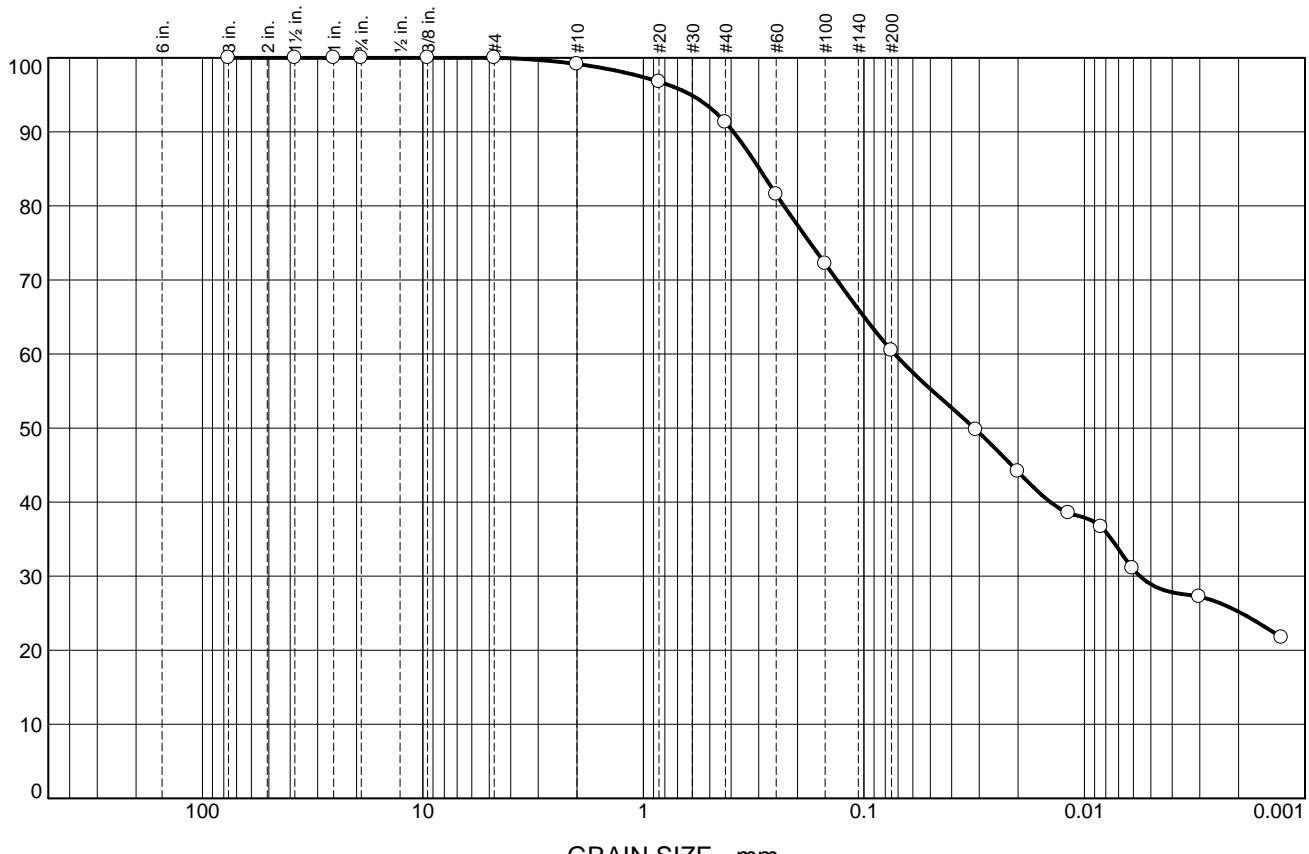
DEPTH, feet



LEGEND	
●	Water Content
■	Plastic Limit
▲	Liquid Limit
★	Fines

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# Particle Size Distribution Report



% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
	0	0	1	8	31	31	29

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
3	100		
1.5	100		
1	100		
.75	100		
.375	100		
#4	100		
#10	99		
#20	97		
#40	91		
#60	82		
#100	72		
#200	60		
0.0311 mm.	50		
0.0201 mm.	44		
0.0118 mm.	39		
0.0084 mm.	37		
0.0061 mm.	31		
0.0030 mm.	27		
0.0013 mm.	22		

\* (no specification provided)

Sample Number: B-8

Depth: 0.0-2.0'

Date: 3.20.2020

## Soil Description

Brown/red Silty Clay

PL=

## Atterberg Limits

LL= PI=

D<sub>90</sub>= 0.3908  
D<sub>50</sub>= 0.0316  
D<sub>10</sub>=

D<sub>85</sub>= 0.2977  
D<sub>30</sub>= 0.0056  
C<sub>u</sub>= C<sub>c</sub>=

USCS=

Classification AASHTO=

Natural Moisture: 23.8%  
F.M.=0.50

## Remarks



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Project: Emergency Bridge Package 2020-1 - York County

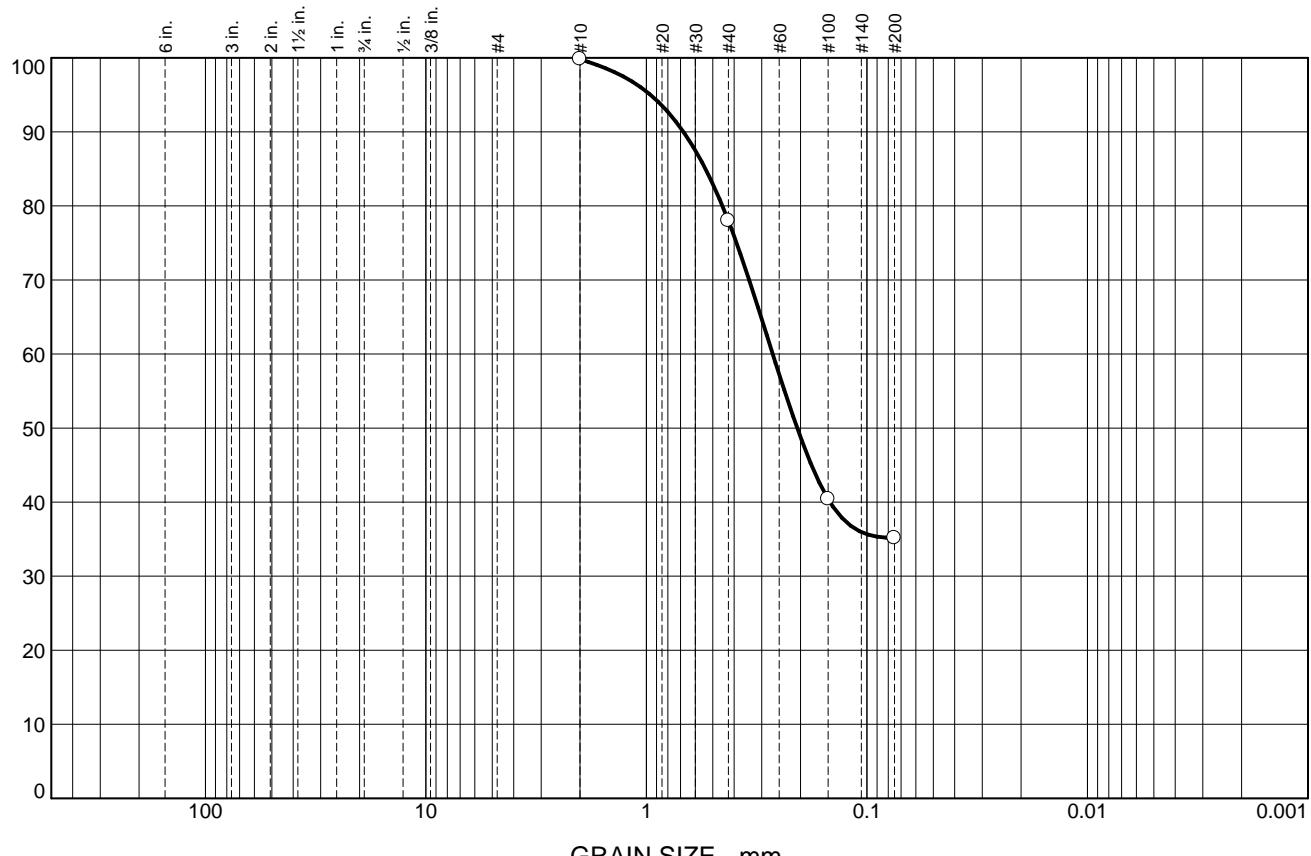
Project No: 14113

Figure

Tested By: CER

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# Particle Size Distribution Report



% +3"	% Gravel	% Sand		% Fines	
		Coarse	Fine	Silt	Clay
		22	43	35	

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#10	100		
#40	78		
#100	40		
#200	35		

\* (no specification provided)

<u>Soil Description</u>				
Red/brown Silty Clay				
PL=	<u>Atterberg Limits</u>	PI=		
	LL=			
D <sub>90</sub> = 0.6793	D <sub>85</sub> = 0.5399	D <sub>60</sub> = 0.2675		
D <sub>50</sub> = 0.2071	D <sub>30</sub> =	D <sub>15</sub> =		
D <sub>10</sub> =	C <sub>u</sub> =	C <sub>c</sub> =		
USCS=	<u>Coefficients</u>			
	D <sub>85</sub> = 0.5399			
	D <sub>30</sub> =			
	C <sub>u</sub> =			
<u>Classification</u>				
AASHTO=				
<u>Remarks</u>				
Natural Moisture: 15.7%				
F.M.=1.10				

**Sample Number:** B-8

**Depth:** 2.0-4.0'

**Date:** 3.20.2020



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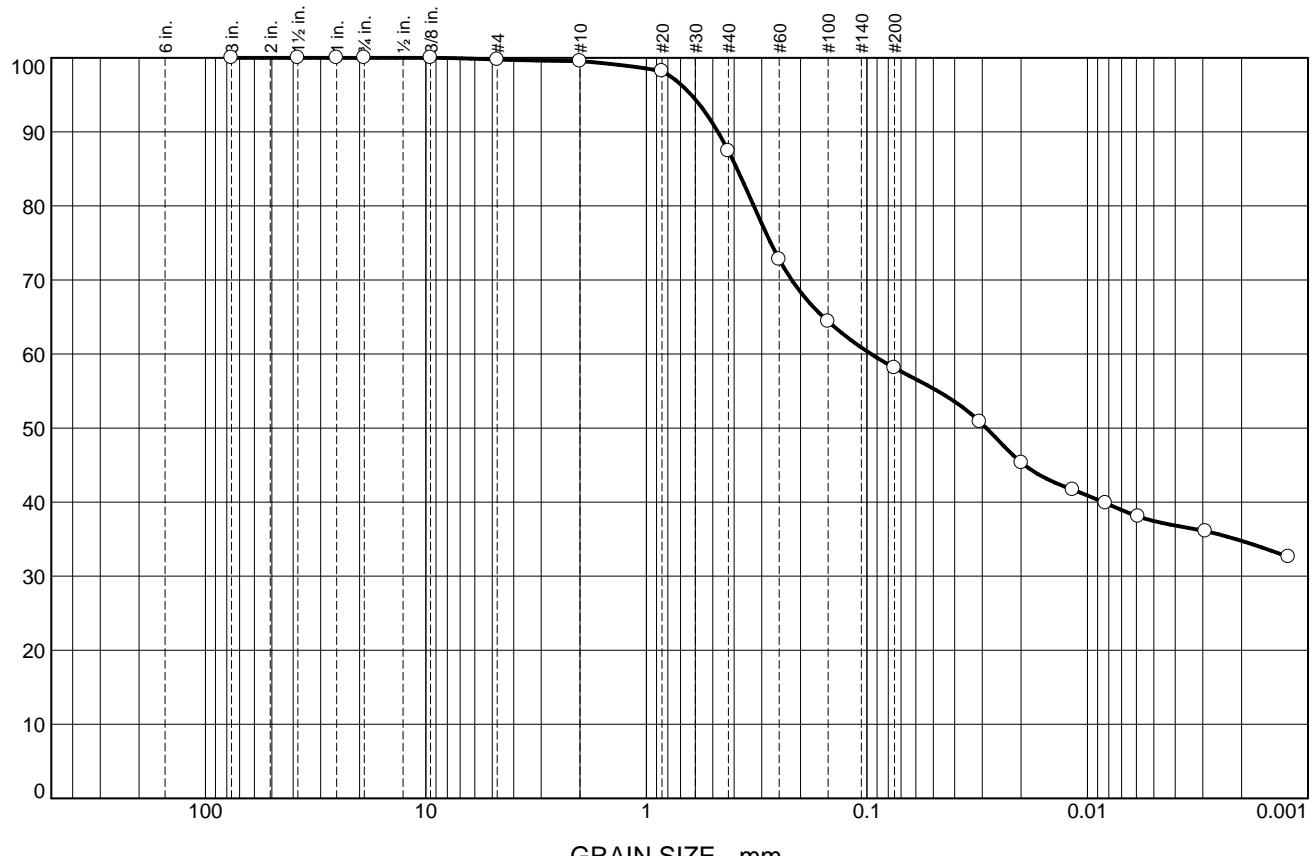
**Project No:** 14113

**Figure**

**Tested By:** CER

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# Particle Size Distribution Report



% +3"	% Gravel	% Sand		% Fines	
		Coarse	Fine	Silt	Clay
0	0	13	29	23	35

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
3	100		
1.5	100		
1	100		
.75	100		
.375	100		
#4	100		
#10	100		
#20	98		
#40	87		
#60	73		
#100	64		
#200	58		
0.0308 mm.	51		
0.0199 mm.	45		
0.0116 mm.	42		
0.0083 mm.	40		
0.0059 mm.	38		
0.0029 mm.	36		
0.0012 mm.	33		

\* (no specification provided)

Soil Description			
Dark red/brown			
Atterberg Limits	Coefficients	Classification	Remarks
PL=	D <sub>90</sub> = 0.4739 D <sub>50</sub> = 0.0287 D <sub>10</sub> =	LL= 0.3880 D <sub>30</sub> = C <sub>u</sub> =	PI= 0.0958 D <sub>15</sub> = C <sub>c</sub> =
USCS=	AASHTO=		Natural Moisture: 29.1% F.M.=0.65

Sample Number: B-8      Depth: 13.5-15.0'

Date: 3.20.2020



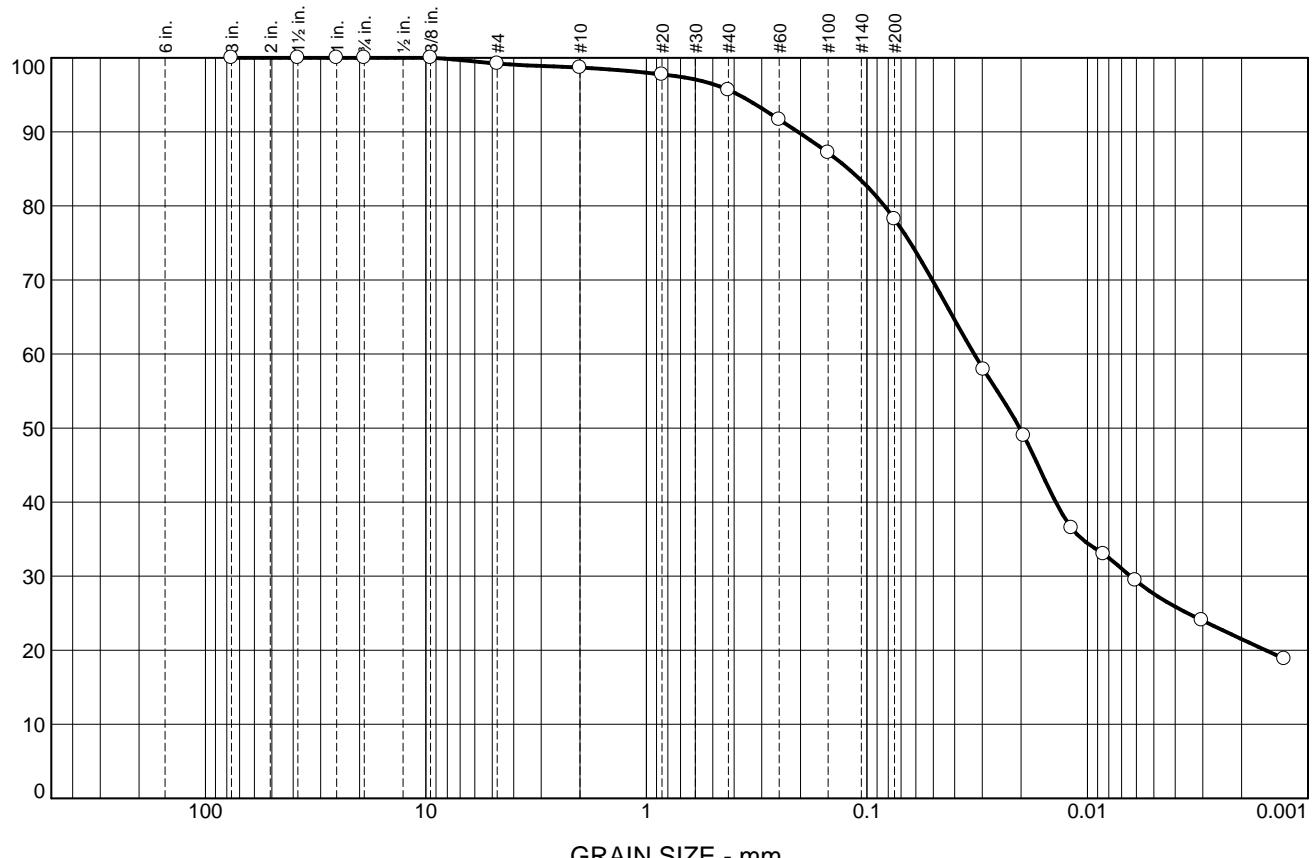
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Client: SCDDOT  
Project: Emergency Bridge Package 2020-1 - York County  
Project No: 14113      Figure

Tested By: CER

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# Particle Size Distribution Report



% +3"	% Gravel	% Sand		% Fines	
		Coarse	Fine	Silt	Clay
0	1	3	18	56	22

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
3	100		
1.5	100		
1	100		
.75	100		
.375	100		
#4	99		
#10	99		
#20	98		
#40	96		
#60	92		
#100	87		
#200	78		
0.0296 mm.	58		
0.0195 mm.	49		
0.0118 mm.	37		
0.0085 mm.	33		
0.0061 mm.	29		
0.0030 mm.	24		
0.0013 mm.	19		

\* (no specification provided)

## Soil Description

Green/gray Sandy Clay (A-6(8))

PL= 21

Atterberg Limits

LL= 33

PI= 12

## Coefficients

D<sub>90</sub>= 0.2056

D<sub>85</sub>= 0.1213

D<sub>60</sub>= 0.0327

D<sub>50</sub>= 0.0203

D<sub>30</sub>= 0.0064

D<sub>15</sub>=

D<sub>10</sub>=

C<sub>u</sub>=

C<sub>c</sub>=

USCS=

Classification

AASHTO= A-6(8)

## Remarks

Natural Moisture: 27.1%

F.M.=0.26

Sample Number: B-8

Depth: 18.5-20.0'

Date: 3.20.2020



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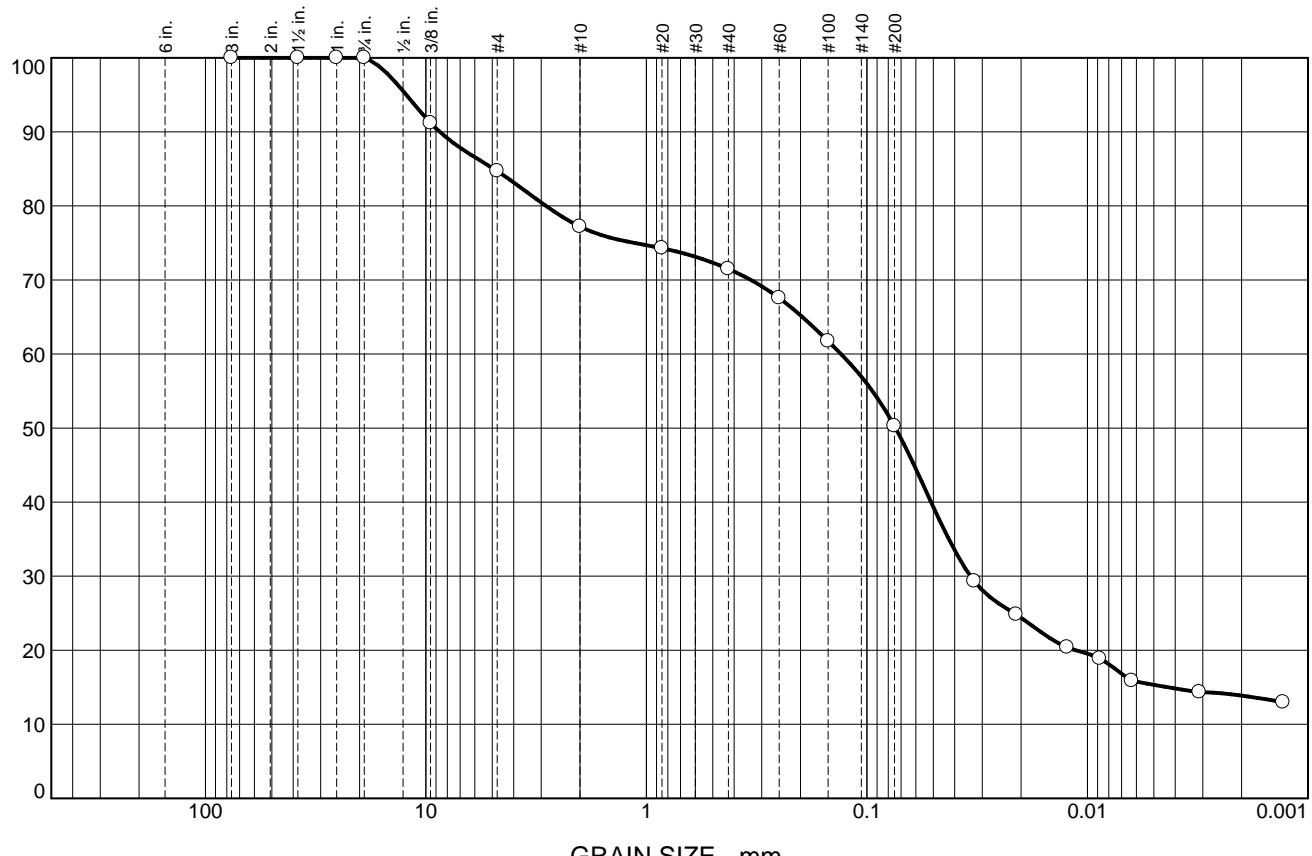
Project No: 14113

Figure

Tested By: CER

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# Particle Size Distribution Report



% +3"	% Gravel	% Sand		% Fines	
		Coarse	Fine	Silt	Clay
0	23	6	21	36	14

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
3	100		
1.5	100		
1	100		
.75	100		
.375	91		
#4	85		
#10	77		
#20	74		
#40	71		
#60	68		
#100	62		
#200	50		
0.0326 mm.	29		
0.0210 mm.	25		
0.0124 mm.	20		
0.0088 mm.	19		
0.0063 mm.	16		
0.0031 mm.	14		
0.0013 mm.	13		

\* (no specification provided)

<u>Soil Description</u>			
Gray/blue			
PL=	<u>Atterberg Limits</u>	LL=	PI=
D <sub>90</sub> = 8.6508	D <sub>85</sub> = 4.9230	D <sub>60</sub> = 0.1311	
D <sub>50</sub> = 0.0741	D <sub>30</sub> = 0.0339	D <sub>15</sub> = 0.0043	
D <sub>10</sub> =	C <sub>u</sub> =	C <sub>c</sub> =	
USCS=	<u>Coefficients</u>	AASHTO=	
	D <sub>90</sub> = 8.6508	D <sub>85</sub> = 4.9230	
	D <sub>50</sub> = 0.0741	D <sub>30</sub> = 0.0339	
	D <sub>10</sub> =	C <sub>u</sub> =	
	USCS=	AASHTO=	
<u>Classification</u>			
USCS=	AASHTO=		
<u>Remarks</u>			
Natural Moisture: 22.7%			
F.M.=1.67			

Sample Number: B-8

Depth: 23.5-25.0'

Date: 3.20.2020



**ECS SOUTHEAST, LLP**  
1812 Center Park Drive, Suite D  
Charlotte, NC 28217  
Phone: (704) 525-5152  
Fax: (704) 357-0023

**Client:** SCDDOT

**Project:** Emergency Bridge Package 2020-1 - York County

**Project No:** 14113

**Figure**

Tested By: CER



# Rock Coring Summary

PAGE 1 OF 1

PROJECT ID N/A

PROJECT NAME Emergency Bridge Package 2020-1

PROJECT COUNTY York

Borehole	Core Run Number	Core Run Top Depth	REC (%)	RQD (%)	q <sub>u</sub> (psi)	Poisson's Ratio	Secant Modulus (ksi)	Unit Weight (pcf)	RMR	GSI
B-6	HQ-1	65.0	78	57	9390	0.24	8699	199	57	55
B-6	HQ-2	70.0	100	90	7921	0.19	8677	183	60	55
B-6	HQ-3	75.0	100	100	3328	0.23	6845	173	64	45
B-7	HQ-1	78.0	12	0						

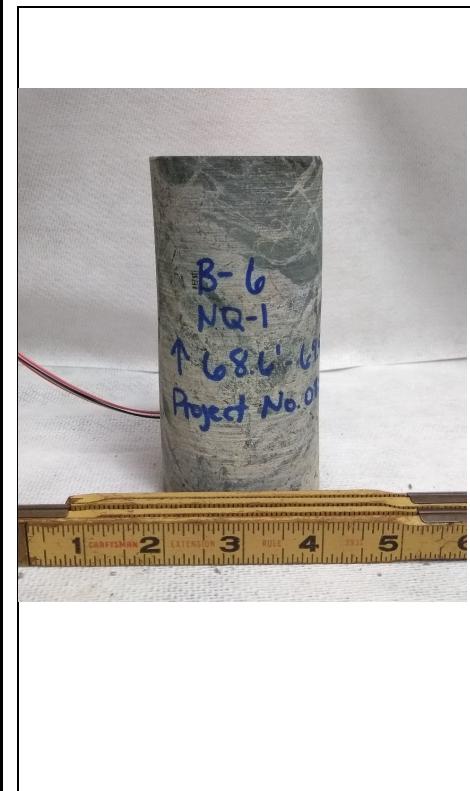
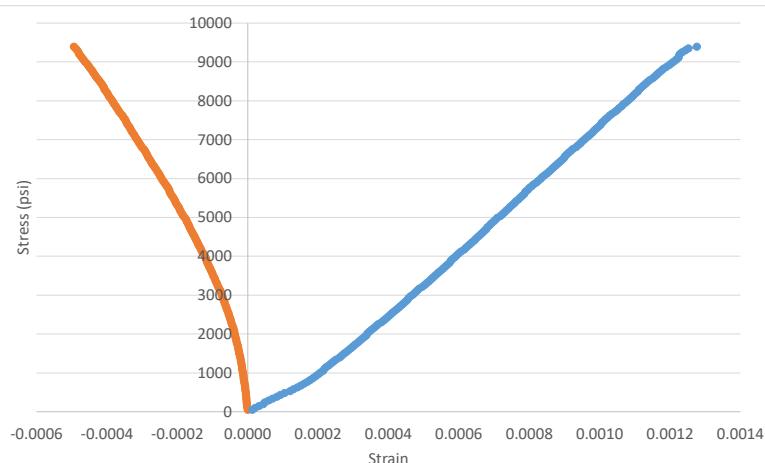


### Uniaxial Compressive Strength of Intact Rock Core Specimens

References:  
ASTM D7012-14 Method D

Project No.:	08:14113	Borehole:	B6
Project:	S-816 Bridge over Mud Creek	Sample No.:	HQ-1
Location:	York County, SC	Depth:	68.6-69.4 ft
Client:			
Date Received:	03/16/2020	Lab ID No.:	B6-HQ1
Date Tested:	03/19/2020		

Testing Results		Sample Measurements	
Max Load	45,728 lbs 203.4 kN	Diameter	2.490 in 6.32 cm
UCS	9391 psi 64.7 MPa	Height	5.273 in 13.39 cm
Elastic Modulus	8699 ksi 59.98 GPa	Area	4.870 in <sup>2</sup> 31.42 cm <sup>2</sup>
Loading Rate	14000 lbs/min 1.04 kN/s	Volume	25.679 in <sup>3</sup> 420.80 cm <sup>3</sup>
Lithology	Intermediate Metavolcanic Rock, gray, slightly weathered, strong rock	Mass	2.951 lbs 1338.55 g
Failure Mode	Vertical splitting	Bulk Density	198.58 lbs/ft <sup>3</sup> 3180.97 kg/m <sup>3</sup>
Poisson's Ratio	0.243		



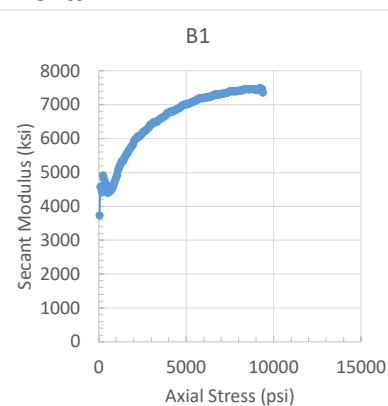
Before Test



After Test

### Comments

1. Sample was received trimmed and was cut to size and repolished
2. One vertical and one lateral strain gages were attached
3. Elastic Modulus and Poisson's ratio was calculated at about 50% failure load



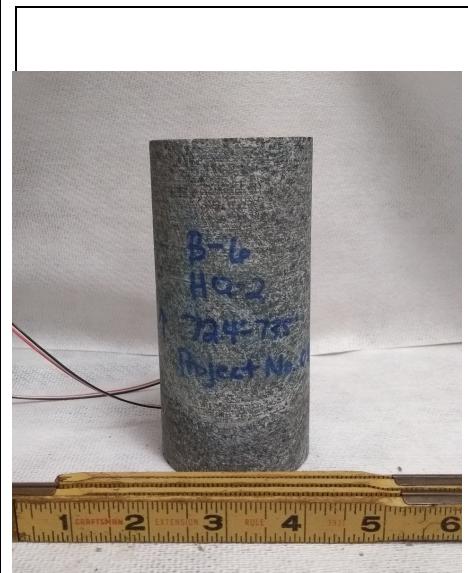
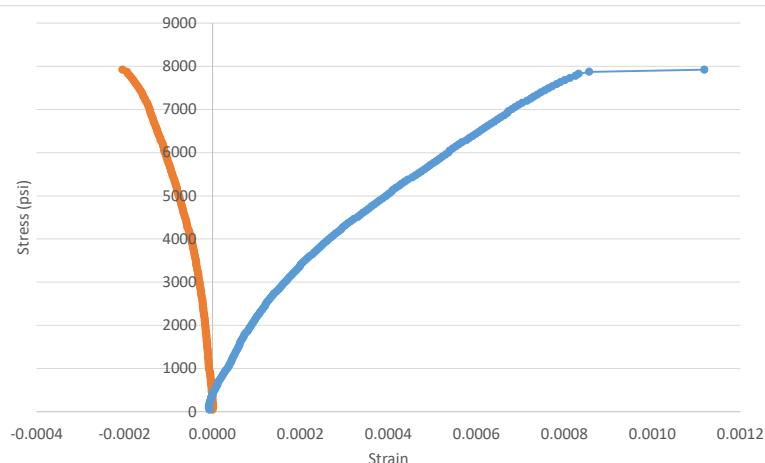


### Uniaxial Compressive Strength of Intact Rock Core Specimens

References:  
ASTM D7012-14 Method D

Project No.:	08:14113	Borehole:	B6
Project:	S-816 Bridge over Mud Creek	Sample No.:	HQ-2
Location:	York County, SC	Depth:	72.4-73.5 ft
Client:			
Date Received:	03/16/2020	Lab ID No.:	B6-HQ2
Date Tested:	03/19/2020		

Testing Results		Sample Measurements	
Max Load	38,490 lbs 171.2 kN	Diameter	2.487 in 6.32 cm
UCS	7921 psi 54.6 MPa	Height	5.297 in 13.46 cm
Elastic Modulus	8687 ksi 59.89 GPa	Area	4.859 in <sup>2</sup> 31.35 cm <sup>2</sup>
Loading Rate	14000 lbs/min 1.04 kN/s	Volume	25.740 in <sup>3</sup> 421.81 cm <sup>3</sup>
Lithology	Intermediate Metavolcanic Rock, gray, slightly weathered, strong rock	Mass	2.732 lbs 1239.21 g
Failure Mode	Vertical splitting	Bulk Density	183.40 lbs/ft <sup>3</sup> 2937.85 kg/m <sup>3</sup>
Poisson's Ratio	0.190		



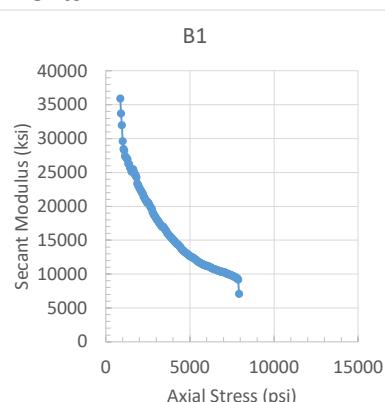
Before Test



After Test

### Comments

1. Sample was received trimmed and was cut to size and repolished
2. One vertical and one lateral strain gages were attached
3. Elastic Modulus and Poisson's ratio was calculated at about 50% failure load



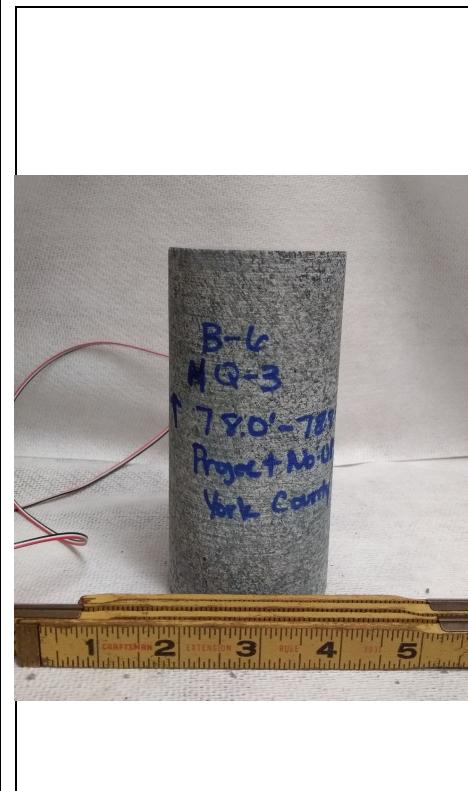
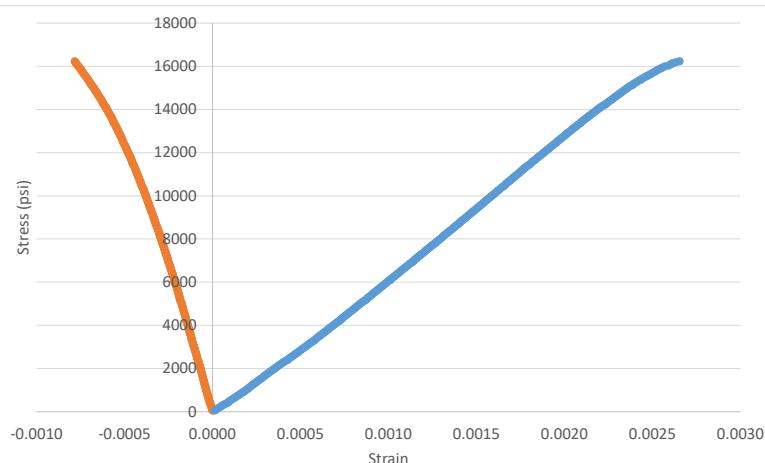


### Uniaxial Compressive Strength of Intact Rock Core Specimens

References:  
ASTM D7012-14 Method D

Project No.:	08:14113	Borehole:	B6
Project:	S-816 Bridge over Mud Creek	Sample No.:	HQ-3
Location:	York County, SC	Depth:	78.0-78.8 ft
Client:			
Date Received:	03/16/2020	Lab ID No.:	B6-HQ3
Date Tested:	03/19/2020		

Testing Results		Sample Measurements	
Max Load	79,122 lbs 352.0 kN	Diameter	2.492 in 6.33 cm
UCS	16227 psi 111.9 MPa	Height	5.286 in 13.43 cm
Elastic Modulus	6845 ksi 47.20 GPa	Area	4.876 in <sup>2</sup> 31.46 cm <sup>2</sup>
Loading Rate	14000 lbs/min 1.04 kN/s	Volume	25.775 in <sup>3</sup> 422.37 cm <sup>3</sup>
Lithology	Intermediate Metavolcanic Rock, gray, slightly weathered, strong rock	Mass	2.580 lbs 1170.27 g
Failure Mode	Diagonal shear plane(s)	Bulk Density	172.97 lbs/ft <sup>3</sup> 2770.68 kg/m <sup>3</sup>
Poisson's Ratio	0.228		

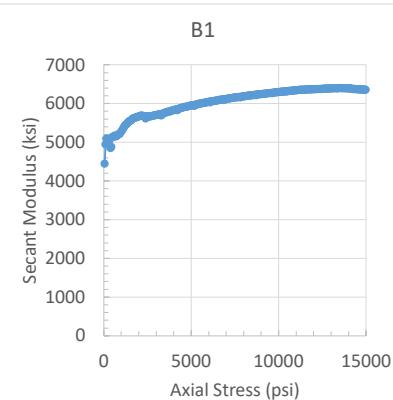


Before Test



After Test

Comments
<p>1. Sample was received trimmed and was cut to size and repolished 2. One vertical and one lateral strain gages were attached 3. Elastic Modulus and Poisson's ratio was calculated at about 50% failure load</p>



## **APPENDIX D – Supplemental Report Documents**

Hammer Calibration



# UNIVERSAL ENGINEERING SCIENCES

Consultants In: Geotechnical Engineering • Environmental Engineering • Construction Materials Testing •  
Threshold Inspection • Private Provider Inspection • Geophysical Studies

Offices In:

- Daytona Beach, FL
- Fort Myers, FL
- Fort Pierce, FL
- Gainesville, FL
- Jacksonville, FL
- Leesburg, FL
- Miami, FL
- Norcross, GA
- Ocala, FL
- Orlando, FL
- Palm Coast, FL
- Panama City, FL
- Pensacola, FL
- Rockledge, FL
- Sarasota, FL
- St. Augustine, FL
- Tampa, FL
- West Palm Beach, FL

Betts Environmental  
361 Airport Square  
Adel, Georgia 31620

April 18, 2019

Subject: **Dynamic Testing Report**  
**SPT Hammer Energy Measurement- CME-75 (S/N 164447)**  
156 N Johnson Street  
Newborn, Georgia 30056  
UES Project 0950.1900024.0000

UES has completed the high strain dynamic (i.e. PDA) testing for the Soil Test Boring drill rig designated CME-75 in use at the above referenced project. Dynamic monitoring was conducted during performance of a soil test boring in order to determine energy transferred by the Standard Penetration Test hammer to the drill rods during split spoon sampling. The dynamic testing was conducted using the Pile Driving Analyzer™ (PDA) Model 8G, which records, digitizes, and processes the force and acceleration signals. The dynamic testing was carried out in accordance with ASTM D4945 *Standard Test Method for High Strain Dynamic Testing of Piles* and ASTM D4633 *Standard Test Method for Energy Measurement for Dynamic Penetrometers*.

## PROJECT DESCRIPTION

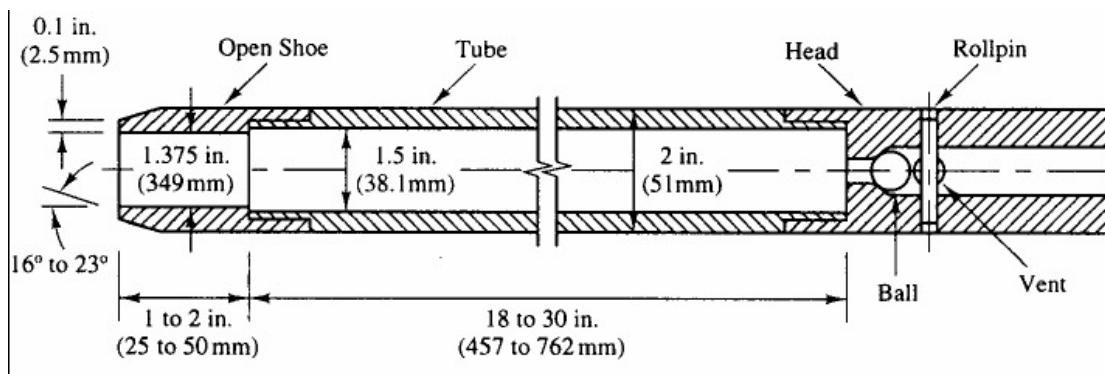
### Overview

The SPT hammer calibration testing was performed on site at the property located at 156 N Johnson Street in Newborn, Georgia. The SPT hammer calibration testing was performed at five (5) depths during sampling of an SPT Test Boring on April 12, 2019. The SPT hammer calibration testing was performed the following sampling depths; 33.5 to 35.0 feet (Sample 1), 38.5 to 40.0 feet (Sample 2), 43.5 to 45.0 feet (Sample 3), 48.5 to 50.0 feet (Sample 4), and 53.5 to 55.0 feet (Sample 5).

## SPT Testing Overview

Numerous technical publications exist regarding the Standard Penetration Test (SPT). Of these publications, ASTM D1586 *Standard Test Method for Penetration Test and Split-Barrel Sampling of Soils* is considered to be the industry standard. This standard was last approved in January, 1999. In addition, U.S. Army Corp of Engineers Engineering Technical Letter (ETL) 1110-1-138 (dated March, 1988) is also a commonly used standard reference.

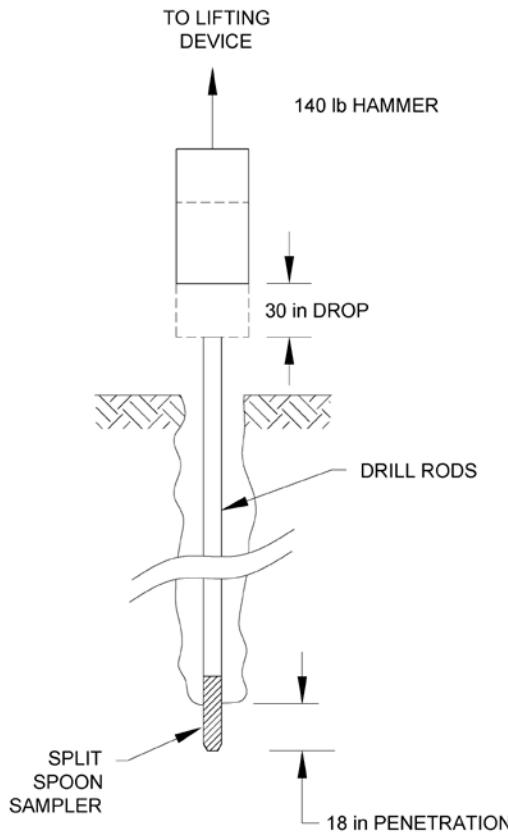
The Standard Penetration Test (SPT) consists of a drive weight assembly (i.e. hammer and anvil), split spoon sampler, and drill rods. The drive weight system consists of a 140 lb hammer raised by a number of mechanical means. The split spoon sampler is placed at the end of the drill rods in a borehole. The 140 lb hammer is raised 30 inches and then dropped to impact the drill rods. This procedure is repeated until the sampler has penetrated 18 inches into the underlying soil. The number of blows required to advance the split spoon sampler 12 inches is recorded as the "N" value for the test. Typically, the test is performed every 2 ½ ft for the upper 10 ft of a boring and then at 5 ft intervals thereafter. The standard dimensions of the split spoon sampler are shown in Figure 1, while a typical SPT setup is presented in Figure 2.



**Figure 1.** Split Spoon Sampler (after Rogers, 2004, adapted from ASTM D1586).

There are three (3) types of SPT hammers currently used in drilling practice today: the donut hammer, the automatic hammer, and the safety hammer. In addition, there are three (3) main types of hammer lifting mechanisms: cathead-rope system, spooling wench, or chain driven systems. Drill rods vary from AW (1 ¾ in O.D.) to NW (2 5/8 in O.D.), with drill rod lengths varying between 2 ft to 10 ft increments. Methods for advancing boreholes for the SPT test include mud rotary drilling, hollow stem augers, and water drilling with steel casing.





**Figure 2.** Typical SPT Setup.

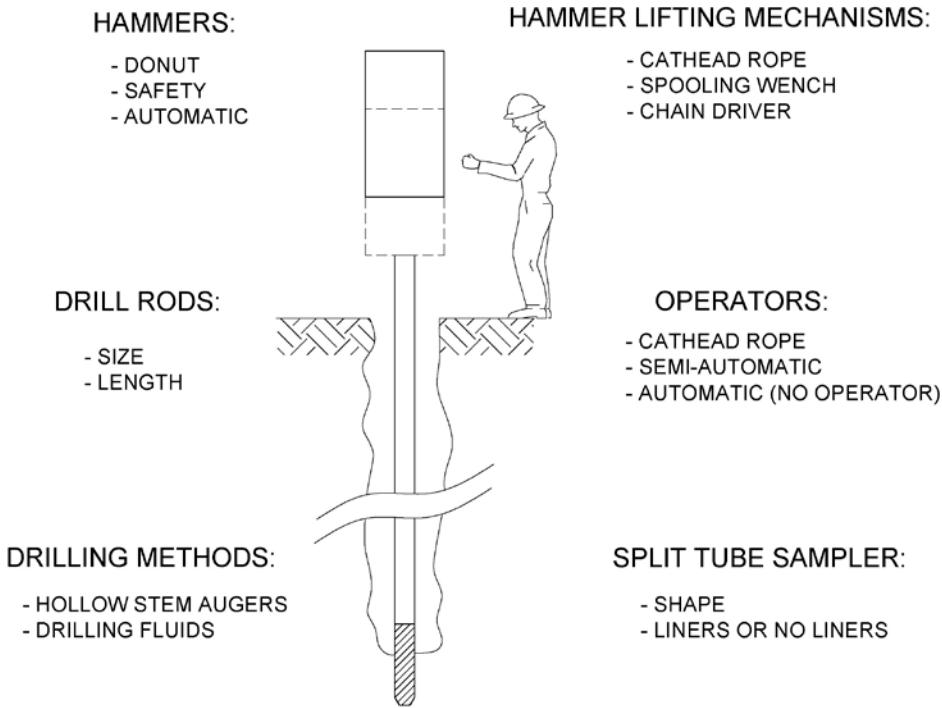
### SPT Energy Measurements

A number of factors can influence the SPT test and the subsequent N value. These include but are not limited to the following:

- Hammer
- Hammer Lifting System
- Operator Field Procedures
- Drill Rod Diameter and Length
- Borehole Drilling Method and Size
- Spilt Spoon Sampler

A graphical representation of various SPT system variables is provided in Figure 3.





**Figure 3.** SPT Testing System Variables (after Lamb, 1997).

In order to account for these system variables, standardized SPT corrections have been developed. The corrected blow count is referred to as the  $N_{60}$  value. The  $N_{60}$  value is derived from the assumed efficiency of the original SPT (Mohr) hammer (Rogers, 2004). The following equation defines  $N_{60}$  values:

$$N_{60} = C_{60} C_b C_s C_r N$$

Where:

$N_{60}$  = SPT N Value corrected for field procedures and apparatus

$C_{60}$  = Hammer Efficiency Correction

$C_b$  = Borehole Diameter Correction

$C_s$  = Sample Barrel Correction

$C_r$  = Rod Length Correction

$N$  = Raw SPT value

In addition, the  $N$  value is influenced by the overburden pressure. Laio and Whitman (1986) proposed the following overburden correction for  $N_{60}$ , termed  $(N_1)_{60}$ :

$$(N_1)_{60} = N_{60} \frac{\sqrt{2000 \text{ psf}}}{\sigma'_v}$$



Where:

$\sigma'_v$  = Effective vertical overburden stress

The hammer efficiency correction ( $C_{60}$ ) is based on the Energy Transfer Efficiency ( $ER_i$ ) and the 60% of the theoretical transferred hammer energy of 350 ft-lbs (i.e. 140 lbs multiplied by a 30 inch drop). The following equations show the derivation of  $C_{60}$ :

$$ER_i = \frac{E_i}{E_{th}}$$

Where:

$ER_i$  = Energy Transfer Efficiency

$E_i$  = Measured Transferred Energy

$E_{th}$  = Theoretical Transferred Energy (i.e. 350 ft-lb)

and

$$C_{60} = \frac{ER_i}{60\%}$$

For liquefaction analysis using SPT N values, transferred energy measurements are required to determine  $(N_1)_{60}$ . The methods for determining the normalized penetration resistance for liquefaction potential are presented in ASTM D6066 *Standard Practice for Determining the Normalized Penetration Resistance of Sands for Evaluation of Liquefaction Potential*.

Transferred (i.e. delivered) energy measurements of SPT testing (i.e. the energy delivered by the hammer to the drill rods) are commonly taken in engineering practice through the use of several types of instruments. The most common of these is the Pile Driving Analyzer (PDA), developed and marketed by Pile Dynamics Inc. of Cleveland, Ohio. The PDA is a computer fitted with a data acquisition and a signal conditioning system and is typically used to conduct high strain dynamic load testing of driven piles, which is analogous to the SPT test. Strain gages and accelerometers which are connected to the PDA are attached to the pile or drill rods (for SPT testing). During pile driving or SPT testing, the strain and acceleration signals are recorded and processed for each hammer blow. The strain signal is converted to a force record and the acceleration signal is converted to a velocity record. The PDA saves selected hammer blows containing this information to disk and determines the compressive stresses, displacement, and



energy at the point of measurement (pile top). The maximum transferred energy (EMX) is derived from the dynamic measurements using the following equation:

$$EMX = \int_b^a F(t)V(t)dt$$

Where:

a = Time Energy Transfer Begins

b = Time Energy Transfer End

F = Force

V = Velocity

t = Time

Refer to Abou-matar and Goble (1997) for additional details of SPT energy measurements using the PDA. Literature regarding the PDA is provided in the Appendix.

### **SPT Rig/Hammer System**

The tested drill rig is designated CME-75 and is manufactured by Central Mine Equipment, Inc. The drill rig was parked on existing grade in a grassy area for this project. We understand that the drill rig was built on October 29, 1984 and is identified with Serial Number 164447. The CME-75 drill rig is fitted with an automatically operated hammer system. The drill rig and SPT hammer were operated by Mr. Chris Golden.

The method of drilling for the rig during testing was hollow stem auger (HSA), with Standard Penetration Testing being performed with AWJ drill rods. AWJ drill rod sections have nominal outside diameter of 1-5/8 inches and wall thickness of 3/16 inches. The instrumented sub-assembly (i.e. where gauges were attached) consisted of a two feet long section of AWJ rod that was threaded into the top drill rod at each testing interval.

### **Dynamic Load Test Instrumentation**

The dynamic pile testing instrumentation consisted of a 2-feet long AWJ instrumented drill rod which is fitted with two strain gauges by Pile Dynamic Inc., in addition two (2) accelerometer transducers are attached a distance of approximately 1 foot below the top (i.e. in the center) of a two feet long instrumented AWJ drill rod. One strain gauge and one accelerometer are on opposite faces of the sub-assembly to minimize the effects of uneven hammer impact and rod bending.

A Model 8G Pile Driving Analyzer™ (PDA), manufactured by Pile Dynamics Inc., was used to collect the instrumentation data. The PDA is a computer fitted with a data acquisition and a



signal conditioning system. During driving, the strain and acceleration signals are recorded and processed for each hammer blow. The strain signal is converted to a force record and the acceleration signal is converted to a velocity record. The sampling frequency used during the SPT Energy Measurement Testing was 20,000 hertz (20 kHz). The PDA saves selected hammer blows containing this information to disk and determines the energy at the point of measurement.

## DYNAMIC TESTING RESULTS

### Hammer Performance

The transferred energy monitored during the sampling is summarized in Table 1. Note that the values are those recorded during the second and third 6-inch sampling interval at each depth. Hammer Efficiency is based on measured transferred energy divided by the energy generated with a 140 pound hammer dropping 30 inches (0.35 kip-ft).

**Table 1. CME-75 Rig SPT Energy Measurement Summary**

SPT 1 <b>Sample Depth (feet)</b>	<b>SPT Blow Count (Per 6 inch)</b>	<b>Hammer Efficiency (%)</b>			
		Min	Max	Average	Standard Deviation
33.5 to 35.0	3-4-4	73.70	75.96	75.02	0.71
38.5 to 40.0	5-12-14	70.58	74.11	72.25	0.92
43.5 to 45.0	5-12-21	70.22	74.76	71.98	1.13
48.5 to 50.0	8-12-25	71.29	74.62	72.84	0.80
53.5 to 55.0	20-22-29	70.49	74.32	72.31	0.78
<b>OVERALL<sup>1</sup>:</b>		71.26	74.75	<b>72.88</b>	0.87

The following figure shows the SPT rig tested.





**Figure 1:** SPT drill rig.



## CONCLUSIONS AND RECOMMENDATIONS

It is our opinion that the SPT hammer on the drill rig designated CME-75 is operating within a normal range for a semi-automatic SPT hammer.

UES appreciates the opportunity to provide this report. This report is for the sole use of this project and should not be relied upon otherwise. Should the project change significantly, we can review and modify our recommendations as needed. If you have questions concerning the contents herein, please contact us.

Sincerely,

UNIVERSAL ENGINEERING SCIENCES, INC.  
Universal Florida Certificate of Authorization No. 549

Joshua C. Adams  
Deep Foundation Engineer  
HSDPT Certified – Master Level



Attachments: PDA Data Output (PDIPILOT Graphs and Tables)



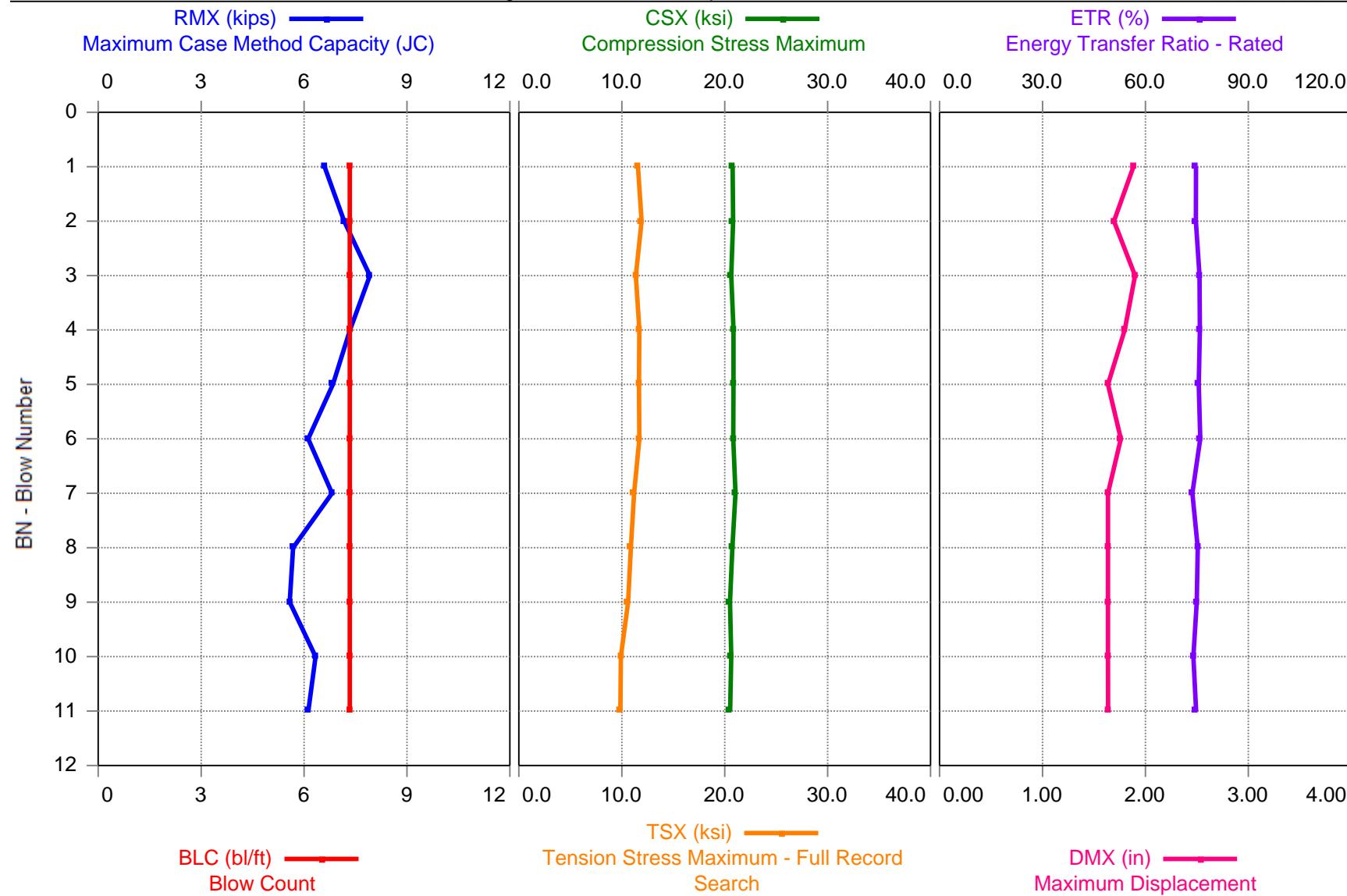
Printed: 18-April-2019

Universal Engineering Sciences, Inc. - PDIPILOT2 Ver 2017.2.58.3 - Case Method & iCAP® Results

Test started: 12-April-2019



Georgia SPT - SPT 2 Sample1



Georgia SPT - SPT 2 Sample1  
OP: NVT

Rod of area 1.18 square inches on CME 75  
Date: 12-April-2019

AR: 1.18 in<sup>2</sup>

SP: 0.492 k/ft<sup>3</sup>

LE: 44.00 ft

EM: 30,000 ksi

WS: 16,807.9 f/s

JC: 0.60

RMX: Maximum Case Method Capacity (JC)

CSB: Compression Stress at Bottom of Pile

CSX: Compression Stress Maximum

DMX: Maximum Displacement

TSX: Tension Stress Maximum - Full Record Search

SFR: Skin Friction (Crude Damping Correction)

STK: Hammer Stroke

ETR: Energy Transfer Ratio - Rated

CSI: Compression Stress Maximum - Individual Sensor

BL#	Depth ft	BLC bl/ft	RMX kips	CSX ksi	TSX ksi	STK ft	CSI ksi	CSB ksi	DMX in	SFR kips	ETR (%)
1	33.64	7	6.6	20.8	11.6	0.00	20.8	15.0	1.88	3	74.72
2	33.77	7	7.2	20.8	11.9	0.00	21.0	14.5	1.69	4	74.72
3	33.91	7	7.9	20.6	11.4	0.00	21.1	15.1	1.90	4	75.75
4	34.05	7	7.3	20.8	11.7	0.00	21.1	14.6	1.80	4	75.86
5	34.18	7	6.8	20.9	11.7	0.00	21.1	14.6	1.64	3	75.54
6	34.32	7	6.1	20.8	11.7	0.00	21.1	15.0	1.76	2	75.96
7	34.45	7	6.8	21.0	11.2	0.00	21.3	15.3	1.64	3	73.70
8	34.59	7	5.7	20.7	10.9	0.00	21.0	14.7	1.64	2	75.25
9	34.73	7	5.6	20.5	10.6	0.00	20.8	14.6	1.64	2	74.95
10	34.86	7	6.3	20.6	9.9	0.00	20.9	14.4	1.64	3	73.99
11	35.00	7	6.1	20.5	9.9	0.00	20.8	14.6	1.64	3	74.78
Average		6.6	20.7	11.1	**	21.0	14.8	1.71	3	75.02	
Std. Dev.		0.7	0.2	0.7	**	0.1	0.3	0.10	1	0.71	
Maximum		7.9	21.0	11.9	**	21.3	15.3	1.90	4	75.96	
Minimum		5.6	20.5	9.9	**	20.8	14.4	1.64	2	73.70	

Total number of blows analyzed: 11

BL# Sensors

1-11 F1: [357AWJ1] 212.0 (1.02); F4: [357AWJ2] 211.2 (1.02); A2: [55385] 915.0 (0.98);  
A3: [50148] 1065.0 (0.98)

BL# Comments

11 End of Set 1. n=10

Time Summary

Drive 13 seconds 1:46 PM - 1:46 PM BN 1 - 11

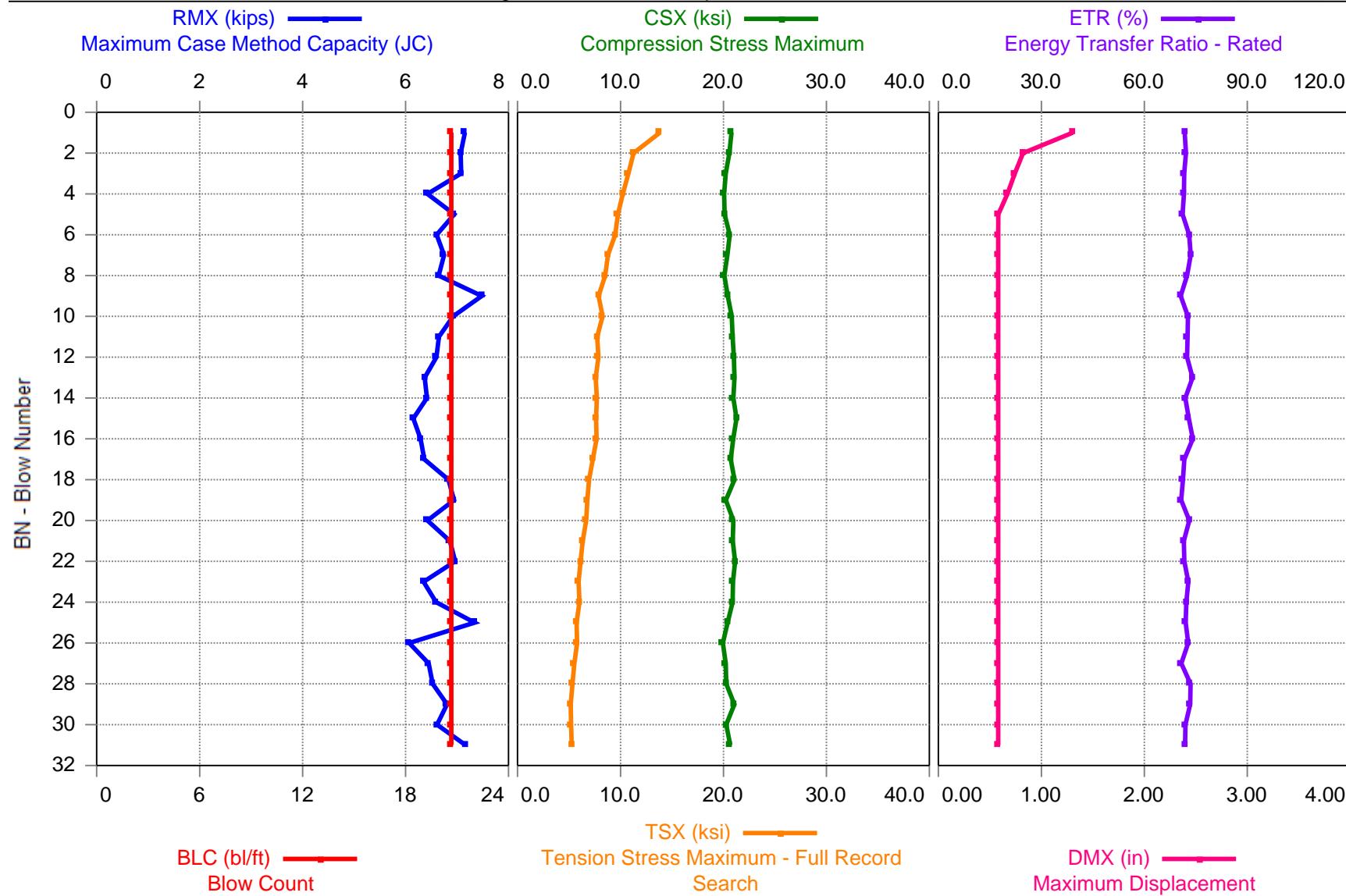
Printed: 18-April-2019

Universal Engineering Sciences, Inc. - PDIPILOT2 Ver 2017.2.58.3 - Case Method & iCAP® Results

Test started: 12-April-2019



Georgia SPT - SPT 2 Sample 2



Georgia SPT - SPT 2 Sample 2  
OP: NVT

Rod of area 1.18 square inches on CME 75  
Date: 12-April-2019

AR: 1.18 in<sup>2</sup>

SP: 0.492 k/ft<sup>3</sup>

LE: 50.00 ft

EM: 30,000 ksi

WS: 16,807.9 f/s

JC: 0.60

RMX: Maximum Case Method Capacity (JC)

CSB: Compression Stress at Bottom of Pile

CSX: Compression Stress Maximum

DMX: Maximum Displacement

TSX: Tension Stress Maximum - Full Record Search

SFR: Skin Friction (Crude Damping Correction)

STK: Hammer Stroke

ETR: Energy Transfer Ratio - Rated

CSI: Compression Stress Maximum - Individual Sensor

BL#	Depth ft	BLC bl/ft	RMX kips	CSX ksi	TSX ksi	STK ft	CSI ksi	CSB ksi	DMX in	SFR kips	ETR (%)
1	38.55	21	7.2	20.8	13.8	0.00	20.9	15.4	1.31	3	71.76
2	38.60	21	7.1	20.6	11.3	0.00	20.6	14.9	0.82	3	72.14
3	38.65	21	7.1	20.2	10.8	0.00	20.5	14.7	0.74	3	71.63
4	38.69	21	6.4	20.1	10.2	0.00	20.3	14.2	0.67	3	71.53
5	38.74	21	6.9	20.1	9.8	0.00	20.3	14.5	0.58	3	71.16
6	38.79	21	6.6	20.6	9.5	0.00	20.9	14.4	0.58	3	73.06
7	38.84	21	6.7	20.4	8.8	0.00	20.4	14.7	0.58	3	73.52
8	38.89	21	6.6	20.1	8.5	0.00	20.1	13.9	0.58	3	72.45
9	38.94	21	7.5	20.4	7.9	0.00	20.4	14.3	0.58	3	70.58
10	38.98	21	6.9	20.8	8.3	0.00	21.0	14.9	0.58	3	72.72
11	39.03	21	6.6	20.9	7.7	0.00	21.0	14.7	0.58	3	72.58
12	39.08	21	6.6	21.0	7.9	0.00	21.2	14.8	0.58	3	72.44
13	39.13	21	6.4	21.1	7.6	0.00	21.1	14.7	0.58	3	74.07
14	39.18	21	6.4	21.0	7.7	0.00	21.2	14.4	0.58	3	71.92
15	39.23	21	6.1	21.3	7.6	0.00	21.3	14.8	0.58	3	72.94
16	39.27	21	6.3	20.9	7.7	0.00	21.2	15.0	0.58	2	74.11
17	39.32	21	6.4	20.7	7.3	0.00	20.8	14.4	0.58	3	71.63
18	39.37	21	6.8	21.1	6.9	0.00	21.1	15.2	0.58	3	71.24
19	39.42	21	6.9	20.2	6.8	0.00	20.4	14.9	0.58	3	70.74
20	39.47	21	6.4	21.0	6.7	0.00	21.0	15.1	0.58	3	73.12
21	39.52	21	6.9	20.9	6.3	0.00	21.0	15.2	0.58	3	71.50
22	39.56	21	7.0	21.1	6.1	0.00	21.3	15.1	0.58	3	71.65
23	39.61	21	6.3	20.9	5.9	0.00	21.0	15.0	0.58	3	72.81
24	39.66	21	6.6	20.9	6.0	0.00	21.0	15.0	0.58	3	72.22
25	39.71	21	7.3	20.4	5.7	0.00	20.7	14.9	0.58	3	72.04
26	39.76	21	6.1	19.9	5.8	0.00	20.0	14.2	0.58	2	72.76
27	39.81	21	6.4	20.2	5.5	0.00	20.5	14.8	0.58	3	70.77
28	39.85	21	6.5	20.3	5.3	0.00	20.5	14.7	0.58	3	73.48
29	39.90	21	6.8	21.1	5.2	0.00	21.3	15.2	0.58	3	73.35
30	39.95	21	6.6	20.3	5.2	0.00	20.6	14.3	0.58	3	71.99
31	40.00	21	7.2	20.7	5.3	0.00	20.9	15.1	0.58	3	71.85
Average			6.7	20.6	7.6	**	20.8	14.8	0.62	3	72.25
Std. Dev.			0.3	0.4	2.0	**	0.4	0.4	0.14	0	0.92
Maximum			7.5	21.3	13.8	**	21.3	15.4	1.31	3	74.11
Minimum			6.1	19.9	5.2	**	20.0	13.9	0.58	2	70.58

Total number of blows analyzed: 31

BL# Sensors

1-31 F1: [357AWJ1] 212.0 (1.12); F4: [357AWJ2] 211.2 (1.12); A2: [55385] 915.0 (0.88);  
A3: [50148] 1065.0 (0.88)

Georgia SPT - SPT 2 Sample 2  
OP: NVT

Rod of area 1.18 square inches on CME 75  
Date: 12-April-2019

BL# Comments

31 end of set 2. N=28

Time Summary

Drive 41 seconds 1:56 PM - 1:56 PM BN 1 - 31

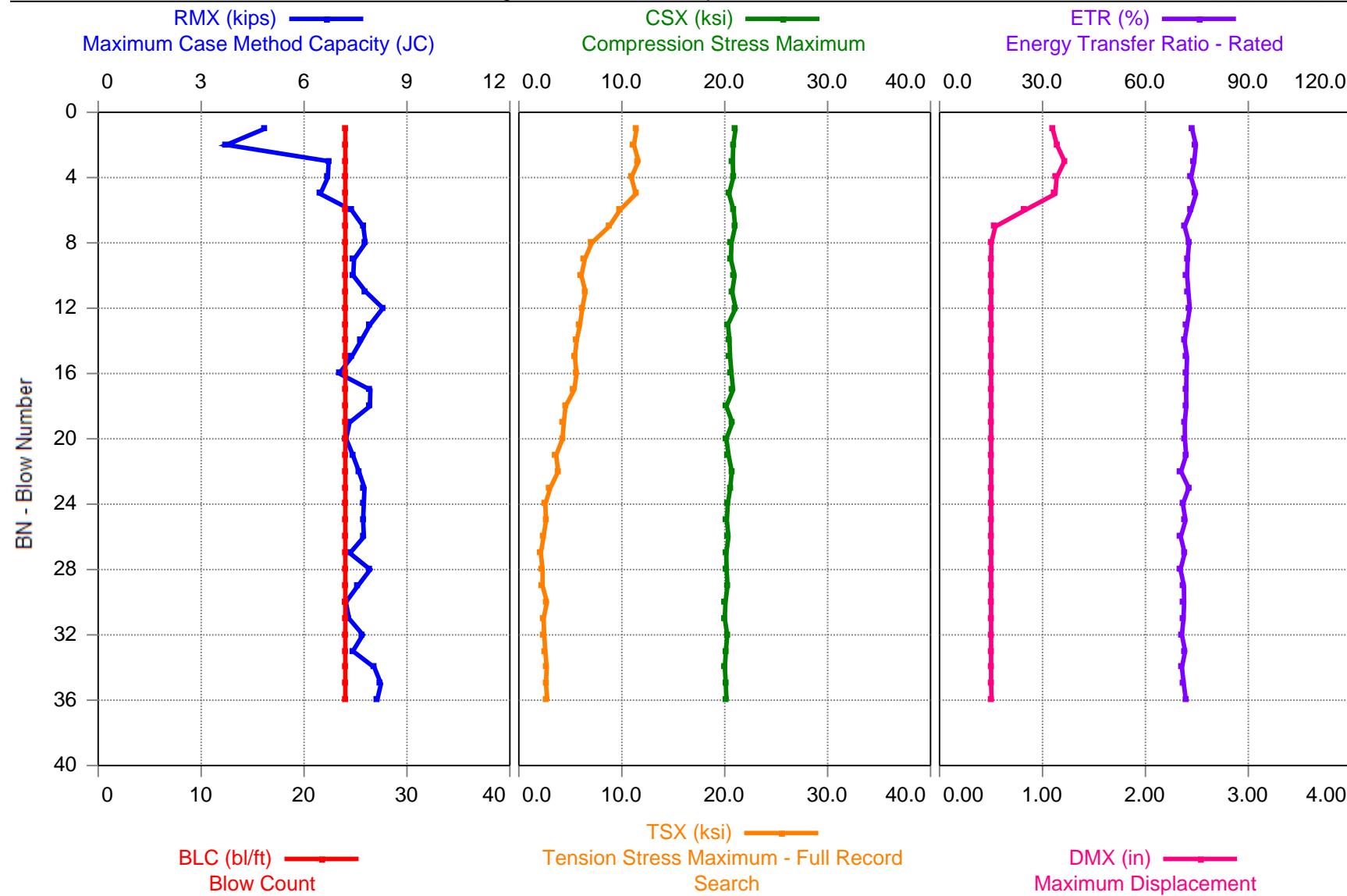
Printed: 18-April-2019

Universal Engineering Sciences, Inc. - PDIPILOT2 Ver 2017.2.58.3 - Case Method & iCAP® Results

Test started: 12-April-2019



Georgia SPT - SPT 2 Sample 3



Georgia SPT - SPT 2 Sample 3  
OP: NVT

Rod of area 1.18 square inches on CME 75  
Date: 12-April-2019

AR: 1.18 in<sup>2</sup>

SP: 0.492 k/ft<sup>3</sup>

LE: 55.00 ft

EM: 30,000 ksi

WS: 16,807.9 f/s

JC: 0.60

RMX: Maximum Case Method Capacity (JC)

CSB: Compression Stress at Bottom of Pile

CSX: Compression Stress Maximum

DMX: Maximum Displacement

TSX: Tension Stress Maximum - Full Record Search

SFR: Skin Friction (Crude Damping Correction)

STK: Hammer Stroke

ETR: Energy Transfer Ratio - Rated

CSI: Compression Stress Maximum - Individual Sensor

BL#	Depth ft	BLC bl/ft	RMX kips	CSX ksi	TSX ksi	STK ft	CSI ksi	CSB ksi	DMX in	SFR kips	ETR (%)
1	43.54	24	4.9	21.1	11.4	0.00	21.6	13.3	1.10	3	73.56
2	43.58	24	3.7	20.8	11.2	0.00	21.3	12.7	1.14	2	74.69
3	43.63	24	6.7	20.8	11.6	0.00	21.2	14.4	1.21	3	74.22
4	43.67	24	6.7	20.8	10.9	0.00	21.4	13.9	1.14	4	73.33
5	43.71	24	6.5	20.4	11.4	0.00	20.9	13.8	1.12	3	74.76
6	43.75	24	7.4	20.9	9.8	0.00	21.5	14.5	0.83	4	73.27
7	43.79	24	7.7	21.0	8.8	0.00	21.6	14.4	0.54	4	71.45
8	43.83	24	7.8	20.7	7.1	0.00	21.3	14.5	0.50	4	72.71
9	43.88	24	7.5	20.6	6.4	0.00	21.2	14.7	0.50	3	72.31
10	43.92	24	7.4	21.0	6.1	0.00	21.6	14.8	0.50	3	72.14
11	43.96	24	7.8	20.7	6.5	0.00	21.4	14.8	0.50	4	72.51
12	44.00	24	8.3	21.1	6.2	0.00	21.9	15.1	0.50	4	72.92
13	44.04	24	7.9	20.3	5.9	0.00	20.8	14.8	0.50	4	72.14
14	44.08	24	7.7	20.5	5.6	0.00	21.2	14.6	0.50	4	71.40
15	44.13	24	7.4	20.5	5.4	0.00	21.3	14.9	0.50	3	72.12
16	44.17	24	7.0	20.7	5.6	0.00	21.4	14.6	0.50	3	71.96
17	44.21	24	7.9	20.8	5.4	0.00	21.5	15.1	0.50	4	71.86
18	44.25	24	7.9	20.2	4.5	0.00	20.7	14.4	0.50	4	71.91
19	44.29	24	7.3	20.7	4.4	0.00	21.5	14.2	0.50	4	71.45
20	44.33	24	7.2	20.2	4.2	0.00	20.7	14.2	0.50	3	71.52
21	44.38	24	7.4	20.4	3.6	0.00	21.1	14.4	0.50	4	71.86
22	44.42	24	7.6	20.7	3.8	0.00	21.3	14.4	0.50	4	70.36
23	44.46	24	7.8	20.5	3.0	0.00	21.4	14.7	0.50	4	72.62
24	44.50	24	7.7	20.3	2.6	0.00	20.9	14.1	0.50	4	70.92
25	44.54	24	7.7	20.2	2.6	0.00	20.8	13.9	0.50	4	71.70
26	44.58	24	7.7	20.4	2.4	0.00	21.1	14.3	0.50	4	70.31
27	44.63	24	7.3	20.1	2.1	0.00	20.8	14.0	0.50	4	71.44
28	44.67	24	7.9	20.2	2.3	0.00	20.7	14.0	0.50	4	70.22
29	44.71	24	7.6	20.3	2.3	0.00	20.9	14.2	0.50	4	71.23
30	44.75	24	7.2	20.1	2.7	0.00	20.7	14.1	0.50	4	71.27
31	44.79	24	7.3	20.0	2.4	0.00	20.6	13.8	0.50	4	71.10
32	44.83	24	7.7	20.2	2.5	0.00	20.8	14.3	0.50	4	70.64
33	44.88	24	7.4	20.1	2.6	0.00	20.7	13.8	0.50	4	71.58
34	44.92	24	8.0	20.0	2.7	0.00	20.5	14.0	0.50	4	70.62
35	44.96	24	8.2	20.1	2.6	0.00	20.7	14.2	0.50	4	71.18
36	45.00	24	8.1	20.2	2.8	0.00	20.6	14.3	0.51	4	71.80
Average		7.4	20.5	5.3	**	21.1	14.3	0.60	4	71.98	
Std. Dev.		0.9	0.3	3.1	**	0.4	0.5	0.23	0	1.13	
Maximum		8.3	21.1	11.6	**	21.9	15.1	1.21	4	74.76	
Minimum		3.7	20.0	2.1	**	20.5	12.7	0.50	2	70.22	

Total number of blows analyzed: 36

Georgia SPT - SPT 2 Sample 3  
OP: NVT

Rod of area 1.18 square inches on CME 75  
Date: 12-April-2019

BL# Sensors

1-36 F1: [357AWJ1] 212.0 (1.12); F4: [357AWJ2] 211.2 (1.12); A2: [55385] 915.0 (0.88);  
A3: [50148] 1065.0 (0.88)

BL# Comments

36 End of Set 3. n=33

Time Summary

Drive 49 seconds 2:14 PM - 2:14 PM BN 1 - 36

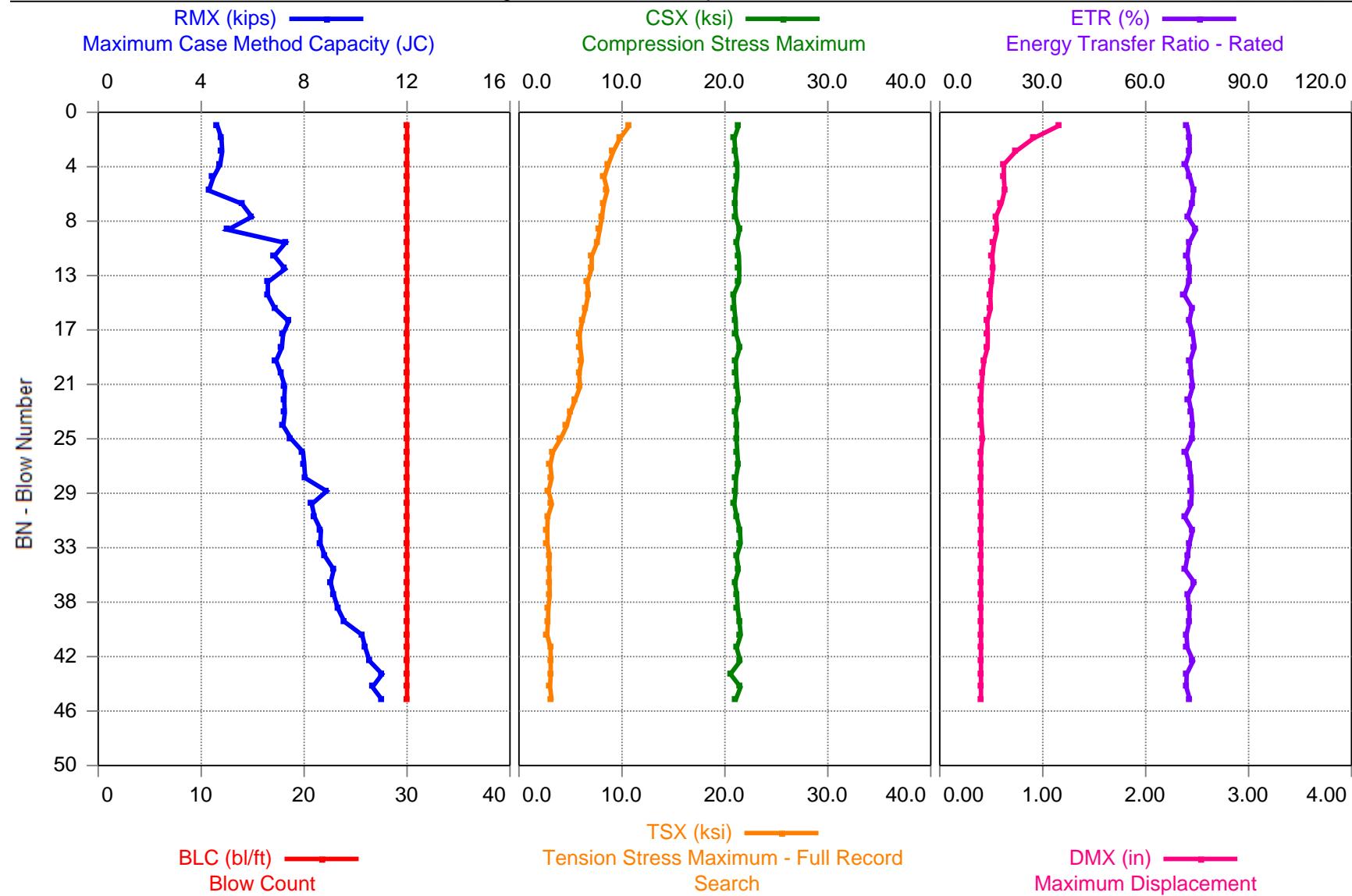
Printed: 18-April-2019

Universal Engineering Sciences, Inc. - PDIPILOT2 Ver 2017.2.58.3 - Case Method & iCAP® Results

Test started: 12-April-2019



Georgia SPT - SPT 2 Sample 4



Georgia SPT - SPT 2 Sample 4  
OP: NVT

Rod of area 1.18 square inches on CME 75  
Date: 12-April-2019

AR: 1.18 in<sup>2</sup>

SP: 0.492 k/ft<sup>3</sup>

LE: 55.00 ft

EM: 30,000 ksi

WS: 16,807.9 f/s

JC: 0.60

RMX: Maximum Case Method Capacity (JC)

CSB: Compression Stress at Bottom of Pile

CSX: Compression Stress Maximum

DMX: Maximum Displacement

TSX: Tension Stress Maximum - Full Record Search

SFR: Skin Friction (Crude Damping Correction)

STK: Hammer Stroke

ETR: Energy Transfer Ratio - Rated

CSI: Compression Stress Maximum - Individual Sensor

BL#	Depth ft	BLC bl/ft	RMX kips	CSX ksi	TSX ksi	STK ft	CSI ksi	CSB ksi	DMX in	SFR kips	ETR (%)
1	48.53	30	4.6	21.3	10.7	0.00	21.5	15.0	1.17	1	72.09
2	48.57	30	4.8	20.9	9.8	0.00	21.1	13.1	0.91	2	72.78
3	48.60	30	4.8	21.0	9.2	0.00	21.0	13.8	0.74	2	72.83
4	48.63	30	4.7	21.2	8.7	0.00	21.2	14.1	0.62	2	71.63
5	48.67	30	4.5	21.2	8.3	0.00	21.2	14.6	0.62	1	72.96
6	48.70	30	4.3	21.0	8.6	0.00	21.1	14.3	0.63	2	73.93
7	48.73	30	5.6	21.0	8.2	0.00	21.0	15.0	0.60	2	73.49
8	48.77	30	6.0	21.1	8.0	0.00	21.1	15.2	0.54	2	72.26
9	48.80	30	5.0	21.4	7.8	0.00	21.5	14.4	0.56	2	74.62
10	48.83	30	7.3	21.1	7.6	0.00	21.2	15.6	0.53	3	72.65
11	48.87	30	6.8	21.4	7.1	0.00	21.4	15.6	0.51	3	72.17
12	48.90	30	7.3	21.4	7.0	0.00	21.5	15.8	0.52	3	72.82
13	48.93	30	6.6	21.4	6.6	0.00	21.5	15.5	0.50	2	72.61
14	48.97	30	6.6	20.8	6.7	0.00	20.9	15.4	0.49	2	71.29
15	49.00	30	6.9	20.9	6.5	0.00	21.0	15.8	0.50	2	73.55
16	49.03	30	7.4	21.0	6.1	0.00	21.1	15.7	0.46	3	72.67
17	49.07	30	7.2	21.1	5.9	0.00	21.2	15.9	0.47	3	73.71
18	49.10	30	7.1	21.5	6.0	0.00	21.7	15.8	0.46	3	74.24
19	49.13	30	6.9	21.1	6.1	0.00	21.1	15.3	0.43	2	73.00
20	49.17	30	7.1	21.1	5.8	0.00	21.1	15.9	0.41	2	73.21
21	49.20	30	7.3	21.2	5.9	0.00	21.3	16.0	0.41	2	73.71
22	49.23	30	7.2	21.3	5.5	0.00	21.5	15.9	0.40	2	72.58
23	49.27	30	7.2	21.0	5.0	0.00	21.1	15.9	0.40	2	73.35
24	49.30	30	7.2	21.2	4.6	0.00	21.2	16.1	0.41	2	73.66
25	49.33	30	7.5	21.1	4.0	0.00	21.1	15.8	0.42	3	73.49
26	49.37	30	8.0	21.2	3.3	0.00	21.4	14.8	0.40	3	71.73
27	49.40	30	8.0	21.3	3.0	0.00	21.4	15.8	0.40	3	72.73
28	49.43	30	8.0	21.1	3.2	0.00	21.1	15.8	0.40	3	73.24
29	49.47	30	8.9	21.0	2.9	0.00	21.1	16.0	0.40	3	73.44
30	49.50	30	8.3	20.9	3.2	0.00	21.0	15.8	0.40	3	73.26
31	49.53	30	8.4	21.2	2.8	0.00	21.2	15.5	0.40	3	71.45
32	49.57	30	8.7	21.5	2.8	0.00	21.7	15.7	0.40	3	73.66
33	49.60	30	8.6	21.5	2.8	0.00	21.8	16.2	0.40	3	72.79
34	49.63	30	8.8	21.1	3.0	0.00	21.3	15.8	0.40	3	72.19
35	49.67	30	9.2	21.3	2.9	0.00	21.6	15.2	0.40	4	71.50
36	49.70	30	9.0	21.0	3.0	0.00	21.2	15.9	0.40	3	74.18
37	49.73	30	9.2	21.2	3.0	0.00	21.2	15.7	0.40	3	72.21
38	49.77	30	9.3	21.2	2.9	0.00	21.4	15.9	0.40	4	72.74
39	49.80	30	9.6	21.4	2.8	0.00	21.6	15.9	0.40	4	72.69
40	49.83	30	10.3	21.5	2.7	0.00	21.8	15.9	0.40	4	71.86
41	49.87	30	10.4	21.1	3.1	0.00	21.3	16.2	0.40	4	72.14
42	49.90	30	10.5	21.5	3.1	0.00	21.7	15.8	0.40	4	73.82
43	49.93	30	11.0	20.5	3.1	0.00	20.6	15.9	0.40	4	71.92
44	49.97	30	10.7	21.5	3.0	0.00	21.6	16.4	0.40	4	71.82
45	50.00	30	11.0	21.0	3.2	0.00	21.1	15.8	0.40	4	72.92

Georgia SPT - SPT 2 Sample 4  
OP: NVT

Rod of area 1.18 square inches on CME 75  
Date: 12-April-2019

BL#	Depth ft	BLC bl/ft	RMX kips	CSX ksi	TSX ksi	STK ft	CSI ksi	CSB ksi	DMX in	SFR kips	ETR (%)
	Average		7.6	21.2	5.2	**	21.3	15.5	0.48	3	72.84
	Std. Dev.		1.8	0.2	2.3	**	0.3	0.7	0.15	1	0.80
	Maximum		11.0	21.5	10.7	**	21.8	16.4	1.17	4	74.62
	Minimum		4.3	20.5	2.7	**	20.6	13.1	0.40	1	71.29

Total number of blows analyzed: 45

BL# Sensors

1-45 F1: [357AWJ1] 212.0 (1.12); F4: [357AWJ2] 211.2 (1.12); A2: [55385] 915.0 (0.88);  
A3: [50148] 1065.0 (0.88)

BL# Comments

45 end of set 4. n=39

Time Summary

Drive 1 minute 2 seconds 2:27 PM - 2:28 PM BN 1 - 45

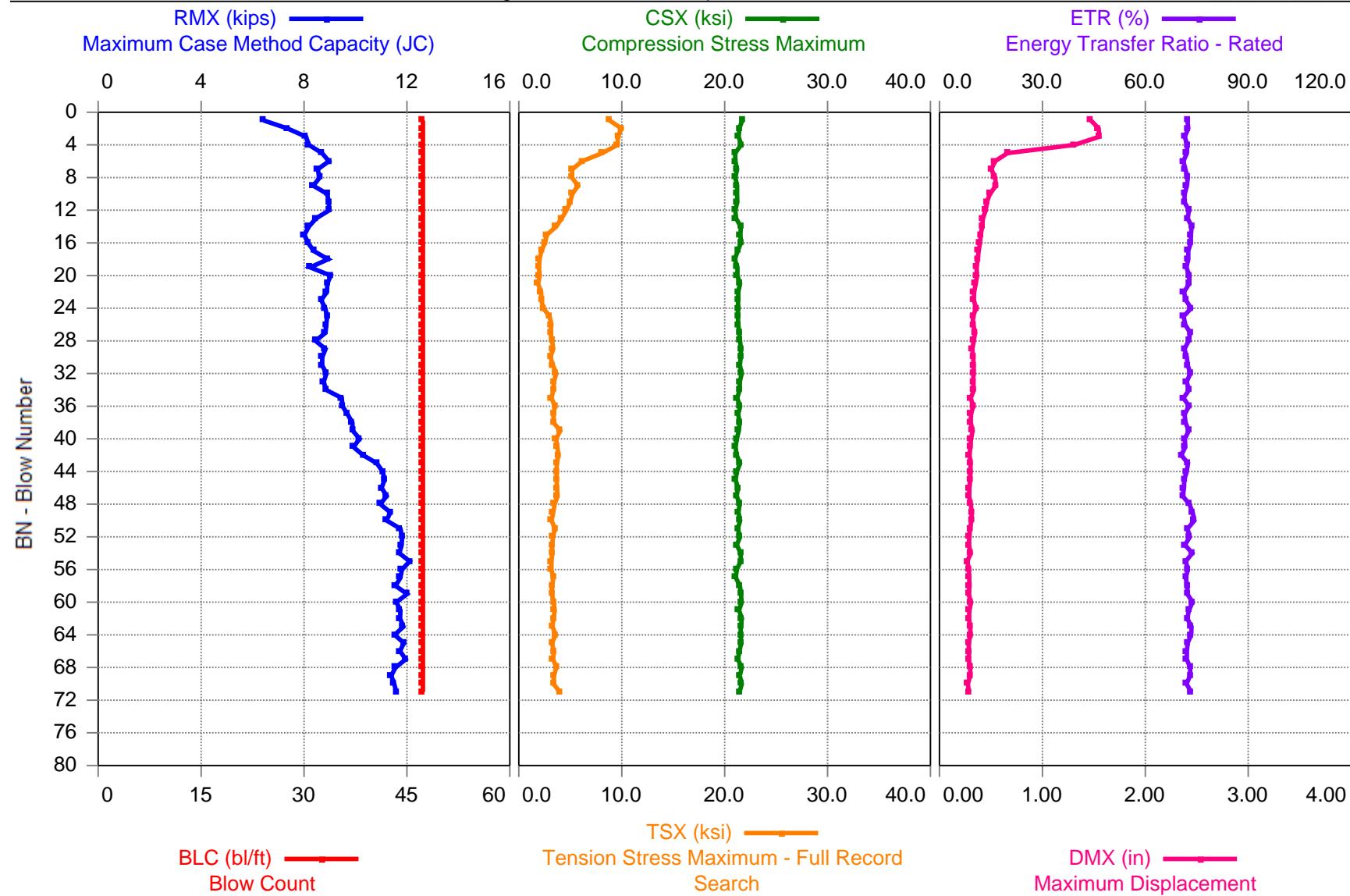
Printed: 18-April-2019

Universal Engineering Sciences, Inc. - PDIPILOT2 Ver 2017.2.58.3 - Case Method & iCAP® Results

Test started: 12-April-2019



Georgia SPT - SPT 2 Sample 5



Georgia SPT - SPT 2 Sample 5  
OP: NVT

Rod of area 1.18 square inches on CME 75  
Date: 12-April-2019

AR: 1.18 in<sup>2</sup>

SP: 0.492 k/ft<sup>3</sup>

LE: 60.00 ft

EM: 30,000 ksi

WS: 16,807.9 f/s

JC: 0.60

RMX: Maximum Case Method Capacity (JC)

CSB: Compression Stress at Bottom of Pile

CSX: Compression Stress Maximum

DMX: Maximum Displacement

TSX: Tension Stress Maximum - Full Record Search

SFR: Skin Friction (Crude Damping Correction)

STK: Hammer Stroke

ETR: Energy Transfer Ratio - Rated

CSI: Compression Stress Maximum - Individual Sensor

BL#	Depth ft	BLC bl/ft	RMX kips	CSX ksi	TSX ksi	STK ft	CSI ft	CSB ksi	DMX in	SFR kips	ETR (%)
1	53.52	47	6.4	21.7	8.8	0.00	21.8	17.7	1.47	1	72.27
2	53.54	47	7.4	21.4	10.0	0.00	21.5	15.4	1.55	3	72.51
3	53.56	47	8.1	21.4	9.6	0.00	21.4	15.5	1.55	4	71.52
4	53.58	47	8.2	21.6	9.6	0.00	21.6	16.4	1.31	3	72.20
5	53.61	47	8.7	21.0	8.1	0.00	21.2	15.8	0.66	4	72.13
6	53.63	47	9.0	21.0	6.1	0.00	21.2	16.1	0.54	3	71.12
7	53.65	47	8.5	21.2	5.2	0.00	21.3	16.4	0.50	3	71.64
8	53.67	47	8.6	21.0	5.2	0.00	21.2	16.6	0.54	3	72.37
9	53.69	47	8.4	21.2	5.7	0.00	21.4	16.1	0.55	3	72.11
10	53.71	47	8.9	21.2	5.2	0.00	21.3	16.7	0.49	3	71.46
11	53.73	47	9.0	21.2	5.0	0.00	21.5	16.8	0.46	3	71.39
12	53.75	47	9.0	21.0	4.6	0.00	21.2	16.7	0.45	3	72.71
13	53.77	47	8.5	21.1	4.2	0.00	21.2	16.0	0.42	3	72.38
14	53.80	47	8.2	21.6	3.6	0.00	21.6	16.8	0.42	3	73.49
15	53.82	47	8.0	21.5	2.7	0.00	21.6	16.6	0.40	3	73.30
16	53.84	47	8.2	21.6	2.5	0.00	21.6	16.6	0.39	3	73.22
17	53.86	47	8.4	21.3	2.2	0.00	21.3	16.0	0.38	3	72.54
18	53.88	47	8.9	21.0	2.0	0.00	21.1	16.8	0.37	3	72.52
19	53.90	47	8.2	21.2	2.0	0.00	21.3	16.6	0.36	3	71.99
20	53.92	47	9.0	21.2	2.0	0.00	21.5	16.7	0.36	3	72.82
21	53.94	47	8.9	21.5	1.9	0.00	21.7	16.7	0.35	3	72.80
22	53.96	47	8.9	21.3	2.2	0.00	21.6	16.5	0.34	3	71.30
23	53.99	47	8.7	21.3	2.2	0.00	21.4	16.5	0.33	3	71.79
24	54.01	47	8.8	21.3	2.4	0.00	21.4	16.4	0.36	3	73.37
25	54.03	47	8.9	21.3	3.0	0.00	21.4	16.8	0.32	3	71.17
26	54.05	47	8.9	21.3	3.2	0.00	21.5	16.6	0.33	3	71.61
27	54.07	47	8.8	21.4	3.1	0.00	21.4	17.5	0.35	2	73.06
28	54.09	47	8.5	21.5	3.2	0.00	21.5	16.7	0.33	3	72.63
29	54.11	47	8.8	21.6	3.3	0.00	21.7	16.8	0.32	3	71.40
30	54.13	47	8.7	21.6	3.1	0.00	21.8	16.6	0.33	3	72.10
31	54.15	47	8.7	21.5	3.3	0.00	21.7	16.9	0.33	3	72.38
32	54.18	47	8.9	21.7	3.6	0.00	21.8	17.1	0.33	3	73.15
33	54.20	47	8.8	21.5	3.4	0.00	21.6	17.1	0.33	3	72.04
34	54.22	47	8.9	21.5	3.3	0.00	21.6	16.8	0.33	3	72.75
35	54.24	47	9.5	21.2	3.2	0.00	21.5	16.8	0.30	3	71.13
36	54.26	47	9.5	21.5	3.5	0.00	21.6	17.0	0.33	3	72.73
37	54.28	47	9.7	21.3	3.4	0.00	21.5	16.8	0.31	3	71.44
38	54.30	47	9.9	21.5	3.4	0.00	21.7	16.4	0.30	4	71.71
39	54.32	47	9.9	21.4	4.0	0.00	21.4	17.0	0.32	3	72.68
40	54.35	47	10.2	21.2	3.6	0.00	21.3	16.6	0.31	4	71.51
41	54.37	47	9.9	21.1	3.7	0.00	21.2	16.6	0.30	4	71.63
42	54.39	47	10.3	21.2	3.8	0.00	21.3	16.5	0.29	4	70.49
43	54.41	47	10.8	21.5	3.7	0.00	21.7	16.6	0.30	4	72.44
44	54.43	47	11.1	21.2	3.7	0.00	21.2	16.5	0.30	4	72.04
45	54.45	47	11.1	21.1	3.7	0.00	21.2	16.6	0.30	4	71.36

Georgia SPT - SPT 2 Sample 5							Rod of area 1.18 square inches on CME 75				
BL#	Depth	BLC	RMX	CSX	TSX	STK	CSI	CSB	DMX	SFR	ETR
	ft	bl/ft	kips	ksi	ksi	ft	ksi	ksi	in	kips	(%)
46	54.47	47	11.0	21.3	3.7	0.00	21.5	16.5	0.29	4	71.27
47	54.49	47	11.2	21.2	3.8	0.00	21.3	16.3	0.29	4	70.87
48	54.51	47	11.0	21.5	3.5	0.00	21.6	16.6	0.30	4	72.83
49	54.54	47	11.4	21.3	3.3	0.00	21.4	16.7	0.31	4	73.80
50	54.56	47	11.2	21.5	3.2	0.00	21.7	16.9	0.31	4	74.32
51	54.58	47	11.7	21.3	3.5	0.00	21.3	16.3	0.30	4	72.31
52	54.60	47	11.8	21.5	3.3	0.00	21.7	16.5	0.29	5	72.94
53	54.62	47	11.8	21.2	3.2	0.00	21.3	16.7	0.28	4	71.57
54	54.64	47	11.7	21.6	3.2	0.00	21.6	16.3	0.30	5	73.68
55	54.66	47	12.1	21.6	3.2	0.00	21.6	16.2	0.27	5	71.81
56	54.68	47	11.8	21.2	3.2	0.00	21.3	16.5	0.29	5	72.43
57	54.70	47	11.7	21.1	3.4	0.00	21.2	16.6	0.29	4	71.75
58	54.73	47	11.6	21.5	3.2	0.00	21.7	16.3	0.29	5	72.23
59	54.75	47	12.0	21.6	3.2	0.00	21.7	16.1	0.28	5	72.28
60	54.77	47	11.6	21.6	3.4	0.00	21.7	16.4	0.31	5	73.76
61	54.79	47	11.7	21.4	3.5	0.00	21.5	15.7	0.29	5	72.69
62	54.81	47	11.7	21.7	3.4	0.00	21.7	16.8	0.29	4	72.24
63	54.83	47	11.9	21.5	3.3	0.00	21.6	15.9	0.30	5	73.48
64	54.85	47	11.5	21.6	3.6	0.00	21.6	15.8	0.30	5	73.37
65	54.87	47	11.9	21.6	3.2	0.00	21.7	16.5	0.28	5	72.35
66	54.89	47	11.7	21.4	3.4	0.00	21.5	16.4	0.29	5	72.12
67	54.92	47	12.0	21.3	3.3	0.00	21.3	16.5	0.28	5	72.10
68	54.94	47	11.6	21.7	3.6	0.00	21.8	16.7	0.30	5	73.06
69	54.96	47	11.4	21.5	3.4	0.00	21.5	16.6	0.30	5	73.07
70	54.98	47	11.5	21.7	3.4	0.00	21.8	16.4	0.28	5	72.03
71	55.00	47	11.6	21.4	4.0	0.00	21.5	16.1	0.28	5	73.35
Average			9.9	21.4	3.9	**	21.5	16.5	0.41	4	72.31
Std. Dev.			1.5	0.2	1.7	**	0.2	0.4	0.27	1	0.78
Maximum			12.1	21.7	10.0	**	21.8	17.7	1.55	5	74.32
Minimum			6.4	21.0	1.9	**	21.1	15.4	0.27	1	70.49

Total number of blows analyzed: 71

#### BL# Sensors

1-71 F1: [357AWJ1] 212.0 (1.12); F4: [357AWJ2] 211.2 (1.12); A2: [55385] 915.0 (0.88);  
A3: [50148] 1065.0 (0.88)

#### BL# Comments

71 end of set 5. n=51

#### Time Summary

Drive 1 minute 41 seconds 2:42 PM - 2:43 PM BN 1 - 71