

# Geotechnical Data Report

**S-38-50 (Four Holes Road)  
over I-26 Emergency Bridge Replacement  
Orangeburg County, South Carolina**

May 22, 2018 (Revision 1)

SCDOT Project ID.: P037465

Terracon Project No. 73155050U

Prepared for:

South Carolina Department of Transportation  
Columbia, South Carolina

Prepared by:

Terracon Consultants, Inc.  
Columbia, South Carolina

Offices Nationwide  
Employee-Owned

Established in 1965  
[terracon.com](http://terracon.com)

The Terracon logo features the word "Terracon" in a bold, white, sans-serif font. The letter "T" is significantly larger and more stylized than the other letters, with a horizontal bar extending to the right. The logo is set against a dark red background.

Geotechnical ■ Environmental ■ Construction Materials ■ Facilities

May 22, 2018 (Revision 1)



South Carolina Department of Transportation  
955 Park Street, Room 421  
Columbia, South Carolina 29201

Attn: Mr. Trapp Harris, P.E.  
Geotechnical Design Engineer – Design-Build Section

Re: Geotechnical Data Report  
S-38-50 (Four Holes Road) Emergency Bridge Replacement over I-26  
Orangeburg County, South Carolina  
SCDOT Project ID.: P037465  
Terracon Project Number: 73155050U

Dear Mr. Harris:

Terracon Consultants Inc. (Terracon) has completed the geotechnical exploration and testing services for the above referenced project. These services were conducted in general accordance with the SCDOT Request for Subsurface Exploration and Laboratory Testing (SCDOT Project ID: P037465, authorized on April 24, 2018). This geotechnical data report presents the findings of the subsurface exploration and laboratory testing along with an overview of testing activities.

## 1.0 INTRODUCTION

The South Carolina Department of Transportation (SCDOT) has contracted Terracon to perform subsurface exploration and laboratory testing for the replacement of the S-38-50 (Four Holes Road) Bridge over I-26 in Orangeburg County, SC. The purpose this work is to develop information relative to subsurface soil, rock, and groundwater conditions at the bridge location. This report presents the results of that work. No geotechnical recommendations are associated with the requested scope of study.

The following sections of this report contain a summary of the activities for our field exploration and laboratory testing. The logs of the borings, the Site Location Map and the Exploration Plan are included in Appendix A of this report. The results of the laboratory testing performed on rock samples obtained from the site during the field exploration are included in Appendix B of this report. Descriptions of the field exploration and laboratory testing are included in their respective appendices.



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Geotechnical



Environmental



Construction Materials



Facilities

## **2.0 PROJECT DESCRIPTION**

The project site is located at the overpass of S-38-50 (Four Holes Road) and Interstate 26 in Orangeburg County, South Carolina. The Site Location Map and Boring Location Plan are presented in Appendix A of this report. It is our understanding that the project will include the replacement of the previously demolished bridge with a new structure on the existing or similar horizontal alignment. The original structure appears to have been supported with deep foundations.

## **3.0 GEOTECHNICAL TESTING**

The geotechnical exploration for this project was performed between April 26 and 27, 2018. The results of our field work and our associated laboratory testing is attached in appendixes A and B of this report.

### **3.1 Field Exploration**

Our field exploration at the site consisted of the following:

- Two (2) Standard Penetration Test (SPT) Borings (B-1 and B-2)
- Two (2) CPT Soundings (C-1 and C-2)
- Geophysical testing including one (1) Multi-channel Analysis of Surface Waves test array (MASW-1)

The tests were performed at the approximate locations provided by the SCDOT. A description of our testing methods and graphical logs outlining the soil conditions at each test location are presented in Appendix A. Test locations were established in the field by Terracon and surveyed by Construction Support Services, LLC, after completion. Photographs of the drill rig set up at each boring location along with general photographs of the existing bridge are provided in Appendix A.

### **3.2 Laboratory Testing**

The following laboratory tests were performed on the soil samples collected at the site.

- Ten (10) Natural Moisture Content Tests
- Ten (10) No. 200 Wash
- Three (3) Compressive Strength of Rock Tests

The scope of the laboratory testing frequency was determined by the SCDOT. The laboratory procedures and results of the laboratory tests are presented in Appendix B.

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**4.0 CLOSURE**

We appreciate the opportunity to be of service to you on this project. If you have any questions concerning this report or we may be of further service, please contact us.

Sincerely,

**Terracon Consultants, Inc.**

Joseph D.M. Fredendall, E.I.T.  
Geotechnical Staff Engineer

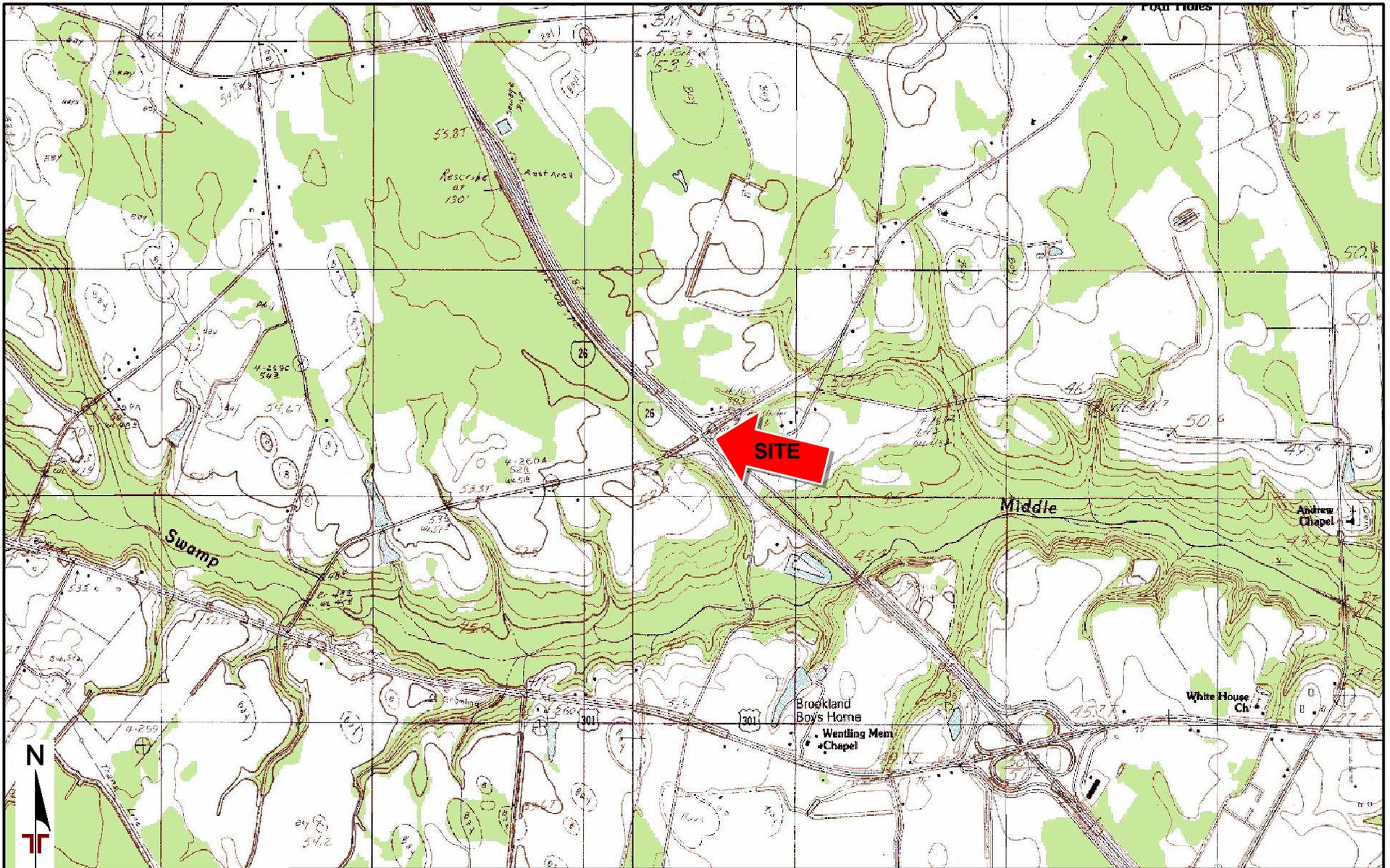
Phillip A. Morrison, P.E.  
Geotechnical Department Manager  
SC Registration No. 17275

Attachments

Copies: Addressee (1 via email)  
File (1)

**APPENDIX A  
FIELD EXPLORATION**

- Exhibit A-1 – Site Location Map**
- Exhibits A-2 – Boring Location Plan**
- Exhibit A-3 – Summary of Field Data**
- Exhibit A-4 – MASW Results**
- Exhibit A-5 – Field Exploration Description**
- Exhibit A-6 – Soil Description Terms**
- Exhibit A-7 – Rock Description Terms**
- Exhibit A-8 – Boring Logs**
- Exhibit A-9 – CPT Logs**
- Exhibit A-10 –Rock Photographic Log**
- Exhibit A-11 – Drill Rig Photograph Log**



TOPOGRAPHIC MAP IMAGE COURTESY OF THE U.S. GEOLOGICAL SURVEY  
 QUADRANGLES INCLUDE: ORANGEBURG SOUTH, SC (1/1/1982) and INDIAN CAMP BRANCH, SC (1/1/1982).

DIAGRAM IS FOR GENERAL LOCATION ONLY, AND IS NOT INTENDED FOR CONSTRUCTION PURPOSES

Project Manager: JDF	Project No. 73155050U
Drawn by: PTK	Scale: 1"=2,000'
Checked by: JDF	File Name: A-1 & A-2
Approved by: PAM	Date: May 2018

**Terracon**

521 Clemson Rd  
 Columbia, SC 29229-4307

**SITE LOCATION MAP**

S-38-50 (Four Holes Road) RBO I-26  
 SC-38-50  
 Columbia, South Carolina

Exhibit

**A-1**



AERIAL PHOTOGRAPHY PROVIDED BY MICROSOFT BING MAPS

DIAGRAM IS FOR GENERAL LOCATION ONLY, AND IS NOT INTENDED FOR CONSTRUCTION PURPOSES

Project Manager: JDF  
 Drawn by: PTK  
 Checked by: JDF  
 Approved by: PAM

Project No. 73155050U  
 Scale: AS SHOWN  
 File Name: A-1 & A-2  
 Date: May 2018

**Terracon**  
 521 Clemson Rd  
 Columbia, SC 29229-4307

**EXPLORATION PLAN**

S-38-50 (Four Holes Road) RBO I-26  
 SC-38-50  
 Columbia, South Carolina

Exhibit  
**A-2**

**Geotechnical Data Report**

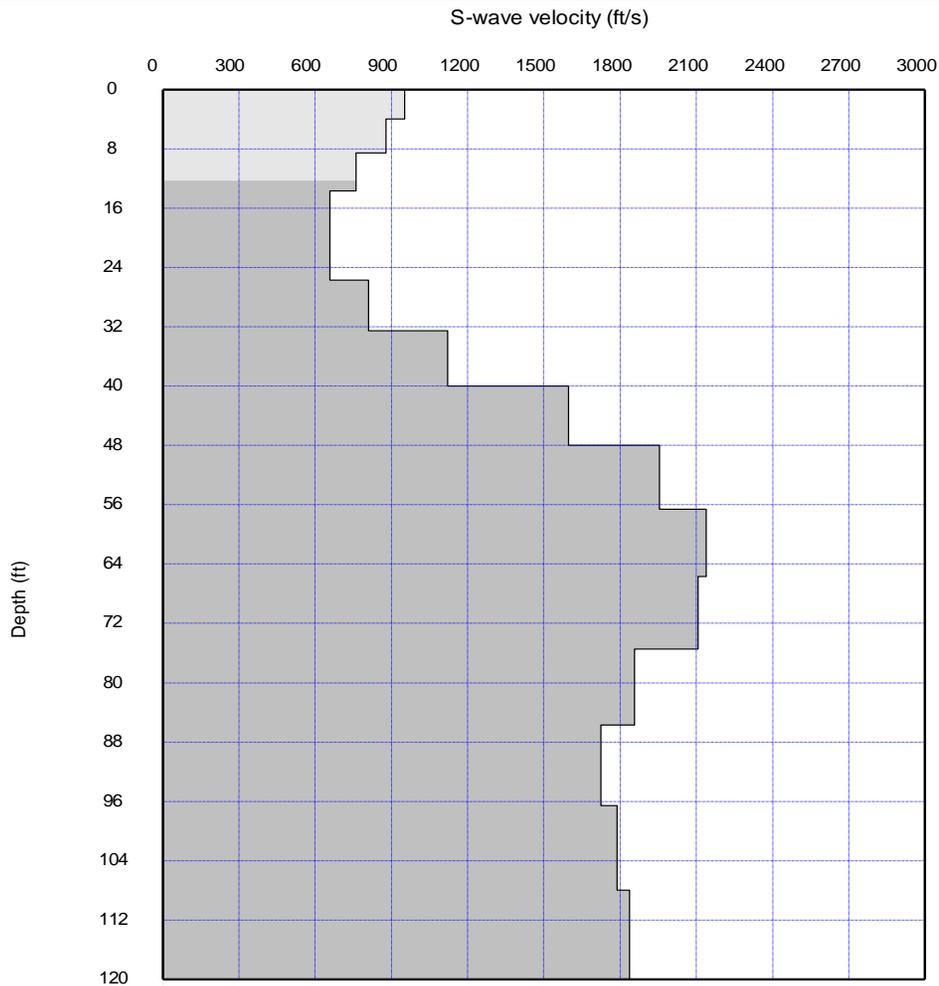
S-38-50 (Four Holes Road) RBO I-26 ■ Orangeburg County, SC

May 22, 2018 (Revision 1) ■ Terracon Project No. 73155050U

**Summary of Field Data**

Test No.	Ground Elevation (ft)	Test Depth (ft.)	Northing	Easting	Latitude	Longitude
B-1	191.31	94	595711.75	2077182.07	33.4703928	-80.7468663
B-2	191.20	90	595846.24	2077438.70	33.4707608	-80.7460235
C-1	190.78	66.8	595687.49	2077171.71	33.4703262	-80.7469007
C-2	190.84	67.4	595869.56	2077446.91	33.4708248	-80.7459964
MASW-1 <sup>1</sup>	152.31 <sup>1</sup>	N.A.	595607.86 <sup>1</sup>	2077075.09 <sup>1</sup>	33.4701081 <sup>1</sup>	-80.7472182 <sup>1</sup>

1. Approximate center of array

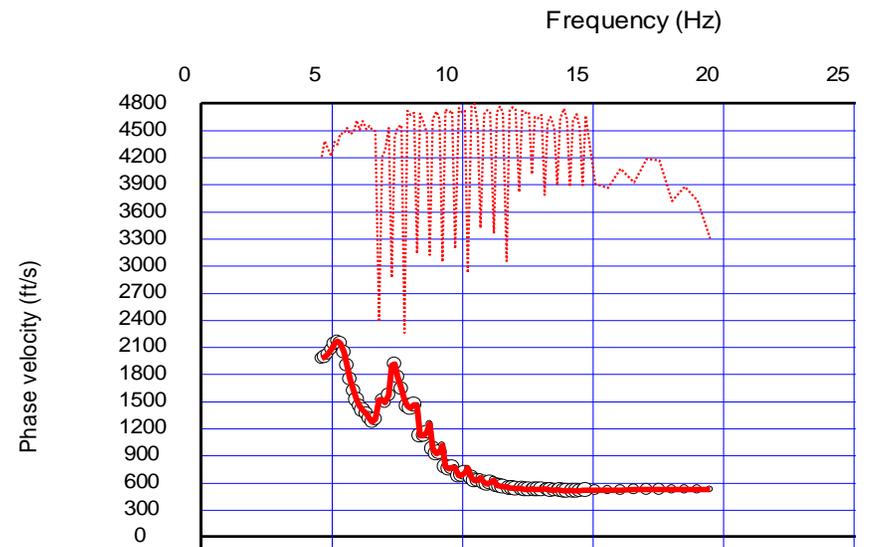


S-wave velocity model : Active and Passive Combined.rst

Average Weighted Shear Wave Velocity (ft/s)<sup>1</sup> = **1271**  
 Seismic Site Classification = **C**

1. Between 0 ft and 100 ft.

Testing Results	
Depth(ft)	S-wave velocity(ft/s)
0.0	952
4.0	878
8.6	760
13.7	658
19.4	658
25.7	810
32.6	1122
40.0	1597
48.0	1954
56.6	2140
65.7	2106
75.4	1857
85.7	1900
96.6	1920
108.0	1836



Dispersion curve : Active and Passive Combined.rst

Project Mgr:	BTS
Prepared by:	WJB
Checked by:	BTS
Approved by:	BTS

Project No.	73155050U
Scale:	NA
Date:	4/30/2018

**Terracon**

1450 FIFTH STREET WEST NORTH CHARLESTON, SC  
 PH: (843) 884-1234 Fax: (843) 884-9234

**GEOPHYSICAL TESTING RESULTS**  
**MASW SHEAR WAVE VELOCITY**  
**S-38-50 (Four Holes Road) over I-26 Bridge Replacement**  
**Orangeburg County, South Carolina**

<b>TEST N0</b>
<b>MASW-1</b>

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## FIELD EXPLORATION DESCRIPTION

### Overview

The testing locations were provided by the SCDOT and located in the field by Terracon by taking measurements from existing structures shown on the provided drawings. The borings were surveyed by Construction Support Services, LLC after testing and drilling was complete. The locations as shown in the Exploration Location Plan are shown to the scale indicated.

A field log of each test location was prepared by our engineer. The final boring logs included with this report represent the engineer's description of the encountered conditions modified as necessary based on laboratory test results of the individual samples.

### Soil Test Borings (STB)

All boring and sampling operations were conducted in general accordance with the following procedures:

- SCDOT Geotechnical Design Manual 2010
- ASTM D5783, "Standard Guide for Use of Direct Rotary Drilling with Water-Based Drilling Fluid for Geo-environmental Exploration"
- ASTM D6151, "Standard Practice for Using Hollow-Stem Augers for Geotechnical Exploration and Soil Sampling"
- ASTM D1586 "Test Method for Penetration Test and Split-Barrel Sampling of Soils"
- ASTM D4220 "Standard Practices for Preserving and Transporting Soil"
- ASTM D2113 "Standard Practice for Rock Core Drilling and Sampling of Rock for Site Exploration"
- ASTM D5079 "Standard Practices for Preserving and Transporting Rock Core Samples"

Each boring was advanced using rotary wash drilling techniques until refusal was encountered. Upon refusal the material was cored using wireline coring methods. The sampling program is summarized in the following table:

Test ID	Total Depth	Interval of Continuous Sampling
B-1	120 feet or refusal and 20 feet of coring	0 to 20 feet
B-2	120 feet or refusal and 20 feet of coring	0 to 20 feet
C-1	75 feet or refusal	N/A
C-2	75 feet or refusal	N/A

Soil samples were obtained with a standard 1.4-inch I.D., 2-inch O.D., split-barrel sampler, also known as a standard split-spoon. The sampler is advanced into the soil a total of 18 to 24 inches

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by striking the drill rod using a 140-pound automatic hammer falling 30 inches. The number of blows required to advance the sampler for each of three to four, 6-inch increments is recorded. The sum of the number of blows for the second and third increments is called the "Standard Penetration Value", or N-value ( $N_{meas}$ , blows per foot). The N-value, when properly evaluated, is an index to the soil strength.

Soil Classification provides a general guide to the engineering properties of various soil types and enables the engineer to apply his experience to current situations. In our exploration, samples obtained during drilling operations are examined and visually classified by a geotechnical engineer using the procedures outlined in ASTM D2487 - Standard Classification of Soils for Engineering Purposes (Unified Soil Classification System). Laboratory testing was also performed on select split-spoon samples to evaluate index properties for further classification. The soils are described according to color, texture, and relative density or consistency (based on standard penetration resistance). The designations shown on the logs are described on Exhibit A-6.

The borings were advanced either to the planned drilling depth at which they were terminated, or to refusal of the drilling equipment and continued below this depth using diamond bit rock coring techniques. NQ2 sized cores were recovered from the borehole. The rock recovery ratios (REC, percentage of the total core run), Rock Quality Designation (RQD, percentage of the total core run of pieces greater than 4 inches) were recorded along with a description of the rock. An explanation of the rock descriptions shown on the logs is provided on Exhibit A-7 Photos of the recovered rock core specimens are provided on Exhibit A-11 of the Appendix.

The rock cores in Boring B-1 were obtained using a #6 diamond core bit. This is a general purpose coring bit suited for low to medium strength rock formations. The bit was changed to a #2 diamond core bit to core the rock in Boring B-2. This bit is generally more compatible with very low to low strength rock formations. Additionally, the water flow and pressure were reduced to aid in the recovery of the interbedded layers of silty and clayey sand. Based on the increased recovery and RQD values from Boring B-2 relative to Boring B-1, it is possible that similar results could be obtained in Boring B-1 using similar techniques.

Consistent with SCDOT GDM, the borings were drilled using mud rotary drilling techniques. As the drilling method introduces water into the borehole, time-of-drilling water levels could not be recorded. As noted on the boring log, the water level of Boring B-1 was recorded 1 day after the start of drilling activities, kept open using 3-inch diameter casing resting on a very dense clayey sand layer. The water level of Boring B-2 was recorded 4 days after the completion of drilling, kept open using 1-inch piezometer casing with well screen in the lower 10 feet. These water levels are indicated on the boring logs. At the conclusion of the work, the boreholes were backfilled with clean sand and the borings were capped with cold-patch asphalt.

## Seismic Surface Wave Testing

Multi-Channel Analysis of Surface Waves (MASW testing) was performed to determine the shear wave velocity profile of the layered soil system. At the test location both MASW readings (active)

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and Microtremor Array Measurement (MAM) readings (passive) were recorded. The MASW test was conducted using the 24-channel Geometrics Geode seismographs and 4.5-Hz geophones with a linear geometry at an interval of 10-ft. Surface waves were generated by a 20-pound sledgehammer striking a polyethylene plate at four locations. MAM testing was performed along the same survey line.

MASW (Active) Testing - Multi-Channel Analysis of Surface Waves (MASW) is a seismic method that uses the dispersive characteristics of Rayleigh-type surface waves to determine the variation of the shear-wave velocity of layered soils with depth.

MAM (Passive) Testing - Microtremor Array Measurement (MAM) “for lower frequency surface waves (passive waves) arising from microtremors and/or urban (traffic) noise and recorded them using a linear or two-dimensional (triangle, circle, semicircle, and “shapes”) array of geophones (Zywicki and Rix, 1999; Lie et al., 2000). Multiple noise records are required for analysis. The data filters out the Rayleigh waves through a technique called spatial auto-correction (SPAC). This allows the development of a dispersion curve that is defined as the lower envelope of the measured energy peaks. MAM testing results in lower peak energy selections than the active testing described above.

## SOIL DESCRIPTION TERMS

### Relative Density/Consistency Terms

<u>Relative Density</u> <sup>1</sup>			<u>Consistency</u> <sup>2</sup>		
Descriptive Term	Relative Density	SPT Blow Count	Descriptive Term	Unconfined Compression Strength (q <sub>u</sub> ) (tsf)	SPT Blow Count
Very Loose	0 to 15%	4 and less	Very Soft	0.25 and less	2 and less
Loose	16 to 35%	5 to 10	Soft	0.26 to 0.50	3 to 4
Medium Dense	36 to 65%	11 to 30	Firm	0.51 to 1.00	5 to 8
Dense	66 to 85%	31 to 50	Stiff	1.01 to 2.00	9 to 15
Very Dense	86 to 100%	51 and more	Very Stiff	2.01 to 4.00	16 to 30
			Hard	4.01 and more	31 and more

### Moisture Condition

<u>Descriptive Term</u>	<u>Criteria</u>
Dry	Absence of moisture, dusty, dry to the touch
Moist	Damp but no visible water
Wet	Visible free water, usually in coarse-grained soils below the water table

### Color

Describe the sample color while sample is still moist.

### Angularity<sup>1</sup>

<u>Descriptive Term</u>	<u>Criteria</u>
Angular	Particles have sharp edges and relatively plane sides with unpolished surfaces.
Subangular	Particles are similar to angular description but have rounded edges.
Subrounded	Particles have nearly plane sides but have well-rounded corners and edges.
Rounded	Particles have smoothly curved sides and no edges.

### HCl Reaction<sup>3</sup>

<u>Descriptive Term</u>	<u>Criteria</u>
None Reactive	No visible reaction
Weakly Reactive	Some reaction, with bubbles forming slowly
Strongly Reactive	Violent reaction, with bubbles forming immediately

### Cementation<sup>3</sup>

<u>Descriptive Term</u>	<u>Criteria</u>
Weakly Cemented	Crumbles or breaks with handling or little finger pressure
Moderately Cemented	Crumbles or breaks with considerable finger pressure
Strongly Cemented	Will not crumble or break with finger pressure

### Particle-Size Range<sup>1</sup>

<u>Gravel</u>	Diameter, mm	Sieve Size	<u>Sand</u>	Diameter, mm	Sieve Size
Fine	4.76 to 19.1	#4 to ¾ inch	Fine	0.074 to 0.42	#200 to #40
Coarse	19.1 to 76.2	¾ inch to 3 inch	Medium	0.42 to 2.00	#40 to #10
			Coarse	4.00 to 4.76	#10 to #4

### Primary Soil Type<sup>1,2</sup>

The primary soil type will be shown in all capital letters.

### USCS Soil Designation

Indicate USCS soil designation as defined in ASTM D-2487 and D-2488

### AASHTO Soil Designation

Indicate AASHTO soil designation as defined in AASHTO M-145 and ASTM D-3282

<sup>1</sup> Applies to coarse-grained soils (major portion retained on No. 200 sieve)

<sup>2</sup> Applies to fine-grained soils (major portion passing No. 200 sieve)

<sup>3</sup> Use as required

## DESCRIPTION OF ROCK PROPERTIES

### WEATHERING

Fresh	Rock fresh, crystals bright, few joints may show slight staining. Rock rings under hammer if crystalline.
Very slight	Rock generally fresh, joints stained, some joints may show thin clay coatings, crystals in broken face show bright. Rock rings under hammer if crystalline.
Slight	Rock generally fresh, joints stained, and discoloration extends into rock up to 1 in. Joints may contain clay. In granitoid rocks some occasional feldspar crystals are dull and discolored. Crystalline rocks ring under hammer.
Moderate	Significant portions of rock show discoloration and weathering effects. In granitoid rocks, most feldspars are dull and discolored; some show clayey. Rock has dull sound under hammer and shows significant loss of strength as compared with fresh rock.
Moderately Severe	All rock except quartz discolored or stained. In granitoid rocks, all feldspars dull and discolored and majority show kaolinization. Rock shows severe loss of strength and can be excavated with geologist's pick.
Severe	All rock except quartz discolored or stained. Rock "fabric" clear and evident, but reduced in strength to strong soil. In granitoid rocks, all feldspars kaolinized to some extent. Some fragments of strong rock usually left.
Very severe	All rock except quartz discolored or stained. Rock "fabric" discernible, but mass effectively reduced to "soil" with only fragments of strong rock remaining.
Complete	Rock reduced to "soil". Rock "fabric" not discernible or discernible only in small, scattered locations. Quartz may be present as dikes or stringers.

### HARDNESS (for engineering description of rock – not to be confused with Moh's scale for minerals)

Very hard	Cannot be scratched with knife or sharp pick. Breaking of hand specimens requires several hard blows of geologist's pick.
Hard	Can be scratched with knife or pick only with difficulty. Hard blow of hammer required to detach hand specimen.
Moderately hard	Can be scratched with knife or pick. Gouges or grooves to ¼ in. deep can be excavated by hard blow of point of a geologist's pick. Hand specimens can be detached by moderate blow.
Medium	Can be grooved or gouged 1/16 in. deep by firm pressure on knife or pick point. Can be excavated in small chips to pieces about 1-in. maximum size by hard blows of the point of a geologist's pick.
Soft	Can be gouged or grooved readily with knife or pick point. Can be excavated in chips to pieces several inches in size by moderate blows of a pick point. Small thin pieces can be broken by finger pressure.
Very soft	Can be carved with knife. Can be excavated readily with point of pick. Pieces 1-in. or more in thickness can be broken with finger pressure. Can be scratched readily by fingernail.

#### Joint, Bedding, and Foliation Spacing in Rock <sup>a</sup>

Spacing	Joints	Bedding/Foliation
Less than 2 in.	Very close	Very thin
2 in. – 1 ft.	Close	Thin
1 ft. – 3 ft.	Moderately close	Medium
3 ft. – 10 ft.	Wide	Thick
More than 10 ft.	Very wide	Very thick

a. Spacing refers to the distance normal to the planes, of the described feature, which are parallel to each other or nearly so.

#### Rock Quality Designator (RQD)<sup>a</sup>

RQD, as a percentage	Diagnostic description
Exceeding 90	Excellent
90 – 75	Good
75 – 50	Fair
50 – 25	Poor
Less than 25	Very poor

#### Joint Openness Descriptors

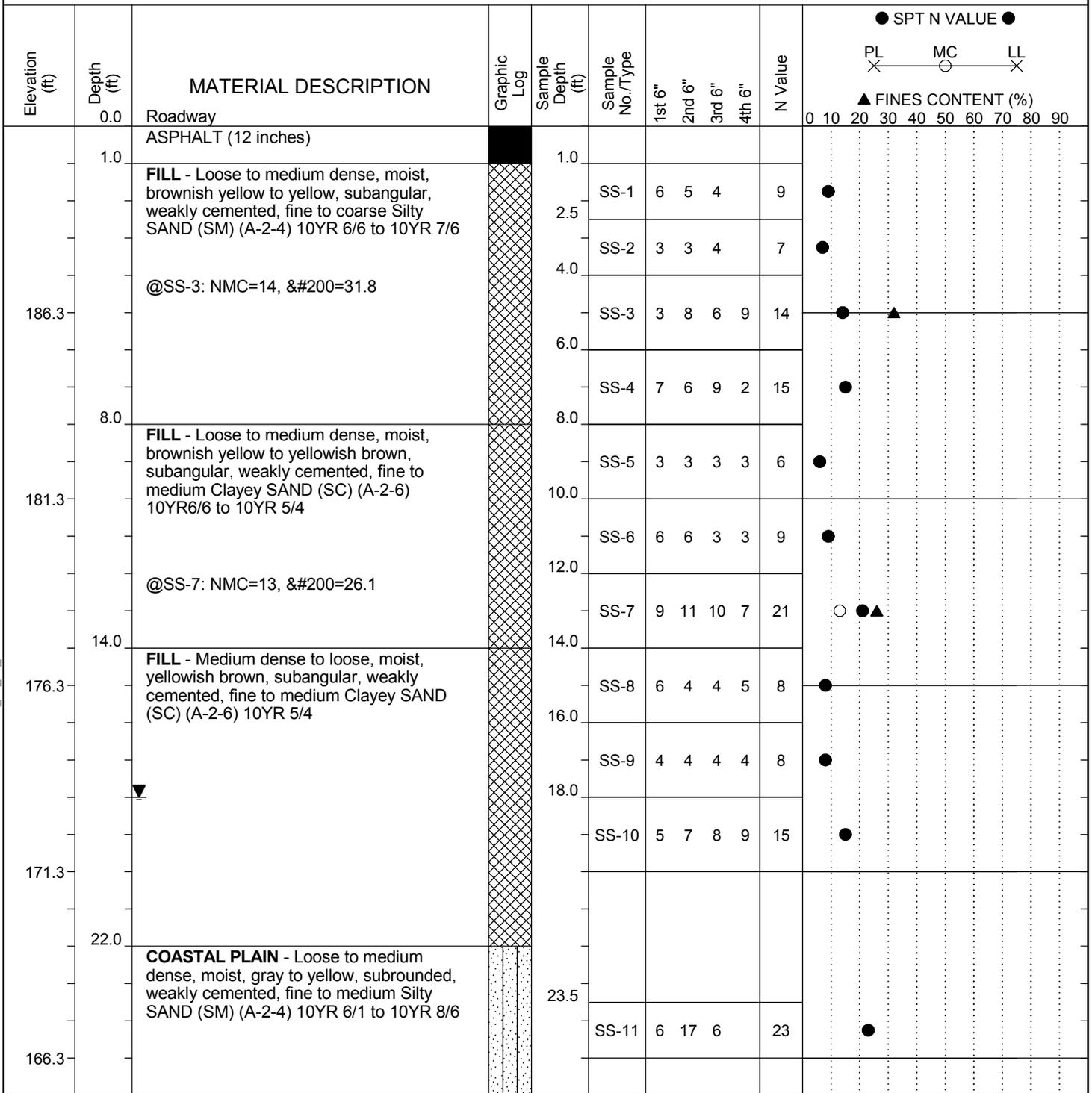
Openness	Descriptor
No Visible Separation	Tight
Less than 1/32 in.	Slightly Open
1/32 to 1/8 in.	Moderately Open
1/8 to 3/8 in.	Open
3/8 in. to 0.1 ft.	Moderately Wide
Greater than 0.1 ft.	Wide

a. RQD (given as a percentage) = length of core in pieces 4 in. and longer/length of run.

References: American Society of Civil Engineers. Manuals and Reports on Engineering Practice - No. 56. Subsurface Investigation for Design and Construction of Foundations of Buildings. New York: American Society of Civil Engineers, 1976. U.S. Department of the Interior, Bureau of Reclamation, Engineering Geology Field Manual.

# SCDOT Soil Test Log

<b>Project ID:</b>	P037465		<b>County:</b>	Orangeburg	<b>Boring No.:</b>	B-1	
<b>Site Description:</b>	S-38-50 (Four Holes Road) over I-26 Emergency Bridge Replacement				<b>Route:</b>	S-38-50	
<b>Eng./Geo.:</b>	J. Fredendall	<b>Boring Location:</b>			<b>Offset:</b>		
<b>Elev.:</b>	191.3 ft	<b>Latitude:</b>	33.4703928	<b>Longitude:</b>	-80.7468663	<b>Date Started:</b>	4/26/2018
<b>Total Depth:</b>	94 ft	<b>Soil Depth:</b>	74 ft	<b>Core Depth:</b>	20 ft	<b>Date Completed:</b>	4/27/2018
<b>Bore Hole Diameter (in):</b>	3.88	<b>Sampler Configuration</b>		<b>Liner Required:</b>	Y (N)	<b>Liner Used:</b>	Y (N)
<b>Drill Machine:</b>	CME-55/300	<b>Drill Method:</b>	RW/RC	<b>Hammer Type:</b>	Automatic	<b>Energy Ratio:</b>	87.7%
<b>Core Size:</b>	NQ2	<b>Driller:</b>	A. McGuire	<b>Groundwater:</b>	TOB N.M.	<b>24HR</b>	18 ft



## LEGEND

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SAMPLER TYPE		DRILLING METHOD	
SS - Split Spoon	NQ - Rock Core, 1-7/8"	HSA - Hollow Stem Auger	RW - Rotary Wash
UD - Undisturbed Sample	CU - Cuttings	CFA - Continuous Flight Augers	RC - Rock Core
AWG - Rock Core, 1-1/8"	CT - Continuous Tube	DC - Driving Casing	

SC\_DOT\_73155050U\_SCDOT\_4\_HOLES\_ROAD\_EBRO\_I-26\_GPJ\_SCDOT\_DATA\_TEMPLATE\_01\_30\_2015.GDT 5/22/18

# SCDOT Soil Test Log

<b>Project ID:</b> P037465	<b>County:</b> Orangeburg	<b>Boring No.:</b> B-1
<b>Site Description:</b> S-38-50 (Four Holes Road) over I-26 Emergency Bridge Replacement	<b>Route:</b> S-38-50	
<b>Eng./Geo.:</b> J. Fredendall	<b>Boring Location:</b>	<b>Offset:</b>
<b>Elev.:</b> 191.3 ft	<b>Latitude:</b> 33.4703928	<b>Longitude:</b> -80.7468663
<b>Total Depth:</b> 94 ft	<b>Soil Depth:</b> 74 ft	<b>Core Depth:</b> 20 ft
<b>Bore Hole Diameter (in):</b> 3.88	<b>Sampler Configuration</b>	<b>Liner Required:</b> Y (N)
<b>Drill Machine:</b> CME-55/300	<b>Drill Method:</b> RW/RC	<b>Hammer Type:</b> Automatic
<b>Core Size:</b> NQ2	<b>Driller:</b> A. McGuire	<b>Energy Ratio:</b> 87.7%
	<b>Groundwater:</b> TOB	<b>24HR:</b> 18 ft

Elevation (ft)	Depth (ft)	MATERIAL DESCRIPTION	Graphic Log	Sample Depth (ft)	Sample No./Type	1st 6"	2nd 6"	3rd 6"	4th 6"	N Value	SPT N VALUE ●									
											PL	MC	LL	▲ FINES CONTENT (%)						
											0	10	20	30	40	50	60	70	80	90
161.3	28.5			28.5	SS-12	3	5	4		9	●									
156.3	33.5	@SS-13: NMC=24, %#200=25.0		33.5	SS-13	3	4	3		7	●	▲								
151.3	37.0	Very loose to loose, wet, red to reddish yellow, subangular, weakly reactive, weakly cemented, fine to medium Silty SAND with shell fragments (SM) (A-2-4) 5R 4/6 to 7.5YR 8/6		38.5	SS-14	2	1	1		2	●									
146.3	43.5	@SS-15: NMC=38, %#200=33.2		43.5	SS-15	woh	1	2		3	●		▲	○						
141.3	48.5	@SS-16: NMC=59, %#200=30.0		48.5	SS-16	woh/12"	2			2	●	▲		○						

LEGEND

Continued Next Page

SAMPLER TYPE		DRILLING METHOD	
SS - Split Spoon	NQ - Rock Core, 1-7/8"	HSA - Hollow Stem Auger	RW - Rotary Wash
UD - Undisturbed Sample	CU - Cuttings	CFA - Continuous Flight Augers	RC - Rock Core
AWG - Rock Core, 1-1/8"	CT - Continuous Tube	DC - Driving Casing	

SCDOT 73155050U SCDOT 4 HOLES ROAD EBRO I-26 GPJ SCDOT DATA TEMPLATE\_01\_30\_2015.GDT 5/22/18

# SCDOT Soil Test Log

<b>Project ID:</b> P037465	<b>County:</b> Orangeburg	<b>Boring No.:</b> B-1
<b>Site Description:</b> S-38-50 (Four Holes Road) over I-26 Emergency Bridge Replacement	<b>Route:</b> S-38-50	
<b>Eng./Geo.:</b> J. Fredendall	<b>Boring Location:</b>	<b>Offset:</b>
<b>Elev.:</b> 191.3 ft	<b>Latitude:</b> 33.4703928	<b>Longitude:</b> -80.7468663
<b>Total Depth:</b> 94 ft	<b>Soil Depth:</b> 74 ft	<b>Core Depth:</b> 20 ft
<b>Bore Hole Diameter (in):</b> 3.88	<b>Sampler Configuration</b>	<b>Liner Required:</b> Y (N)
<b>Drill Machine:</b> CME-55/300	<b>Drill Method:</b> RW/RC	<b>Hammer Type:</b> Automatic
<b>Core Size:</b> NQ2	<b>Driller:</b> A. McGuire	<b>Energy Ratio:</b> 87.7%
	<b>Groundwater:</b> TOB	<b>24HR:</b> 18 ft

Elevation (ft)	Depth (ft)	MATERIAL DESCRIPTION	Graphic Log	Sample Depth (ft)	Sample No./Type	1st 6"	2nd 6"	3rd 6"	4th 6"	N Value	SPT N VALUE									
											PL	MC								
											▲ FINES CONTENT (%)									
											0	10	20	30	40	50	60	70	80	90
136.3	57.0	Stiff, wet, reddish yellow, weakly reactive, Sandy SILT with shell fragments (ML) (A-4) 7.5YR 8/6 @SS-18: NMC=54, %#200=50.9		53.5	SS-17	2	4	4		8	●									
131.3	58.5			58.5	SS-18	2	4	5		9	●	▲								
126.3	67.0	Very dense, moist, gray, angular, weakly reactive, moderately cemented, fine to coarse, Clayey SAND with limestone fragments (SC) (A-2-6) 7.5YR 6/1		63.5	SS-19	3	4	5		9	●									
121.3	68.5			68.5	SS-20	28	39	32		71		●								
72.0	72.0	Hard, moist, light gray, weakly reactive, Lean CLAY with sand (CL) (A-6) 7.5YR 7/1		73.5																
74.0	74.0			74.0	SS-21	50/50/0"				50/0"			>>●							
116.3	74.0	<b>Refusal encountered at 74 feet, set casing and begin coring with #6 bit</b>			NQ2-1															
	76.0	Limestone, light greenish gray, 10G 8/1, smooth, fine to coarse grained, moderately to highly weathered, very weak to medium strong with bedding, narrow to moderately wide discontinuity width, infilled with clay																		

LEGEND

Continued Next Page

SAMPLER TYPE		DRILLING METHOD	
SS - Split Spoon	NQ - Rock Core, 1-7/8"	HSA - Hollow Stem Auger	RW - Rotary Wash
UD - Undisturbed Sample	CU - Cuttings	CFA - Continuous Flight Augers	RC - Rock Core
AWG - Rock Core, 1-1/8"	CT - Continuous Tube	DC - Driving Casing	

SC.DOT 73155050U SCDOT 4 HOLES ROAD EBRO I-26 GPJ SCDOT DATA TEMPLATE\_01\_30\_2015.GDT 5/22/18

# SCDOT Soil Test Log

<b>Project ID:</b>	P037465		<b>County:</b>	Orangeburg	<b>Boring No.:</b>	B-1	
<b>Site Description:</b>	S-38-50 (Four Holes Road) over I-26 Emergency Bridge Replacement				<b>Route:</b>	S-38-50	
<b>Eng./Geo.:</b>	J. Fredendall	<b>Boring Location:</b>		<b>Offset:</b>		<b>Alignment:</b>	Existing
<b>Elev.:</b>	191.3 ft	<b>Latitude:</b>	33.4703928	<b>Longitude:</b>	-80.7468663	<b>Date Started:</b>	4/26/2018
<b>Total Depth:</b>	94 ft	<b>Soil Depth:</b>	74 ft	<b>Core Depth:</b>	20 ft	<b>Date Completed:</b>	4/27/2018
<b>Bore Hole Diameter (in):</b>	3.88	<b>Sampler Configuration</b>		<b>Liner Required:</b>	Y (N)	<b>Liner Used:</b>	Y (N)
<b>Drill Machine:</b>	CME-55/300	<b>Drill Method:</b>	RW/RC	<b>Hammer Type:</b>	Automatic	<b>Energy Ratio:</b>	87.7%
<b>Core Size:</b>	NQ2	<b>Driller:</b>	A. McGuire	<b>Groundwater:</b>	TOB N.M.	<b>24HR</b>	18 ft

Elevation (ft)	Depth (ft)	MATERIAL DESCRIPTION	Graphic Log	Sample Depth (ft)	Sample No./Type	1st 6"	2nd 6"	3rd 6"	4th 6"	N Value	SPT N VALUE									
											PL	MC	LL	FINES CONTENT (%)						
											0	10	20	30	40	50	60	70	80	90
111.3		and sand, very close to close discontinuity spacing, smooth to slightly rough surface @NQ2-1: RQD=0, %REC=16, Run Time = 4 minutes, GSI=10 @NQ2-2: RQD=33, %REC=50, Run Time = 13 minutes, GSI=20, q <sub>u</sub> =2,845psi, RMR=21 Class IIV: Poor Rock @NQ2-3: RQD=0, %REC=10, Run Time = 4 minutes, GSI=10		81.0	NQ2-2															
106.3		@NQ2-4: RQD=10, %REC=10, Run Time = 5 minutes, GSI=5		86.0	NQ2-3															
101.3		@NQ2-5: RQD=18, %REC=50, Run Time = 10 minutes, GSI=10		91.0	NQ2-4															
94.0		<b>Coring Terminated at 94 feet</b>			NQ2-5															

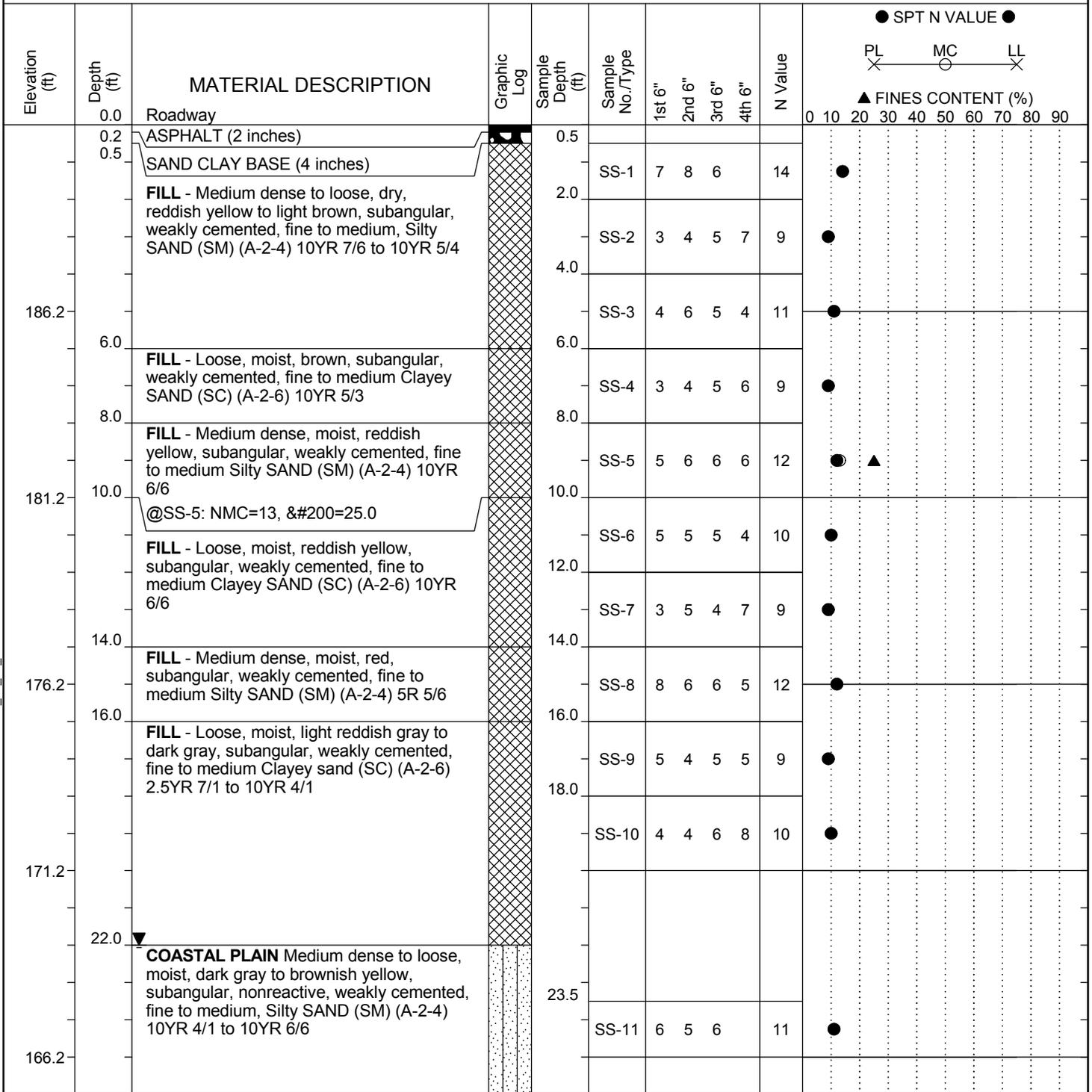
### LEGEND

SAMPLER TYPE		DRILLING METHOD	
SS - Split Spoon	NQ - Rock Core, 1-7/8"	HSA - Hollow Stem Auger	RW - Rotary Wash
UD - Undisturbed Sample	CU - Cuttings	CFA - Continuous Flight Augers	RC - Rock Core
AWG - Rock Core, 1-1/8"	CT - Continuous Tube	DC - Driving Casing	

SC\_DOT\_73155050U\_SCDOT\_4\_HOLES\_ROAD\_EBRO\_I-26\_GPJ\_SCDOT\_DATA\_TEMPLATE\_01\_30\_2015\_GDT\_5/22/18

# SCDOT Soil Test Log

<b>Project ID:</b>	P037465		<b>County:</b>	Orangeburg	<b>Boring No.:</b>	B-2	
<b>Site Description:</b>	S-38-50 (Four Holes Road) over I-26 Emergency Bridge Replacement				<b>Route:</b>	S-38-50	
<b>Eng./Geo.:</b>	J. Fredendall	<b>Boring Location:</b>			<b>Offset:</b>		
<b>Elev.:</b>	191.2 ft	<b>Latitude:</b>	33.4707608	<b>Longitude:</b>	-80.7460235	<b>Date Started:</b>	4/27/2018
<b>Total Depth:</b>	90 ft	<b>Soil Depth:</b>	70 ft	<b>Core Depth:</b>	20 ft	<b>Date Completed:</b>	5/1/2018
<b>Bore Hole Diameter (in):</b>	3.88	<b>Sampler Configuration</b>		<b>Liner Required:</b>	Y (N)	<b>Liner Used:</b>	Y (N)
<b>Drill Machine:</b>	CME-55/300	<b>Drill Method:</b>	RW/RC	<b>Hammer Type:</b>	Automatic	<b>Energy Ratio:</b>	87.7%
<b>Core Size:</b>	NQ2	<b>Driller:</b>	A. McGuire	<b>Groundwater:</b>	TOB N.M.	<b>24HR</b>	22 ft



## LEGEND

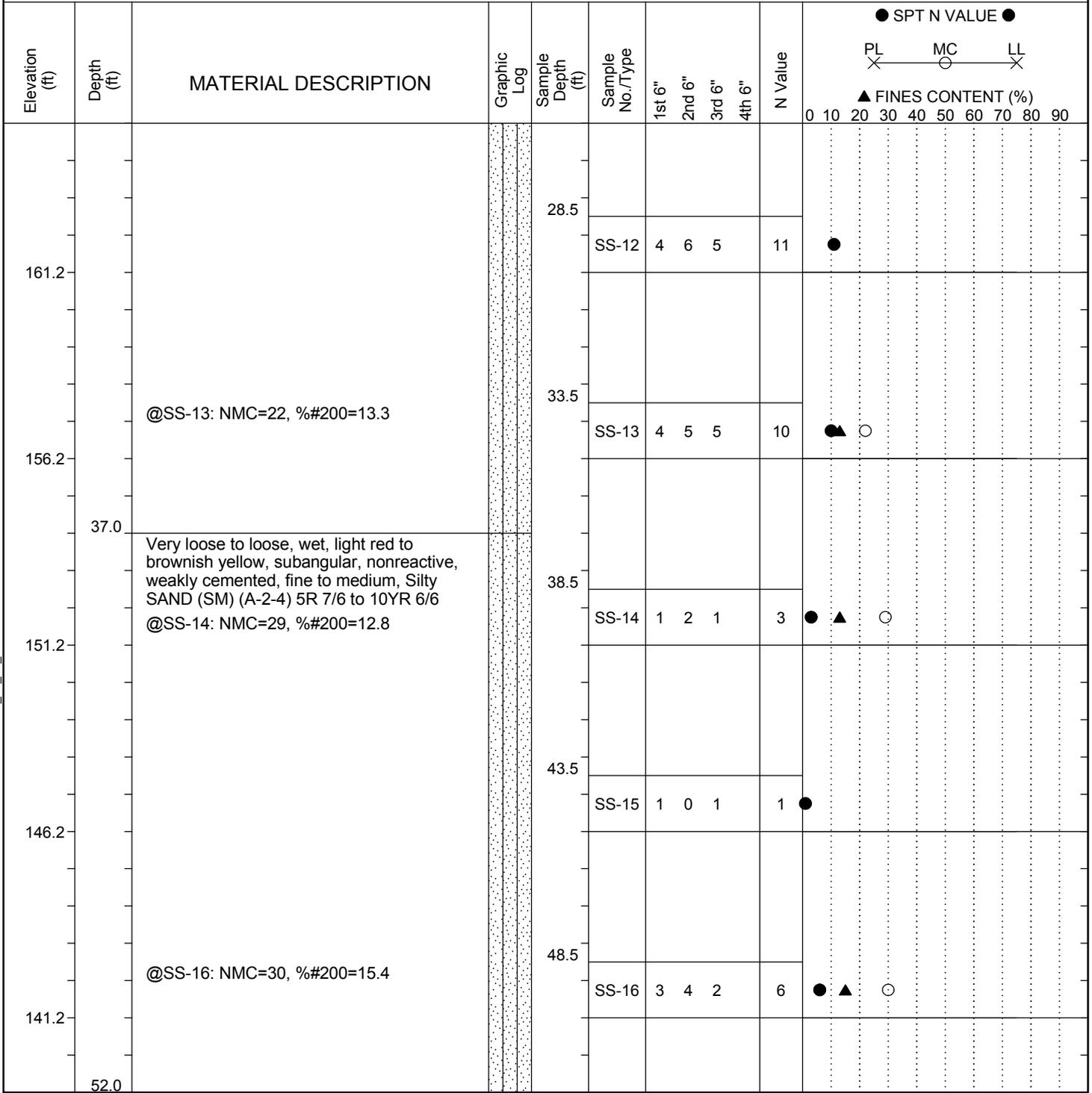
Continued Next Page

SAMPLER TYPE		DRILLING METHOD	
SS - Split Spoon	NQ - Rock Core, 1-7/8"	HSA - Hollow Stem Auger	RW - Rotary Wash
UD - Undisturbed Sample	CU - Cuttings	CFA - Continuous Flight Augers	RC - Rock Core
AWG - Rock Core, 1-1/8"	CT - Continuous Tube	DC - Driving Casing	

SC.DOT 73155050U SCDOT 4 HOLES ROAD EBRO I-26 GPJ SCDOT DATA TEMPLATE\_01\_30\_2015.GDT 5/22/18

# SCDOT Soil Test Log

<b>Project ID:</b> P037465	<b>County:</b> Orangeburg	<b>Boring No.:</b> B-2
<b>Site Description:</b> S-38-50 (Four Holes Road) over I-26 Emergency Bridge Replacement	<b>Route:</b> S-38-50	
<b>Eng./Geo.:</b> J. Fredendall	<b>Boring Location:</b>	<b>Offset:</b>
<b>Elev.:</b> 191.2 ft	<b>Latitude:</b> 33.4707608	<b>Longitude:</b> -80.7460235
<b>Total Depth:</b> 90 ft	<b>Soil Depth:</b> 70 ft	<b>Core Depth:</b> 20 ft
<b>Bore Hole Diameter (in):</b> 3.88	<b>Sampler Configuration</b>	<b>Liner Required:</b> Y (N)
<b>Drill Machine:</b> CME-55/300	<b>Drill Method:</b> RW/RC	<b>Hammer Type:</b> Automatic
<b>Core Size:</b> NQ2	<b>Driller:</b> A. McGuire	<b>Energy Ratio:</b> 87.7%
	<b>Groundwater:</b> TOB	<b>24HR:</b> 22 ft



**LEGEND**

*Continued Next Page*

<b>SAMPLER TYPE</b>		<b>DRILLING METHOD</b>	
SS - Split Spoon	NQ - Rock Core, 1-7/8"	HSA - Hollow Stem Auger	RW - Rotary Wash
UD - Undisturbed Sample	CU - Cuttings	CFA - Continuous Flight Augers	RC - Rock Core
AWG - Rock Core, 1-1/8"	CT - Continuous Tube	DC - Driving Casing	

SC\_DOT\_73155050U\_SCDOT\_4 HOLES ROAD EBRO I-26.GPJ\_SCDOT DATA TEMPLATE\_01\_30\_2015.GDT 5/22/18



# SCDOT Soil Test Log

<b>Project ID:</b>	P037465			<b>County:</b>	Orangeburg	<b>Boring No.:</b>	B-2
<b>Site Description:</b>	S-38-50 (Four Holes Road) over I-26 Emergency Bridge Replacement					<b>Route:</b>	S-38-50
<b>Eng./Geo.:</b>	J. Fredendall	<b>Boring Location:</b>		<b>Offset:</b>		<b>Alignment:</b>	Existing
<b>Elev.:</b>	191.2 ft	<b>Latitude:</b>	33.4707608	<b>Longitude:</b>	-80.7460235	<b>Date Started:</b>	4/27/2018
<b>Total Depth:</b>	90 ft	<b>Soil Depth:</b>	70 ft	<b>Core Depth:</b>	20 ft	<b>Date Completed:</b>	5/1/2018
<b>Bore Hole Diameter (in):</b>	3.88	<b>Sampler Configuration</b>		<b>Liner Required:</b>	Y (N)	<b>Liner Used:</b>	Y (N)
<b>Drill Machine:</b>	CME-55/300	<b>Drill Method:</b>	RW/RC	<b>Hammer Type:</b>	Automatic	<b>Energy Ratio:</b>	87.7%
<b>Core Size:</b>	NQ2	<b>Driller:</b>	A. McGuire	<b>Groundwater:</b>	TOB N.M.	<b>24HR</b>	22 ft

Elevation (ft)	Depth (ft)	MATERIAL DESCRIPTION	Graphic Log	Sample Depth (ft)	Sample No./Type	1st 6"	2nd 6"	3rd 6"	4th 6"	N Value	SPT N VALUE										
											PL	MC	LL	FINES CONTENT (%)							
111.2		Class IV: Poor Rock  @NQ2-3: RQD=52, %REC=96, Run Time = 7 minutes, GSI=50, q <sub>u</sub> =3,358 psi, RMR=21 Class IV: Poor Rock	[Graphic Log: Rock]	80.0	NQ2-3																
106.2		@NQ2-4: RQD=30, %REC=100, Run Time = 8 minutes, GSI=30		85.0	NQ2-4																
101.2	90.0	<b>Coring Terminated at 90 feet</b>																			
96.2																					
91.2																					

**LEGEND**

<b>SAMPLER TYPE</b>		<b>DRILLING METHOD</b>	
SS - Split Spoon	NQ - Rock Core, 1-7/8"	HSA - Hollow Stem Auger	RW - Rotary Wash
UD - Undisturbed Sample	CU - Cuttings	CFA - Continuous Flight Augers	RC - Rock Core
AWG - Rock Core, 1-1/8"	CT - Continuous Tube	DC - Driving Casing	

SC\_DOT 73155050U SCDOT 4 HOLES ROAD EBRO I-26.GPJ SCDOT DATA TEMPLATE\_01\_30\_2015.GDT 5/22/18

# CPT LOG NO. C-1

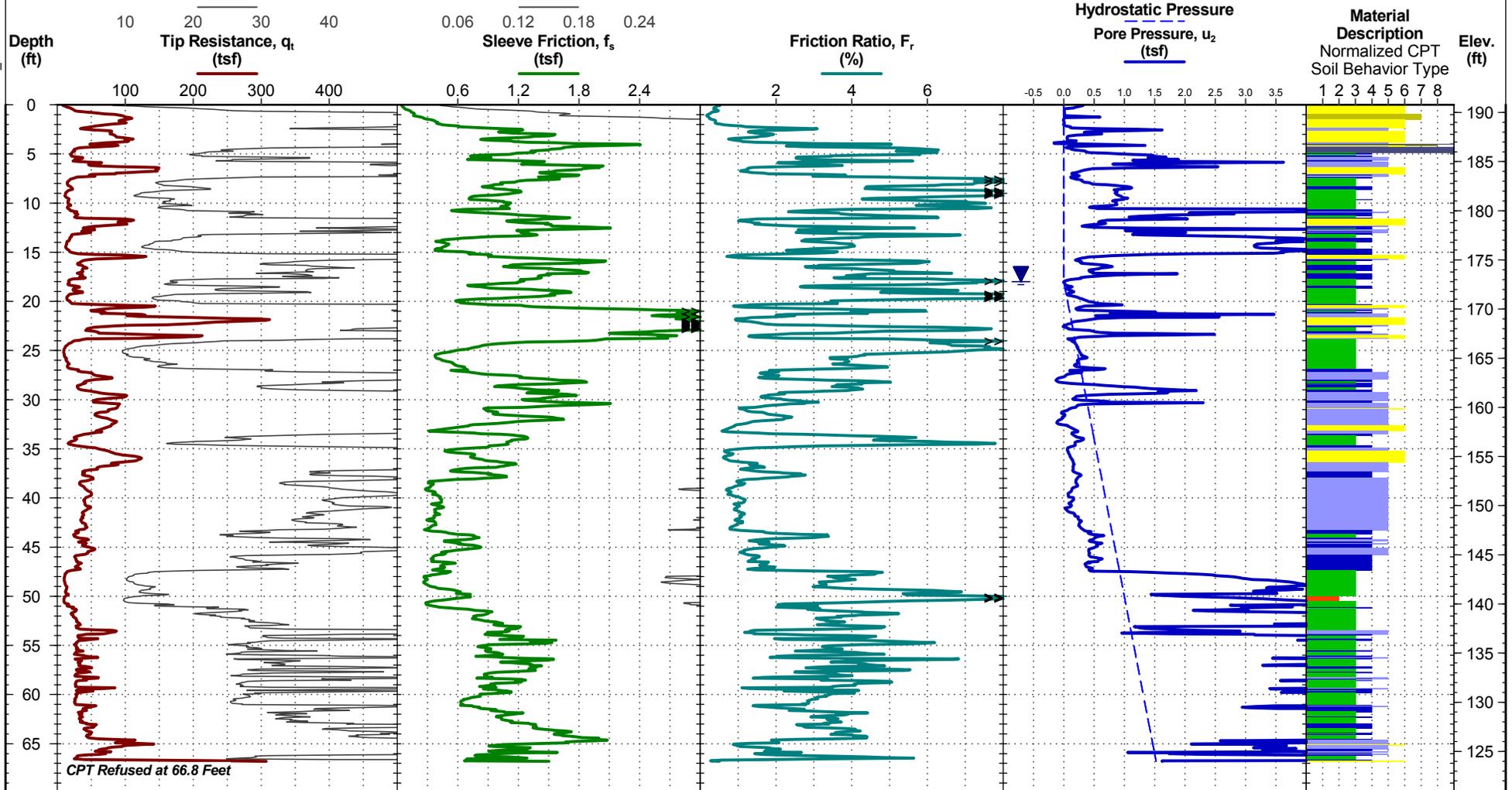
**PROJECT:** S-38-50 (Four Holes Road) Emergency Bridge Replacement over I-26

**CLIENT:** SCDOT  
Columbia, South Carolina

**TEST LOCATION:** See Exhibit A-2

Surface Elev.: 190.78 ft  
Latitude: 33.4703262°  
Longitude: -80.7469007°

**SITE:** 4 Holes Road  
Orangeburg County, South Carolina



See Terracon's CPT General Notes for explanation of symbols and abbreviations.  
Elevations provided by Construction Support Services

Auger anchors used as reaction force.  
CPT sensor calibration reports available upon request.

- 1 Sensitive, fine grained
- 2 Organic soils - clay
- 3 Clay - silty clay to clay
- 4 Silt mixtures - clayey silt to silty clay
- 5 Sand mixtures - silty sand to sandy silt
- 6 Sands - clean sand to silty sand
- 7 Gravelly sand to dense sand
- 8 Very stiff sand to clayey sand
- 9 Very stiff fine grained

THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT. CPT REPORT 73155050U TERRACON LAB 4 HOLES ROAD.GPJ TERRACON\_DATATEMPLATE.GDT 5/22/18

**WATER LEVEL OBSERVATION**

▼ 18 ft measured water depth  
(used in normalizations and correlations)

Probe no. 4986 with net area ratio of 0.865  
U2 pore pressure transducer location  
Manufactured by Geotech A.B.; calibrated 10/3/2017  
Tip and sleeve areas of 10 cm<sup>2</sup> and 150 cm<sup>2</sup>  
Ring friction reducer with O.D. of 1.875 in



CPT Started: 4/25/2018

Rig: Pagani TG73-200

Project No.: 73155050U

CPT Completed: 4/25/2018

Operator: B. Rozier

# CPT LOG NO. C-2

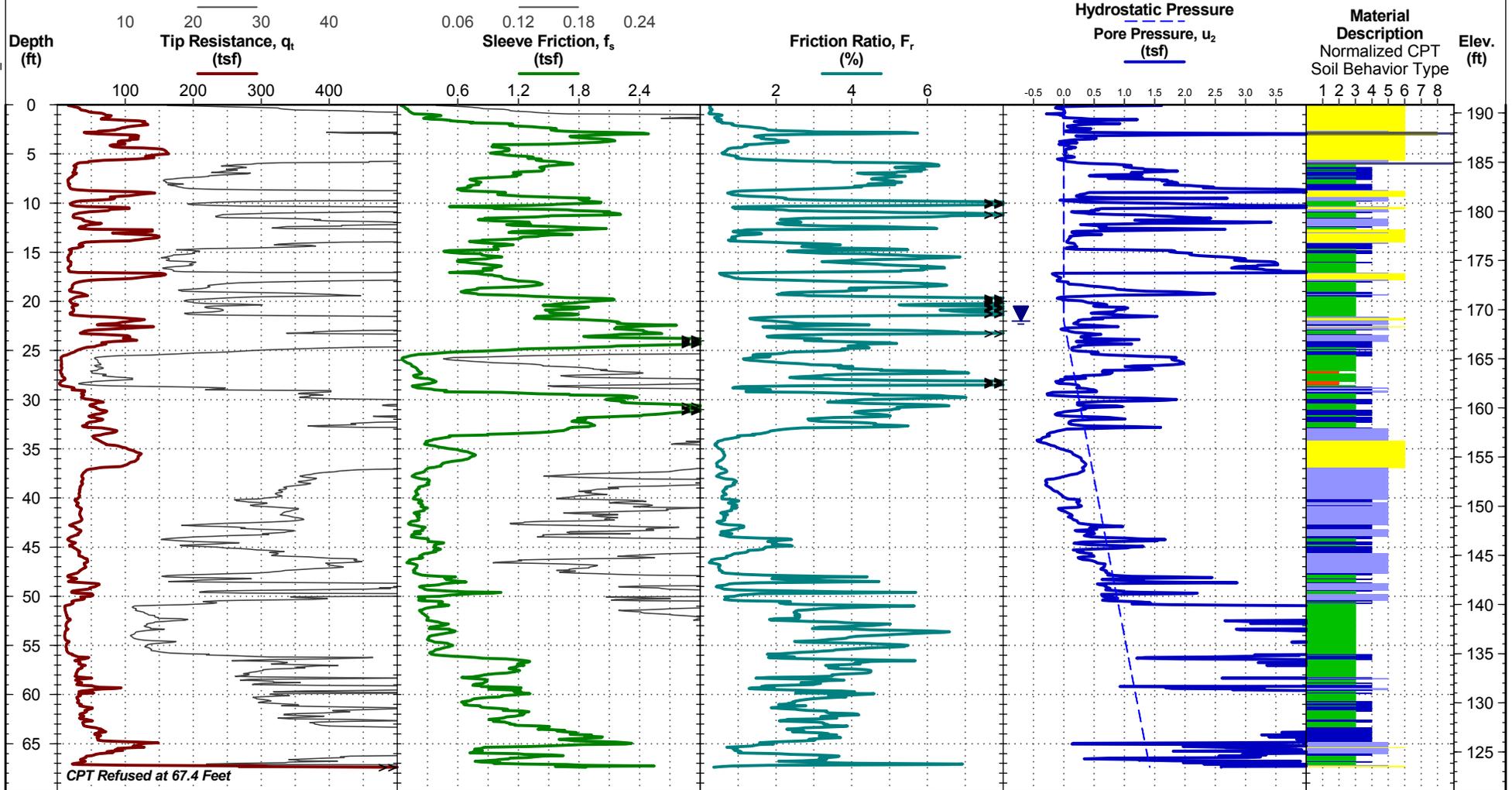
**PROJECT:** S-38-50 (Four Holes Road) Emergency Bridge Replacement over I-26

**CLIENT:** SCDOT  
Columbia, South Carolina

**TEST LOCATION:** See Exhibit A-2

Surface Elev.: 190.84 ft  
Latitude: 33.4708248°  
Longitude: -80.7459964°

**SITE:** 4 Holes Road  
Orangeburg County, South Carolina



See Terracon's CPT General Notes for explanation of symbols and abbreviations.  
Elevations provided by Construction Support Services

Auger anchors used as reaction force.  
CPT sensor calibration reports available upon request.

- 1 Sensitive, fine grained
- 2 Organic soils - clay
- 3 Clay - silty clay to clay
- 4 Silt mixtures - clayey silt to silty clay
- 5 Sand mixtures - silty sand to sandy silt
- 6 Sands - clean sand to silty sand
- 7 Gravelly sand to dense sand
- 8 Very stiff sand to clayey sand
- 9 Very stiff fine grained

THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT. CPT REPORT 73155050U TERRACON LAB 4 HOLES ROAD.GPJ TERRACON\_DATATEMPLATE.GDT 5/22/18

**WATER LEVEL OBSERVATION**

▼ 22 ft measured water depth (used in normalizations and correlations)

Probe no. 4986 with net area ratio of 0.865  
U2 pore pressure transducer location  
Manufactured by Geotech A.B.; calibrated 10/3/2017  
Tip and sleeve areas of 10 cm<sup>2</sup> and 150 cm<sup>2</sup>  
Ring friction reducer with O.D. of 1.875 in



CPT Started: 4/25/2018

Rig: Pagani TG73-200

Project No.: 73155050U

CPT Completed: 4/25/2018

Operator: B. Rozier

# CPT CORRELATIVE PARAMETER LOG NO. C-1

SEE CPT LOG NO. C-1 FOR DETAILED TEST RESULTS

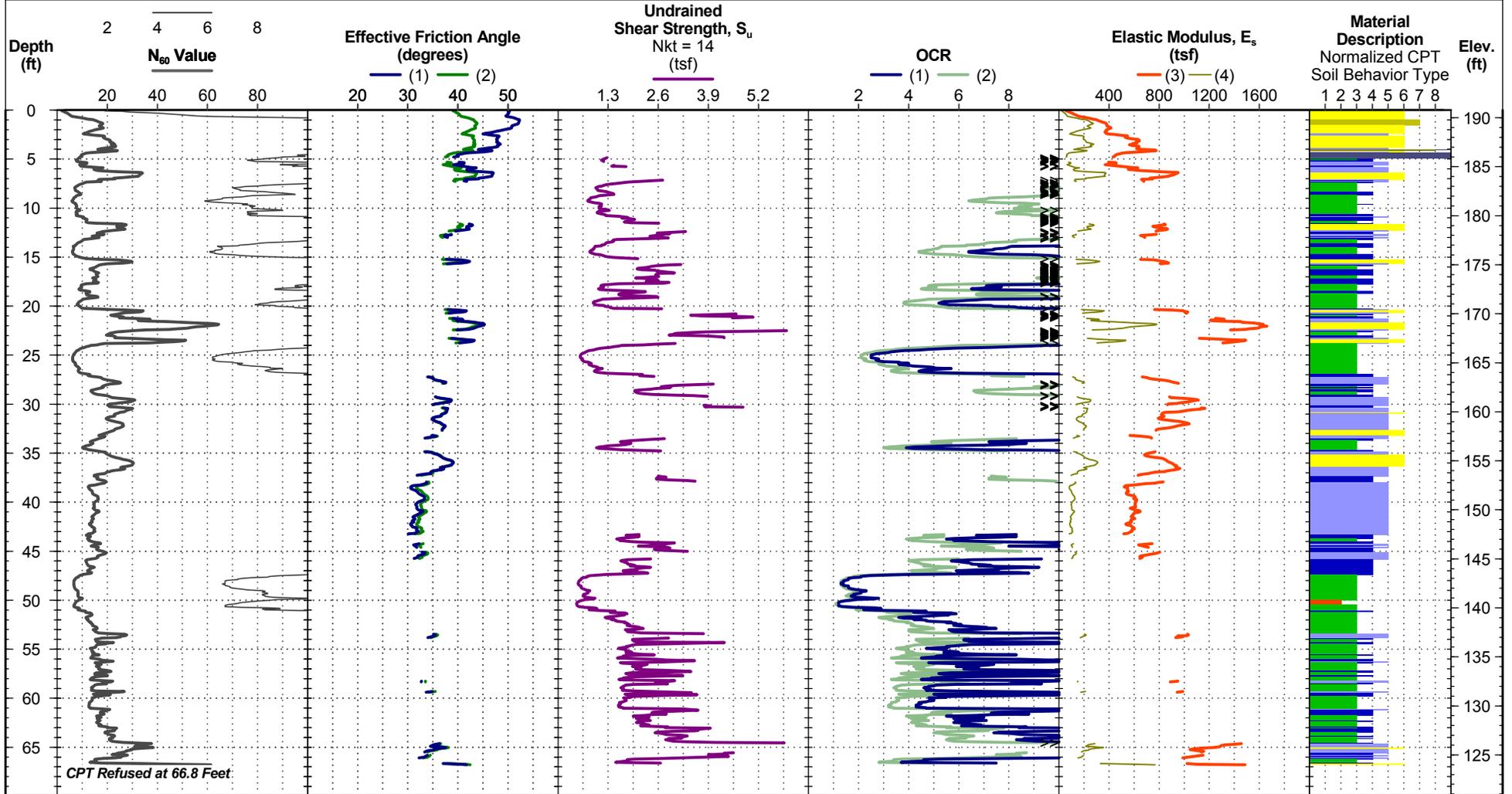
**PROJECT:** S-38-50 (Four Holes Road) Emergency Bridge Replacement over I-26

**CLIENT:** SCDOT  
Columbia, South Carolina

**TEST LOCATION:** See Exhibit A-2

Surface Elev.: 190.78 ft  
Latitude: 33.4703262°  
Longitude: -80.7469007°

**SITE:** 4 Holes Road  
Orangeburg County, South Carolina



Tip resistance, sleeve resistance, porewater pressure, and tilt angle are measured. Other parameters presented are derived from interpretations of the measured data, based upon published correlations, but do not necessarily represent actual values that would be derived from direct testing.

**WATER LEVEL OBSERVATION**

18 ft measured water depth (used in normalizations and correlations)

Notes:  
Probe no. 4986 with net area ratio of 0.865  
Manufactured by Geotech A.B.; calibrated 10/3/2017  
Tip and sleeve areas of 10 cm<sup>2</sup> and 150 cm<sup>2</sup>  
Ring friction reducer with O.D. of 1.875 in



CPT Started: 4/25/2018

Rig: Pagani TG73-200

Project No.: 73155050U

CPT Completed: 4/25/2018

Operator: B. Rozier

THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT. CPT CORRELATIVE PARAMETERS REPORT 73155050U TERRACON LAB 4 HOLES ROAD.GPJ TERRACON\_DATA.TEMPLATE

# CPT CORRELATIVE PARAMETER LOG NO. C-2

SEE CPT LOG NO. C-2 FOR DETAILED TEST RESULTS

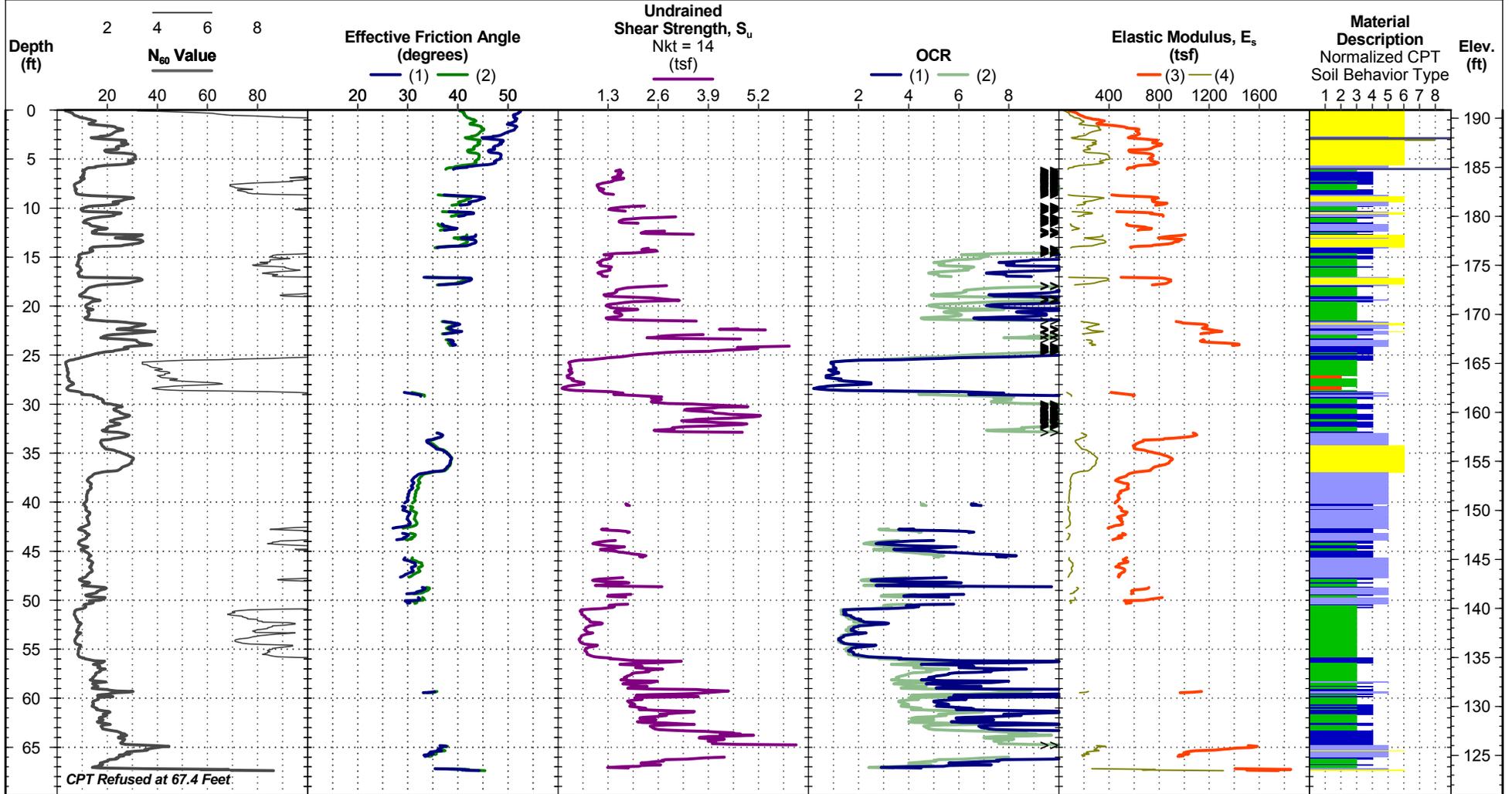
**PROJECT:** S-38-50 (Four Holes Road) Emergency Bridge Replacement over I-26

**CLIENT:** SCDOT  
Columbia, South Carolina

**TEST LOCATION:** See Exhibit A-2

Surface Elev.: 190.84 ft  
Latitude: 33.4708248°  
Longitude: -80.7459964°

**SITE:** 4 Holes Road  
Orangeburg County, South Carolina



Tip resistance, sleeve resistance, porewater pressure, and tilt angle are measured. Other parameters presented are derived from interpretations of the measured data, based upon published correlations, but do not necessarily represent actual values that would be derived from direct testing.

**WATER LEVEL OBSERVATION**

22 ft measured water depth (used in normalizations and correlations)

Notes:  
Probe no. 4986 with net area ratio of 0.865  
Manufactured by Geotech A.B.; calibrated 10/3/2017  
Tip and sleeve areas of 10 cm<sup>2</sup> and 150 cm<sup>2</sup>  
Ring friction reducer with O.D. of 1.875 in



CPT Started: 4/25/2018

Rig: Pagani TG73-200

Project No.: 73155050U

CPT Completed: 4/25/2018

Operator: B. Rozier

THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT. CPT CORRELATIVE PARAMETERS REPORT 73155050U TERRACON LAB 4 HOLES ROAD.GPJ TERRACON\_DATA.TEMPLATE

**Geotechnical Data Report**

S-38-50 (Four Holes Road) RBO I-26 ■ Orangeburg County, SC  
May 22, 2018 (Revision 1) ■ Terracon Project No. 73155050U



B-1 NQ2-1 74-76, NQ2-2 76-81, and NQ2-3 81-86



B-1 NQ2-4 86-91 and NQ2-5 91-94

**Geotechnical Data Report**

S-38-50 (Four Holes Road) RBO I-26 ■ Orangeburg County, SC  
May 22, 2018 (Revision 1) ■ Terracon Project No. 73155050U



B-2 NQ2-1 70-75 and NQ2-2 75-80



B-2 NQ2-3 80-85 and NQ2-4 85-90

**Geotechnical Data Report**

S-38-50 (Four Holes Road) RBO I-26 ■ Orangeburg County, SC  
May 22, 2018 (Revision 1) ■ Terracon Project No. 73155050U



Drill rig on B-1



Drill rig on B-2

**Geotechnical Data Report**

S-38-50 (Four Holes Road) RBO I-26 ■ Orangeburg County, SC  
May 22, 2018 (Revision 1) ■ Terracon Project No. 73155050U



CPT rig on C-1



CPT rig on C-2

**APPENDIX B**  
**LABORATORY TESTING**

**Exhibit B-1 – Laboratory Testing Description**  
**Exhibit B-2 – Summary of Laboratory Data**  
**Laboratory Data Sheets**

## Geotechnical Data Report

S-38-50 (Four Holes Road) RBO I-26 ■ Orangeburg County, SC  
May 22, 2018 (Revision 1) ■ Terracon Project No. 73155050U



### LABORATORY TESTING DESCRIPTION

The samples collected during the field exploration were taken to our laboratory for additional testing. The laboratory testing program was developed by the SCDOT. Using the provided testing program, the laboratory tests were conducted on selected soil samples from the borings and the bulk samples locations. The test results are presented in this appendix

The laboratory test results were used to confirm the soil descriptions presented on the boring logs in Appendix A. Laboratory tests were performed in general accordance with the applicable ASTM, AASHTO, SCDOT or other accepted standards.

Selected soil samples obtained from the site were tested for the following engineering properties:

- Particle-Size Distribution (Gradation) of Soils                   AASHTO T88/(ASTM D6913)
- Moisture Content Determination                                    AASHTO T265/(ASTM D2216)
- Compressive Strength and Elastic Moduli of Rock            AASHTO T226/(ASTM D7012)

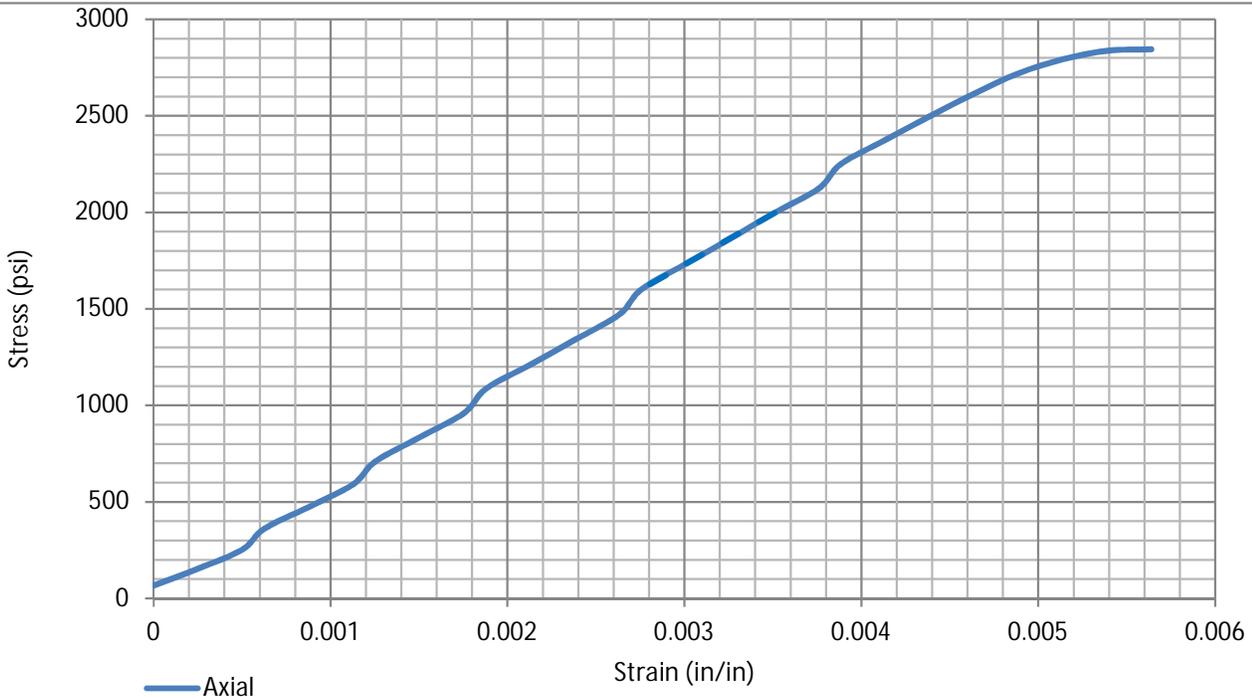
# Summary of Laboratory Results

BORING ID	Depth (Ft.)	% Fines	Water Content (%)
B-1	4 - 6	31.8	14
B-1	12 - 14	26.1	13
B-1	33.5 - 35	25.0	24
B-1	43.5 - 45	33.2	38
B-1	48.5 - 50	30.0	59
B-1	58.5 - 60	50.9	54
B-2	8 - 10	25.0	13
B-2	33.5 - 35	13.3	22
B-2	38.5 - 40	12.8	29
B-2	48.5 - 50	15.4	30

LABORATORY TESTS ARE NOT VALID IF SEPARATED FROM ORIGINAL REPORT. SMART LAB SUMMARY-PORTRAIT\_73155050U TERRACON LAB 4 HOLES ROAD.GPJ TERRACON\_DATATEMPLATE.GDT 5/19/18

PROJECT: S-38-50 (Four Holes Road) Emergency Bridge Replacement over I-26 SITE: Four Holes Road Orangeburg County, South Carolina	 <b>Terracon</b> 521 Clemson Rd Columbia, SC	PROJECT NUMBER: 73155050U CLIENT: SCDOT Columbia, South Carolina EXHIBIT: B-2
---	---	--

**COMPRESSIVE STRENGTH AND ELASTIC MODULUS OF  
INTACT ROCK ASTM D7012**



SAMPLE LOCATION			
Boring:	B-1	Depth (feet):	76.0 - 81.0
SPECIMEN INFORMATION			
Sample No.:	NQ2-2	Mass (g):	489.90
Length (in.):	4.01	Diameter (in.):	1.96
L/D Ratio:	2.05	Density (pcf):	154.25
TEST RESULTS			
Failure Load (lbs):			8,591
Failure Strain (%):			0.56
Unconfined Compressive Strength (psi):			2,845
Elastic Modulus, E, (ksi):			528

Description: Limestone

**NOTES:**

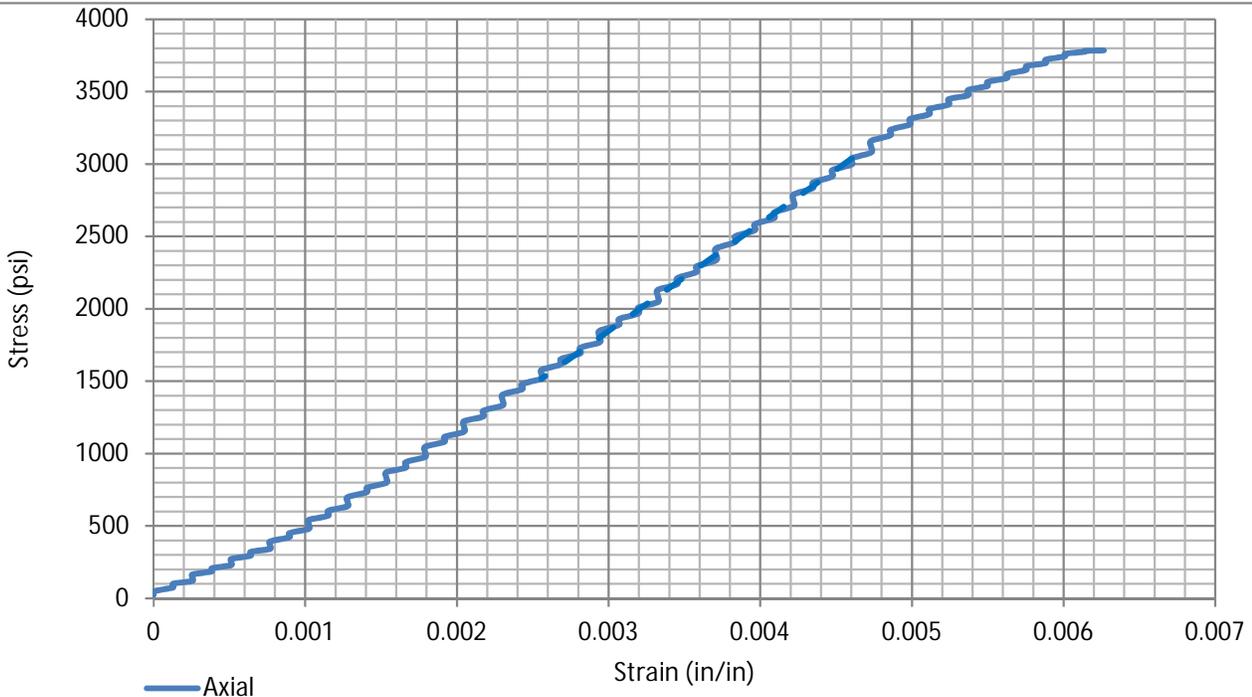
Poisson's Ratio not provided due to non-linear deformation.

CLIENT: SCDOT  
PROJECT: S-38-50 (Four Holes Road)  
over I-26 Emergency Replacement  
PROJECT NO.: 73155050U



LAB NO.: 4026 - Unconfined  
DATE TESTED: 5/15/2018  
DATE REDUCED: 5/18/2018

**COMPRESSIVE STRENGTH AND ELASTIC MODULUS OF  
INTACT ROCK ASTM D7012**



**SAMPLE LOCATION**

Boring:	B-2	Depth (feet):	75.0 - 80.0
---------	-----	---------------	-------------

**SPECIMEN INFORMATION**

Sample No.:	NQ2-2	Mass (g):	475.20
Length (in.):	3.93	Diameter (in.):	1.95
L/D Ratio:	2.02	Density (pcf):	154.24

**TEST RESULTS**

Failure Load (lbs):	11,178
Failure Strain (%):	0.63
Unconfined Compressive Strength (psi):	3,786
Elastic Modulus, E, (ksi):	744

Description: Limestone

**NOTES:**

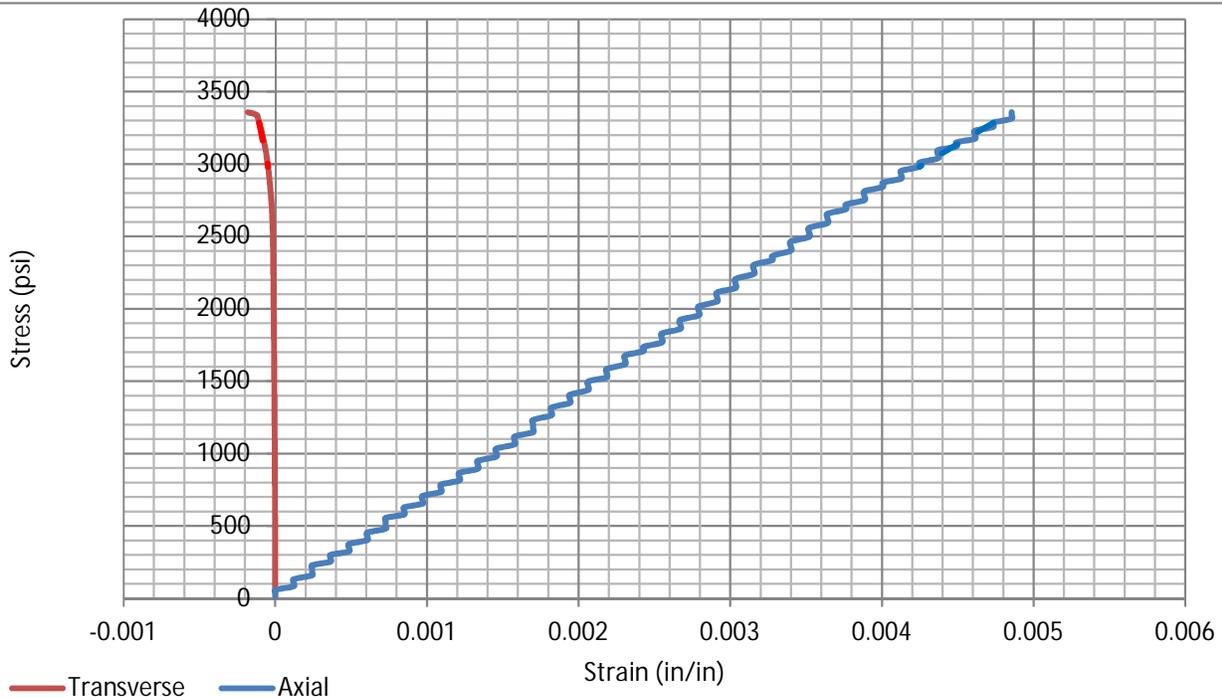
Poisson's Ratio not provided due to non-linear deformation.

CLIENT: SCDOT  
PROJECT: S-38-50 (Four Holes Road)  
over I-26 Emergency Replacement  
PROJECT NO.: 73155050U



LAB NO.: 4027  
DATE TESTED: 5/15/2018  
DATE REDUCED: 5/18/2018

**COMPRESSIVE STRENGTH AND ELASTIC MODULUS OF  
INTACT ROCK ASTM D7012**



SAMPLE LOCATION			
Boring:	B-2	Depth (feet):	80.0 - 85.0
SPECIMEN INFORMATION			
Sample No.:	NQ2-3	Mass (g):	515.50
Length (in.):	4.14	Diameter (in.):	1.97
L/D Ratio:	2.10	Density (pcf):	155.63
TEST RESULTS			
Failure Load (lbs):			10,182
Failure Strain (%):			0.49
Unconfined Compressive Strength (psi):			3,358
Elastic Modulus, E, (ksi):			625
Poisson's Ratio, v:			0.12

Description: Limestone

NOTES:

CLIENT: SCDOT  
 PROJECT: S-38-50 (Four Holes Road)  
 over I-26 Emergency Replacement  
 PROJECT NO.: 73155050U



LAB NO.: 4028  
 DATE TESTED: 5/15/2018  
 DATE REDUCED: 5/18/2018

**APPENDIX C**  
**SUPPORTING DOCUMENTS**

**Exhibit C-1 – General Notes**  
**Exhibit C-2 – Unified Soil Classification System**  
**Exhibit C-3 – Rock Description Terms**  
**Rig Calibration Documentation**

# GENERAL NOTES

## DESCRIPTION OF SYMBOLS AND ABBREVIATIONS

<b>SAMPLING</b>			<b>WATER LEVEL</b>		Water Initially Encountered	<b>FIELD TESTS</b>	(HP) Hand Penetrometer	
	<b>Auger</b>	<b>Split Spoon</b>			Water Level After a Specified Period of Time		(T) Torvane	
					Water Level After a Specified Period of Time		(b/f) Standard Penetration Test (blows per foot)	
	<b>Shelby Tube</b>	<b>Macro Core</b>		Water levels indicated on the soil boring logs are the levels measured in the borehole at the times indicated. Groundwater level variations will occur over time. In low permeability soils, accurate determination of groundwater levels is not possible with short term water level observations.			(PID) Photo-Ionization Detector	
							(OVA) Organic Vapor Analyzer	
<b>Ring Sampler</b>	<b>Rock Core</b>							
								
<b>Grab Sample</b>	<b>No Recovery</b>							

## DESCRIPTIVE SOIL CLASSIFICATION

Soil classification is based on the Unified Soil Classification System. Coarse Grained Soils have more than 50% of their dry weight retained on a #200 sieve; their principal descriptors are: boulders, cobbles, gravel or sand. Fine Grained Soils have less than 50% of their dry weight retained on a #200 sieve; they are principally described as clays if they are plastic, and silts if they are slightly plastic or non-plastic. Major constituents may be added as modifiers and minor constituents may be added according to the relative proportions based on grain size. In addition to gradation, coarse-grained soils are defined on the basis of their in-place relative density and fine-grained soils on the basis of their consistency.

## LOCATION AND ELEVATION NOTES

Unless otherwise noted, Latitude and Longitude are approximately determined using a hand-held GPS device. The accuracy of such devices is variable. Surface elevation data annotated with +/- indicates that no actual topographical survey was conducted to confirm the surface elevation. Instead, the surface elevation was approximately determined from topographic maps of the area.

<b>STRENGTH TERMS</b>	<b>RELATIVE DENSITY OF COARSE-GRAINED SOILS</b> (More than 50% retained on No. 200 sieve.) Density determined by Standard Penetration Resistance Includes gravels, sands and silts.			<b>CONSISTENCY OF FINE-GRAINED SOILS</b> (50% or more passing the No. 200 sieve.) Consistency determined by laboratory shear strength testing, field visual-manual procedures or standard penetration resistance		
	Descriptive Term (Density)	Standard Penetration or N-Value Blows/Ft.	Ring Sampler Blows/Ft.	Descriptive Term (Consistency)	Unconfined Compressive Strength, Qu, psf	Standard Penetration or N-Value Blows/Ft.
Very Loose	0 - 3	0 - 6	Very Soft	less than 500	0 - 1	< 3
Loose	4 - 9	7 - 18	Soft	500 to 1,000	2 - 4	3 - 4
Medium Dense	10 - 29	19 - 58	Medium-Stiff	1,000 to 2,000	4 - 8	5 - 9
Dense	30 - 50	59 - 98	Stiff	2,000 to 4,000	8 - 15	10 - 18
Very Dense	> 50	≥ 99	Very Stiff	4,000 to 8,000	15 - 30	19 - 42
			Hard	> 8,000	> 30	> 42

## RELATIVE PROPORTIONS OF SAND AND GRAVEL

<u>Descriptive Term(s) of other constituents</u>	<u>Percent of Dry Weight</u>
Trace	< 15
With	15 - 29
Modifier	> 30

## RELATIVE PROPORTIONS OF FINES

<u>Descriptive Term(s) of other constituents</u>	<u>Percent of Dry Weight</u>
Trace	< 5
With	5 - 12
Modifier	> 12

## GRAIN SIZE TERMINOLOGY

<u>Major Component of Sample</u>	<u>Particle Size</u>
Boulders	Over 12 in. (300 mm)
Cobbles	12 in. to 3 in. (300mm to 75mm)
Gravel	3 in. to #4 sieve (75mm to 4.75 mm)
Sand	#4 to #200 sieve (4.75mm to 0.075mm)
Silt or Clay	Passing #200 sieve (0.075mm)

## PLASTICITY DESCRIPTION

<u>Term</u>	<u>Plasticity Index</u>
Non-plastic	0
Low	1 - 10
Medium	11 - 30
High	> 30

# UNIFIED SOIL CLASSIFICATION SYSTEM

Criteria for Assigning Group Symbols and Group Names Using Laboratory Tests <sup>A</sup>				Soil Classification		
				Group Symbol	Group Name <sup>B</sup>	
<b>Coarse Grained Soils:</b> More than 50% retained on No. 200 sieve	<b>Gravels:</b> More than 50% of coarse fraction retained on No. 4 sieve	<b>Clean Gravels:</b> Less than 5% fines <sup>C</sup>	$Cu \geq 4$ and $1 \leq Cc \leq 3$ <sup>E</sup>	GW	Well-graded gravel <sup>F</sup>	
		<b>Gravels with Fines:</b> More than 12% fines <sup>C</sup>	Fines classify as ML or MH	GP	Poorly graded gravel <sup>F</sup>	
			Fines classify as CL or CH	GM	Silty gravel <sup>F,G,H</sup>	
		<b>Sands:</b> 50% or more of coarse fraction passes No. 4 sieve	<b>Clean Sands:</b> Less than 5% fines <sup>D</sup>	$Cu \geq 6$ and $1 \leq Cc \leq 3$ <sup>E</sup>	GC	Clayey gravel <sup>F,G,H</sup>
	<b>Sands with Fines:</b> More than 12% fines <sup>D</sup>		Fines classify as ML or MH	SW	Well-graded sand <sup>I</sup>	
			Fines classify as CL or CH	SP	Poorly graded sand <sup>I</sup>	
	<b>Fine-Grained Soils:</b> 50% or more passes the No. 200 sieve		<b>Silts and Clays:</b> Liquid limit less than 50	<b>Inorganic:</b>	$PI > 7$ and plots on or above "A" line <sup>J</sup>	SM
		$PI < 4$ or plots below "A" line <sup>J</sup>			SC	Clayey silt <sup>G,H,I</sup>
<b>Organic:</b>		Liquid limit - oven dried		< 0.75	CL	Lean clay <sup>K,L,M</sup>
		Liquid limit - not dried			ML	Silt <sup>K,L,M</sup>
<b>Silts and Clays:</b> Liquid limit 50 or more		<b>Inorganic:</b>	$PI$ plots on or above "A" line	OL	Organic clay <sup>K,L,M,N</sup>	
			$PI$ plots below "A" line	OH	Organic silt <sup>K,L,M,O</sup>	
		<b>Organic:</b>	Liquid limit - oven dried	< 0.75	CH	Fat clay <sup>K,L,M</sup>
			Liquid limit - not dried		MH	Elastic Silt <sup>K,L,M</sup>
<b>Highly organic soils:</b> Primarily organic matter, dark in color, and organic odor				OH	Organic clay <sup>K,L,M,P</sup>	
				PT	Organic silt <sup>K,L,M,Q</sup>	
				PT	Peat	

<sup>A</sup> Based on the material passing the 3-inch (75-mm) sieve

<sup>B</sup> If field sample contained cobbles or boulders, or both, add "with cobbles or boulders, or both" to group name.

<sup>C</sup> Gravels with 5 to 12% fines require dual symbols: GW-GM well-graded gravel with silt, GW-GC well-graded gravel with clay, GP-GM poorly graded gravel with silt, GP-GC poorly graded gravel with clay.

<sup>D</sup> Sands with 5 to 12% fines require dual symbols: SW-SM well-graded sand with silt, SW-SC well-graded sand with clay, SP-SM poorly graded sand with silt, SP-SC poorly graded sand with clay

$$E \quad Cu = D_{60}/D_{10} \quad Cc = \frac{(D_{30})^2}{D_{10} \times D_{60}}$$

<sup>F</sup> If soil contains  $\geq 15\%$  sand, add "with sand" to group name.

<sup>G</sup> If fines classify as CL-ML, use dual symbol GC-GM, or SC-SM.

<sup>H</sup> If fines are organic, add "with organic fines" to group name.

<sup>I</sup> If soil contains  $\geq 15\%$  gravel, add "with gravel" to group name.

<sup>J</sup> If Atterberg limits plot in shaded area, soil is a CL-ML, silty clay.

<sup>K</sup> If soil contains 15 to 29% plus No. 200, add "with sand" or "with gravel," whichever is predominant.

<sup>L</sup> If soil contains  $\geq 30\%$  plus No. 200 predominantly sand, add "sandy" to group name.

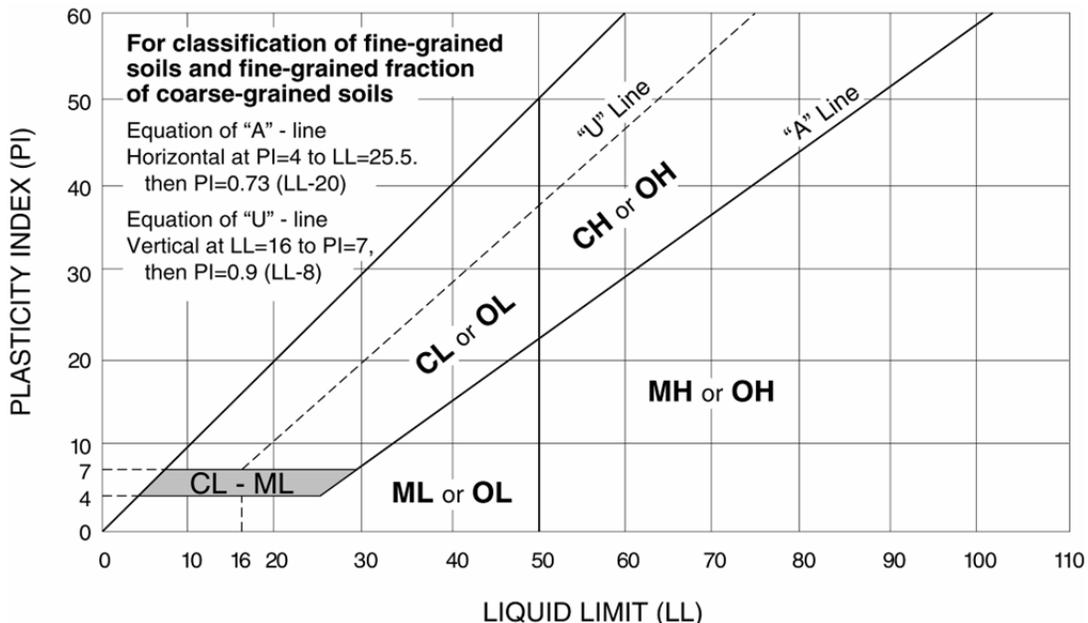
<sup>M</sup> If soil contains  $\geq 30\%$  plus No. 200, predominantly gravel, add "gravelly" to group name.

<sup>N</sup>  $PI \geq 4$  and plots on or above "A" line.

<sup>O</sup>  $PI < 4$  or plots below "A" line.

<sup>P</sup>  $PI$  plots on or above "A" line.

<sup>Q</sup>  $PI$  plots below "A" line.



## DESCRIPTION OF ROCK PROPERTIES

### WEATHERING

Term	Description
<b>Unweathered</b>	No visible sign of rock material weathering, perhaps slight discoloration on major discontinuity surfaces.
<b>Slightly weathered</b>	Discoloration indicates weathering of rock material and discontinuity surfaces. All the rock material may be discolored by weathering and may be somewhat weaker externally than in its fresh condition.
<b>Moderately weathered</b>	Less than half of the rock material is decomposed and/or disintegrated to a soil. Fresh or discolored rock is present either as a continuous framework or as corestones.
<b>Highly weathered</b>	More than half of the rock material is decomposed and/or disintegrated to a soil. Fresh or discolored rock is present either as a discontinuous framework or as corestones.
<b>Completely weathered</b>	All rock material is decomposed and/or disintegrated to soil. The original mass structure is still largely intact.
<b>Residual soil</b>	All rock material is converted to soil. The mass structure and material fabric are destroyed. There is a large change in volume, but the soil has not been significantly transported.

### STRENGTH OR HARDNESS

Description	Field Identification	Uniaxial Compressive Strength, PSI (MPa)
<b>Extremely weak</b>	Indented by thumbnail	40-150 (0.3-1)
<b>Very weak</b>	Crumbles under firm blows with point of geological hammer, can be peeled by a pocket knife	150-700 (1-5)
<b>Weak rock</b>	Can be peeled by a pocket knife with difficulty, shallow indentations made by firm blow with point of geological hammer	700-4,000 (5-30)
<b>Medium strong</b>	Cannot be scraped or peeled with a pocket knife, specimen can be fractured with single firm blow of geological hammer	4,000-7,000 (30-50)
<b>Strong rock</b>	Specimen requires more than one blow of geological hammer to fracture it	7,000-15,000 (50-100)
<b>Very strong</b>	Specimen requires many blows of geological hammer to fracture it	15,000-36,000 (100-250)
<b>Extremely strong</b>	Specimen can only be chipped with geological hammer	>36,000 (>250)

### DISCONTINUITY DESCRIPTION

Fracture Spacing (Joints, Faults, Other Fractures)		Bedding Spacing (May Include Foliation or Banding)	
Description	Spacing	Description	Spacing
<b>Extremely close</b>	< ¾ in (<19 mm)	<b>Laminated</b>	< ½ in (<12 mm)
<b>Very close</b>	¾ in – 2-1/2 in (19 - 60 mm)	<b>Very thin</b>	½ in – 2 in (12 – 50 mm)
<b>Close</b>	2-1/2 in – 8 in (60 – 200 mm)	<b>Thin</b>	2 in – 1 ft (50 – 300 mm)
<b>Moderate</b>	8 in – 2 ft (200 – 600 mm)	<b>Medium</b>	1 ft – 3 ft (300 – 900 mm)
<b>Wide</b>	2 ft – 6 ft (600 mm – 2.0 m)	<b>Thick</b>	3 ft – 10 ft (900 mm – 3 m)
<b>Very Wide</b>	6 ft – 20 ft (2.0 – 6 m)	<b>Massive</b>	> 10 ft (3 m)

Discontinuity Orientation (Angle): Measure the angle of discontinuity relative to a plane perpendicular to the longitudinal axis of the core. (For most cases, the core axis is vertical; therefore, the plane perpendicular to the core axis is horizontal.) For example, a horizontal bedding plane would have a 0 degree angle.

### ROCK QUALITY DESIGNATION (RQD\*)

Description	RQD Value (%)
<b>Very Poor</b>	0 - 25
<b>Poor</b>	25 – 50
<b>Fair</b>	50 – 75
<b>Good</b>	75 – 90
<b>Excellent</b>	90 - 100

\*The combined length of all sound and intact core segments equal to or greater than 4 inches in length, expressed as a percentage of the total core run length.

Reference: U.S. Department of Transportation, Federal Highway Administration, Publication No FHWA-NHI-10-034, December 2009  
Technical Manual for Design and Construction of Road Tunnels – Civil Elements

# DRILL RIG SPT HAMMER ENERGY CALIBRATION REPORT

Drill Rig Model CME-55 SN 359485

Terracon Drill Rig No. 727

Columbia, SC

July 7, 2016

Project No. 73XX0500



**Prepared for:**

Terracon Consultants, Inc.  
Columbia, SC

**Prepared by:**

Terracon Consultants, Inc.  
North Charleston, SC

Offices Nationwide  
Employee-Owned

Established in 1965  
[terracon.com](http://terracon.com)

# Terracon

Geotechnical   ■   Environmental   ■   Construction Materials   ■   Facilities

July 7, 2016



Terracon Consultants Inc.  
521 Clemson Road  
Columbia, SC 29229

Attn: Mr. Phillip Morris  
P: (803) 212-0062  
M: (803) 518-3788  
E: Phillip.Morrison@Terracon.com

Re: SPT Rig Calibration Report  
Columbia, SC  
Terracon Project Number: 73XX0500

Mr. Morrison:

The Charleston office of Terracon Consultants, Inc. (Terracon) has completed the SPT rig calibration for the above referenced rig. This report provides Energy Transfer Ratio (ETR) for the SPT hammer found on CME-55 (Serial Number 359485).

We appreciate the opportunity to be of service to you on this project. If you have any questions concerning this report, or if we may be of further service, please contact us.

Sincerely,  
**Terracon Consultants, Inc.**

Yulian A. Kebede,  
Project Manager  
Geotechnical Services



Bryan T. Shiver, P.E.  
Geotechnical Department Manager  
SC Registration No. 27816

Susheel Kolwalkar, Ph.D., P.E.  
Senior Engineer  
Geotechnical Services



## 1.0 PROJECT INFORMATION

ITEM	DESCRIPTION
Drill Rig Identification	CME-55, SN: 359485 (see photograph on cover page)
Drill Rig Owner	Terracon
Drill Rig Operator	Craig Fredrychowsky
Testing Date	June 14, 2016
Testing Location	Columbia, SC
Terracon Project Number	73XX0500
Boring Identification	Test Hole (B-1)
Energy Measurement Depths	40.5 ft.; 43.5 ft.; 45.5 ft.; 48.5ft.
Hammer Type	Automatic
Boring Method	Mud Rotary
Drill Rods	<ul style="list-style-type: none"> <li>■ AWJ</li> <li>■ 1¾" outside diameter</li> <li>■ 3/16" wall thickness</li> </ul>
SPT Calibration Testing Equipment	<ul style="list-style-type: none"> <li>■ 2 foot AWJ rod instrumented w/ 2 strain gauges and 2 accelerometers</li> <li>■ Model PAX Pile Driving Analyzer™ (PDA)</li> </ul>
SPT Calibration Personnel	Kenneth Zur

## 2.0 TEST RESULTS

**Table 1:**

SPT Hammer Energy Calibration Testing Summary.

Boring	Start Depth <sup>1</sup> (ft)	Rod Length <sup>2</sup> (ft)	Rod Sections <sup>3</sup>			Measured Blow Counts (blows/6 inches)				SPT N <sub>m</sub> (bpf)	Soil Type <sup>4</sup>
			2 ft	5 ft	10 ft	1 <sup>st</sup> Inc.	2 <sup>nd</sup> Inc.	3 <sup>rd</sup> Inc.	4 <sup>th</sup> Inc.		
Test Hole (B-1)	40.5	45.83	1	8	0	9	10	12	-	22	Sand
	43.5	48.83	0	9	0	9	9	12	-	21	Sand
	45.5	50.85	1	9	0	12	19	19	-	38	Sand
	48.5	53.83	0	10	0	10	13	13	-	26	Sand

1. Depth from existing ground surface to bottom of drill rods at the beginning of SPT
2. Total rod length measured from instrumentation to bottom of sampler
3. Two foot section is instrumented and is located at top of drill rods
4. Soil type provided by Terracon personnel.

**Table 2:**  
 Energy Measurement and Analysis Summary.

Boring	Start Depth <sup>1</sup> (ft)	SPT N <sub>m</sub> (bpf)	No. of Blows <sup>2</sup>	EFV (kip-ft) <sup>3</sup>			ETR (%) <sup>3</sup>		
				Max.	Min.	Ave.	Std. Dev.	Ave.	Std. Dev.
Test Hole (B-1)	40.5	22	25	0.29	0.27	0.28	0.004	80.2	1.14
	43.5	21	27	0.29	0.28	0.28	0.005	81.4	1.45
	45.5	38	48	0.29	0.27	0.28	0.007	80.2	1.94
	48.5	26	32	0.28	0.26	0.27	0.006	78.2	1.58
Average:			33	0.29	0.27	0.28	0.01	80.0	1.53

1. Boring ID and depth from existing ground surface to bottom of drill rods at the beginning of SPT  
 2. Number of blows used in energy calibration analysis; limited to measurements recorded during the second and third 6-inch sampling intervals at each depth or during the first increment if refusal were encountered  
 3. EFV = Measured Transferred Energy, ETR = Energy Transfer Ratio.

**Table 3:**  
 Hammer Blow Rate Summary.

Boring	Start Depth <sup>1</sup> (ft)	SPT N <sub>m</sub> (bpf)	No. of Blows <sup>2</sup>	BPM <sup>3</sup>			
				Max.	Min.	Ave.	Std. Dev.
Test Hole (B-1)	40.5	22	25	54.60	53.00	53.74	0.476
	43.5	21	27	54.60	53.10	53.71	0.344
	45.5	38	48	54.90	52.50	53.56	0.454
	48.5	26	32	54.40	52.90	53.68	0.426
Average:			33	54.63	52.88	53.67	0.425

1. Boring ID and depth from existing ground surface to bottom of drill rods at the beginning of SPT.  
 2. Number of blows used in energy calibration analysis. Limited to measurements recorded during the second and third 6-inch sampling intervals at each depth or during the 1st increment if refusal conditions were encountered.  
 3. BPM = Blows per minute

### 3.0 CONCLUSIONS

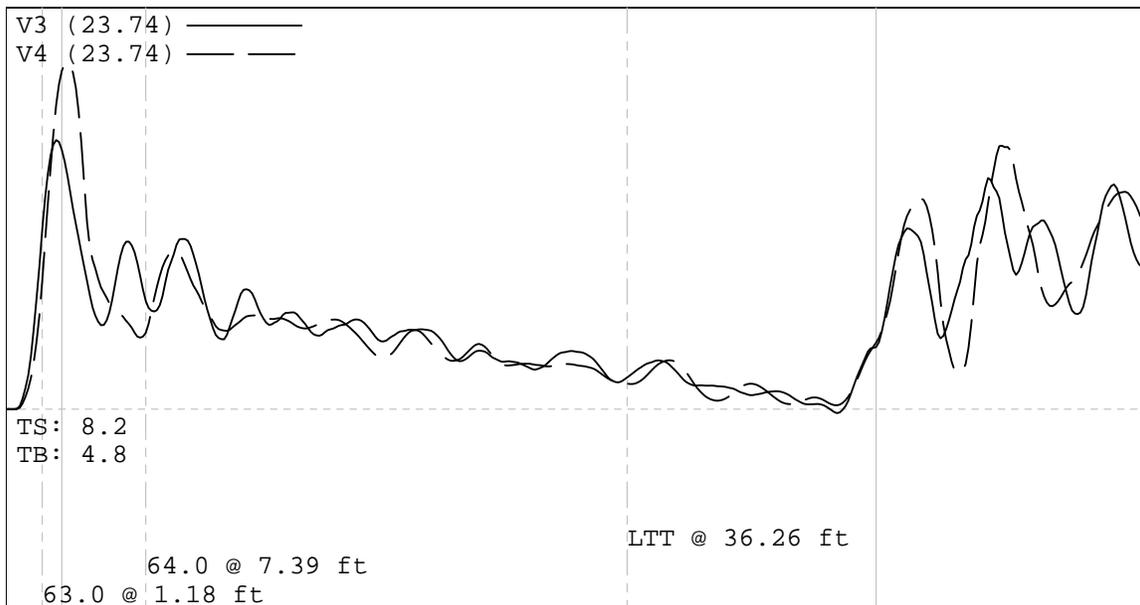
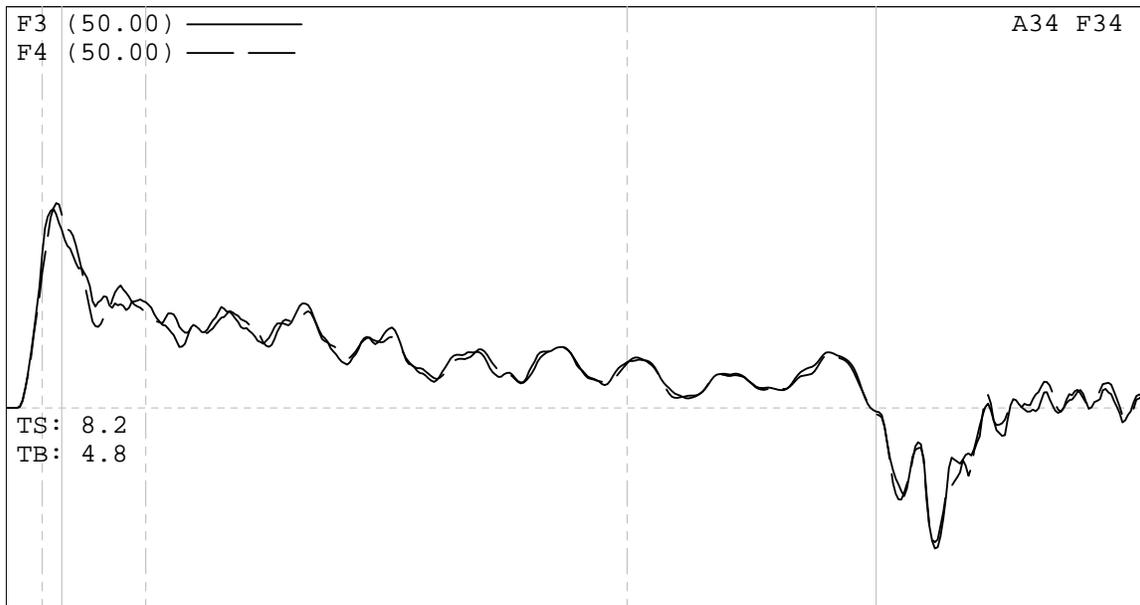
#### 3.1 Energy Transfer Ratio (ETR) and Hammer Efficiency Correction (CE)

Based on our testing and subsequent analysis, CME-55 (Serial Number 359485) has an **ETR of 80.0% ± 1.53%**. Based on this ETR, the hammer efficiency correction (**C<sub>E</sub>**) is **1.33**.

## **Exhibit A-1 Representative Blow**

CME-55 CAL JUNE 2016

B-1, 43.5 ft to 45 ft



Project Information

PROJECT: CME-55 CAL JUNE 2016  
 PILE NAME: B-1, 43.5 ft to 45 ft  
 DESCR: CME-55, SERIAL# 359485  
 OPERATOR: CF  
 FILE: B-1, 43.5-45.W01  
 6/14/2016 4:50:51 PM  
 Blow Number 9

Quantity Results

FMX 24.83 kips  
 VMX 17.67 f/s  
 EFV 0.28 k-ft  
 ETR 79.0 (%)  
 BPM 53.30 bpm  
 DMX 0.79 in  
 CSX 21.05 ksi  
 DFN 0.67 in  
 TSX 15.40 ksi

Pile Properties

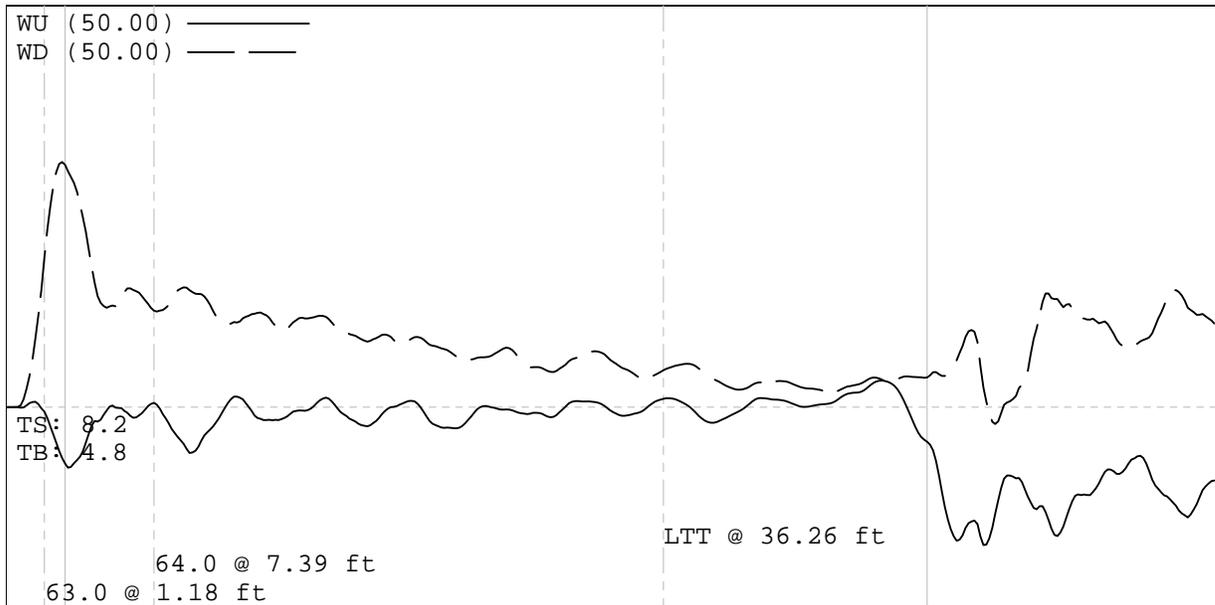
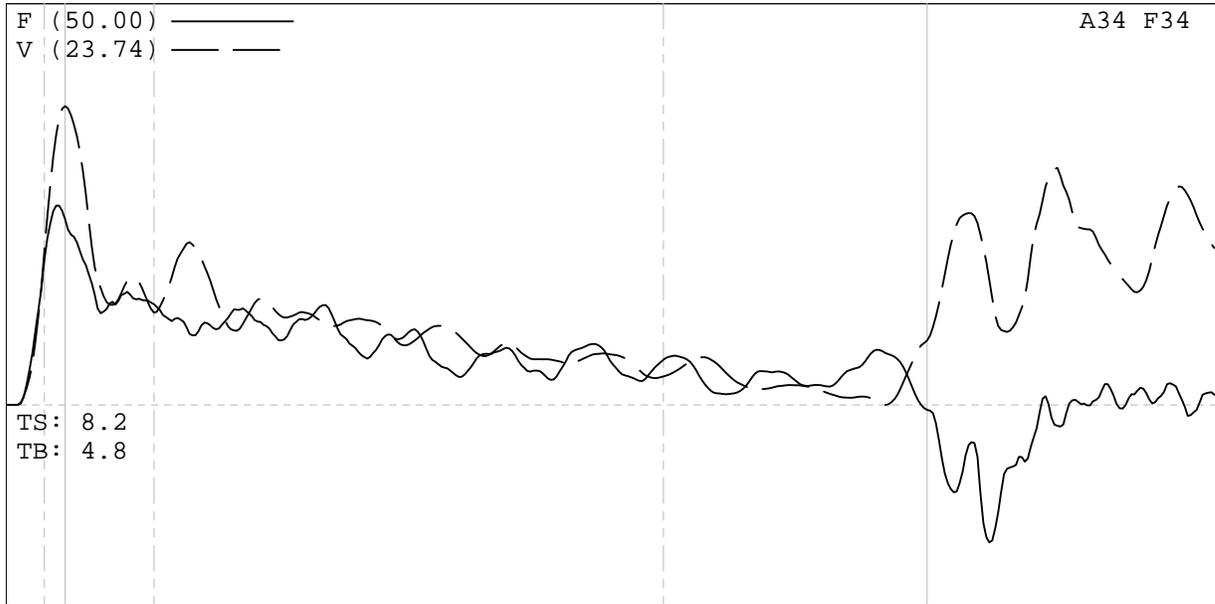
LE 48.83 ft  
 AR 1.18 in<sup>2</sup>  
 EM 30000 ksi  
 SP 0.492 k/ft<sup>3</sup>  
 WS 16807.9 f/s  
 EA/C 2.1 ksec/ft  
 2L/C 5.82 ms  
 JC []  
 LP 44.00 ft

Sensors

F3: [AWJ 1] 211.53 (1)  
 F4: [AWJ 2] 211.77 (1)  
 A3: [K1737] 342 mv/5000g's (1)  
 A4: [K1732] 360 mv/5000g's (1)  
 CLIP: OK

CME-55 CAL JUNE 2016

B-1, 43.5 ft to 45 ft



Project Information

PROJECT: CME-55 CAL JUNE 2016  
PILE NAME: B-1, 43.5 ft to 45 ft  
DESCR: CME-55, SERIAL# 359485  
OPERATOR: CF  
FILE: B-1, 43.5-45.W01  
6/14/2016 4:50:51 PM  
Blow Number 9

Quantity Results

FMX 24.83 kips  
VMX 17.67 f/s  
EFV 0.28 k-ft  
ETR 79.0 (%)  
BPM 53.30 bpm  
DMX 0.79 in  
CSX 21.05 ksi  
DFN 0.67 in  
TSX 15.40 ksi

Pile Properties

LE 48.83 ft  
AR 1.18 in<sup>2</sup>  
EM 30000 ksi  
SP 0.492 k/ft<sup>3</sup>  
WS 16807.9 f/s  
EA/C 2.1 ksec/ft  
2L/C 5.82 ms  
JC []  
LP 44.00 ft

Sensors

F3: [AWJ 1] 211.53 (1)  
F4: [AWJ 2] 211.77 (1)  
A3: [K1737] 342 mv/5000g's (1)  
A4: [K1732] 360 mv/5000g's (1)  
CLIP: OK

## **Exhibit A-2 PDA Equipment Calibrations**

# Certificate of Calibration

**Pile Dynamics, Inc. certifies that the**

**Pile Driving Analyzer®, Model PAX**

**Serial Number: 3766L**

was calibrated on 28 March 2014

using a PDA Calibration Box whose output was calibrated with test equipment traceable to NIST.

This certificate is valid for 2 years from above date.



Tested by: 



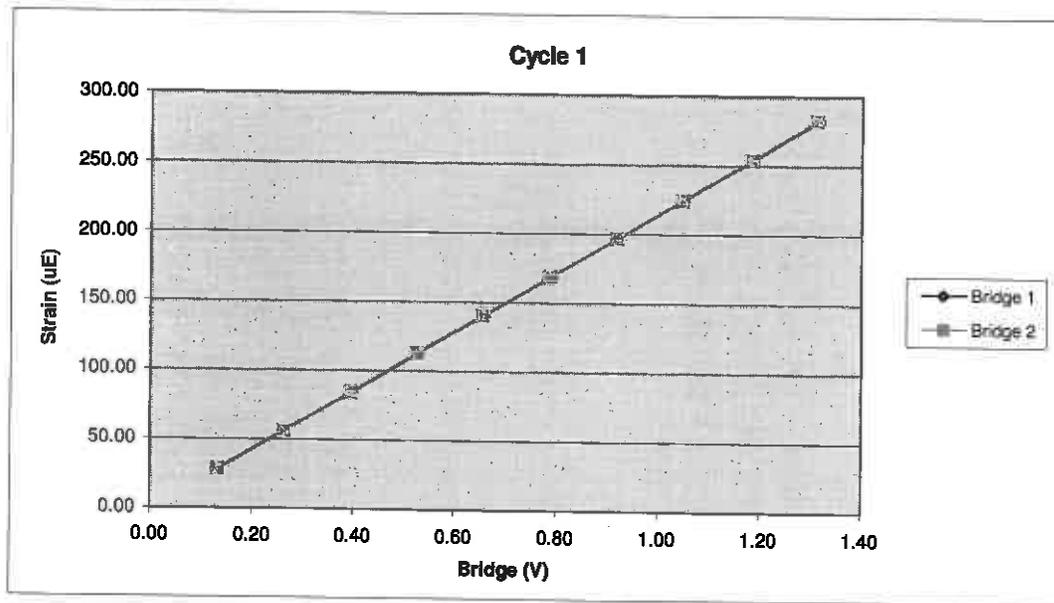
Pile Dynamics, Inc.  
30725 Aurora Road  
Cleveland, Ohio 44139 USA

# March 2015

267AWJ		Cycle 1		
Sample	Force (lb)	Strain ( $\mu$ E)	Bridge 1 (V)	Bridge 2 (V)
1	0.00	0.00	0.00	0.00
2	989.85	28.25	0.13	0.13
3	1984.04	55.90	0.26	0.26
4	2984.15	84.22	0.40	0.39
5	3983.07	112.75	0.53	0.53
6	4967.80	140.04	0.66	0.65
7	5960.01	168.66	0.79	0.79
8	6950.26	196.46	0.92	0.92
9	7933.41	224.50	1.05	1.05
10	8967.62	253.80	1.18	1.18
11	9960.63	282.25	1.31	1.31

Bridge 1		Bridge 2	
Force Calibration (lb/V)	7580.05	Force Calibration (lb/V)	7594.00
Offset	-6.55	Offset	-12.19
Correlation	0.999997	Correlation	0.999996
Strain Calibration ( $\mu$ E/V)	214.70	Strain Calibration ( $\mu$ E/V)	215.09
Offset	-0.38	Offset	-0.54
Correlation	0.999994	Correlation	0.999993

Force Strain Calibration	
EA (Kips)	35305.52
Offset	6.95
Correlation	0.999996

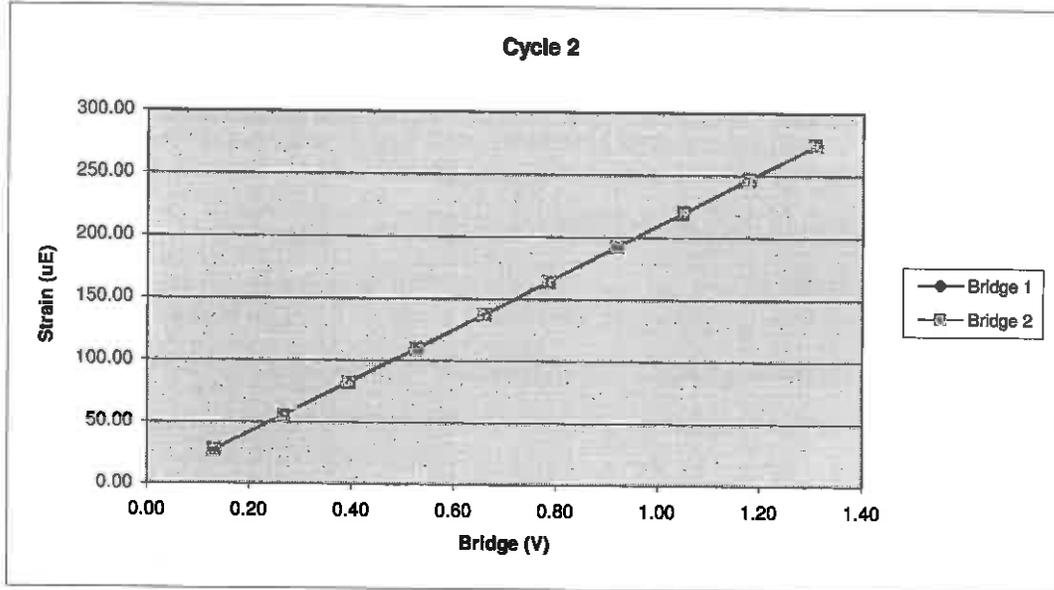


March 2015

267AWJ		Cycle 2		
Sample	Force (lb)	Strain ( $\mu E$ )	Bridge 1 (V)	Bridge 2 (V)
1	0.00	0.00	0.00	0.00
2	985.91	27.42	0.13	0.13
3	2013.22	55.80	0.27	0.27
4	2976.66	82.22	0.39	0.39
5	3986.03	109.72	0.53	0.53
6	4991.06	137.06	0.66	0.66
7	5966.52	164.10	0.79	0.79
8	6974.31	192.21	0.92	0.92
9	7944.65	219.38	1.05	1.05
10	8931.15	246.44	1.18	1.18
11	9931.65	273.99	1.31	1.31

Bridge 1		Bridge 2	
Force Calibration (lb/V)	7594.28	Force Calibration (lb/V)	7600.39
Offset	-7.07	Offset	-19.16
Correlation	0.999997	Correlation	0.999998
Strain Calibration ( $\mu E/V$ )	209.38	Strain Calibration ( $\mu E/V$ )	209.55
Offset	-0.18	Offset	-0.51
Correlation	0.999994	Correlation	0.999993

Force Strain Calibration	
EA (Kips)	36269.26
Offset	-0.51
Correlation	0.999993

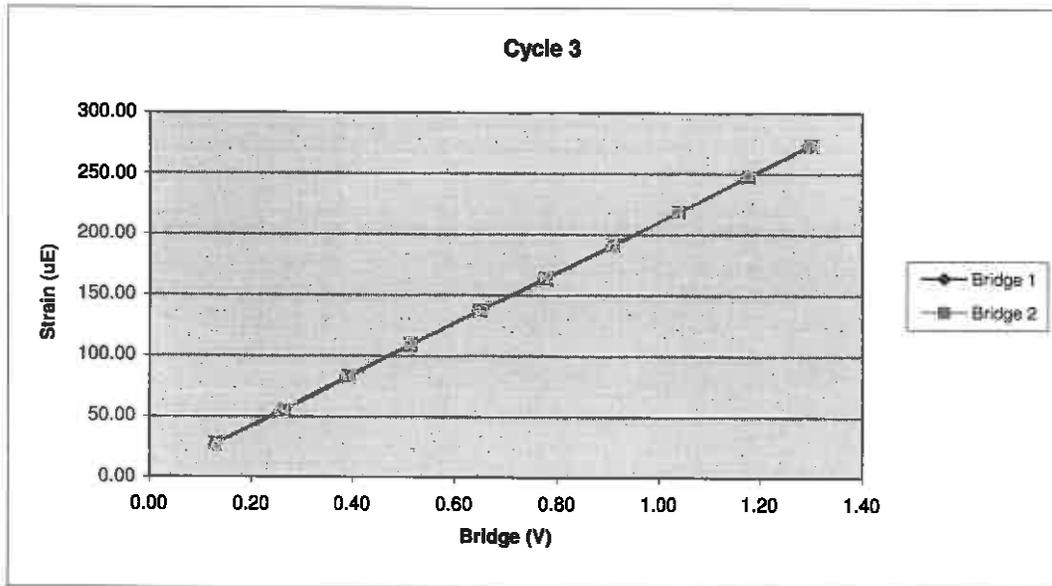


March 2015

267AWJ		Cycle 3		
Sample	Force (lb)	Strain ( $\mu E$ )	Bridge 1 (V)	Bridge 2 (V)
1	0.00	0.00	0.00	0.00
2	978.02	27.23	0.13	0.13
3	1983.45	54.94	0.26	0.26
4	2969.76	82.48	0.39	0.39
5	3927.08	108.47	0.51	0.51
6	4947.10	136.99	0.65	0.65
7	5912.50	163.76	0.77	0.78
8	6922.07	191.13	0.91	0.91
9	7898.71	218.67	1.04	1.04
10	8946.33	247.50	1.17	1.18
11	9882.76	273.33	1.30	1.30

Bridge 1		Bridge 2	
Force Calibration (lb/V)	7616.04	Force Calibration (lb/V)	7621.58
Offset	10.36	Offset	-12.46
Correlation	0.999996	Correlation	0.999993
Strain Calibration ( $\mu E/V$ )	210.51	Strain Calibration ( $\mu E/V$ )	210.66
Offset	0.46	Offset	-0.17
Correlation	0.999997	Correlation	0.999993

Force Strain Calibration	
EA (Kips)	36178.74
Offset	-6.36
Correlation	0.999997



Bridge Excitation (V) 5  
Shunt Resistor (ohm) 60.4k

Calibration Factors	267AWJ		
Bridge 1 ( $\mu\text{E/V}$ )	211.53	Bridge 2 ( $\mu\text{E/V}$ )	211.77
EA Factor (Kips)	35917.84	Area ( $\text{in}^2$ )	1.20

Calibrated by: 

Calibrated Date: 3/30/2015

Pile Dynamics Inc  
30725 Aurora Rd  
Solon, OH 44139

Traceable to N.I.S.T.

QBTA: ON [ALT-F1/BB=60]

File Dynamics, Inc.

TG F2 DPF

File Dynamics  
19-Sep-14 08:34

FS — BN 71  
10 SL 124/ 3440/ 2

PJ: PN: HOPBAR

A 4 -- US  
F 2 3.3

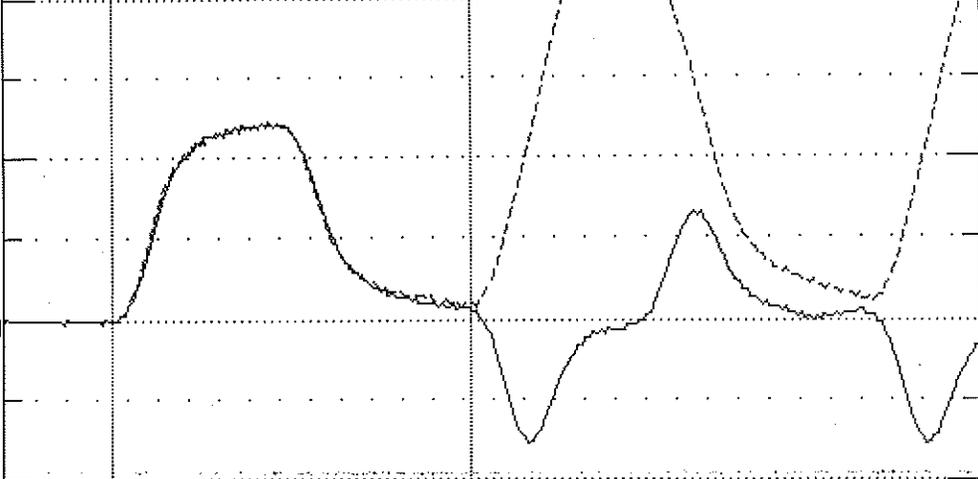
LE 39.6 ft  
AR 1.7 in2  
EM 30000 Ksi  
SP 0.492 K/ft3  
WS 16810 ft/s  
WC 16862 ft/s

JC 0.40  
FM 1.00  
UM 1.00

EA/C 30.3 Ks/ft  
UN ~~KIPS=0.0~~  
FR 20000 MB 30

DL -44  
UT -1  
PK 1 TM-PEAK

F1/2 500/ 213  
F3/4 213/ 213  
A1/2 999/ 999  
A3/4 999/ 342



TS 12 E B PD: k1737 LP 0.00 ft  
TB 8.0 T1 9.4 2L/C 4.7 UA 1000 UE 1022 LI 1.0

ACCEPT SQ-OFF FL-OFF PR-OFF  
VMX= 3.9 FMX= 62 AMX= 120  
EMX= 0.2 MEX= 121 FVP= 1.00



contact File Dynamics USA  
with your questions  
tel USA - 216 - 831- 6131  
fax USA - 216 - 831- 0916

ACCELEROMETER CALIBRATION N.I.S.T. Traceable  
SERIAL NUMBER: K1737  
CALIBRATION FACTOR: 0.0684 mV/g  
PAK (\*5000): 342 DATE: 19SEPT14  
PDA OPERATOR: M.W.M.

←-PIEZORESISTIVE

OP: Iain Iver:4.051

PIEZOELECTRIC-→

Smart Sensor

Smart Chip Programmed By M.W.M. on 19SEPT14 CRC Value 95C7

QBTA: DN [ALT-F1/BB=60]

Pile Dynamics, Inc.

TG F2 DPF

File Dynamics 19-Sep-14 08:37	FS 10	BN 76 SL 128/ 3440/ 99	PJ: PN: HOPBAR	A 4 -- US F 2 3.3			
LE 39.6 ft AR 1.7 in2 EM 30000 Ksi SP 0.492 K/ft3 WS 16810 ft/s WC 16862 ft/s							
JC 0.40 FM 1.00 UM 1.00							
EA/C 30.3 Ks/ft UN KIPS*0.1 FR 20000 MB 30							
DL -38 UT -1 PK 1 TM-PEAK							
F1/2 500/ 213 F3/4 213/ 213 A1/2 999/ 999 A3/4 999/ 360							
TS 12 TB 8.0					E B PD: k1732 TI 9.6 2L/C 4.7	VA 1000	LP 0.00 ft LI 1.0
ACCEPT SQ-OFF FL-OFF PR-OFF							
contact Pile Dynamics USA with your questions tel USA - 216 - 831- 6131 fax USA - 216 - 831- 0916							
ACCELEROMETER CALIBRATION N.I.S.T. Traceable SERIAL NUMBER: K1732 CALIBRATION FACTOR: .072 mV/g PAK (*5000): 360 DATE: 19SEPT14 PDA OPERATOR: J.M.W.							

UMX= 4.2 FMX= 65 AMX= 129  
EMX= 0.3 MEX= 127 FVP= 1.00

OP: laine [ver:4.05]

Smart Sensor

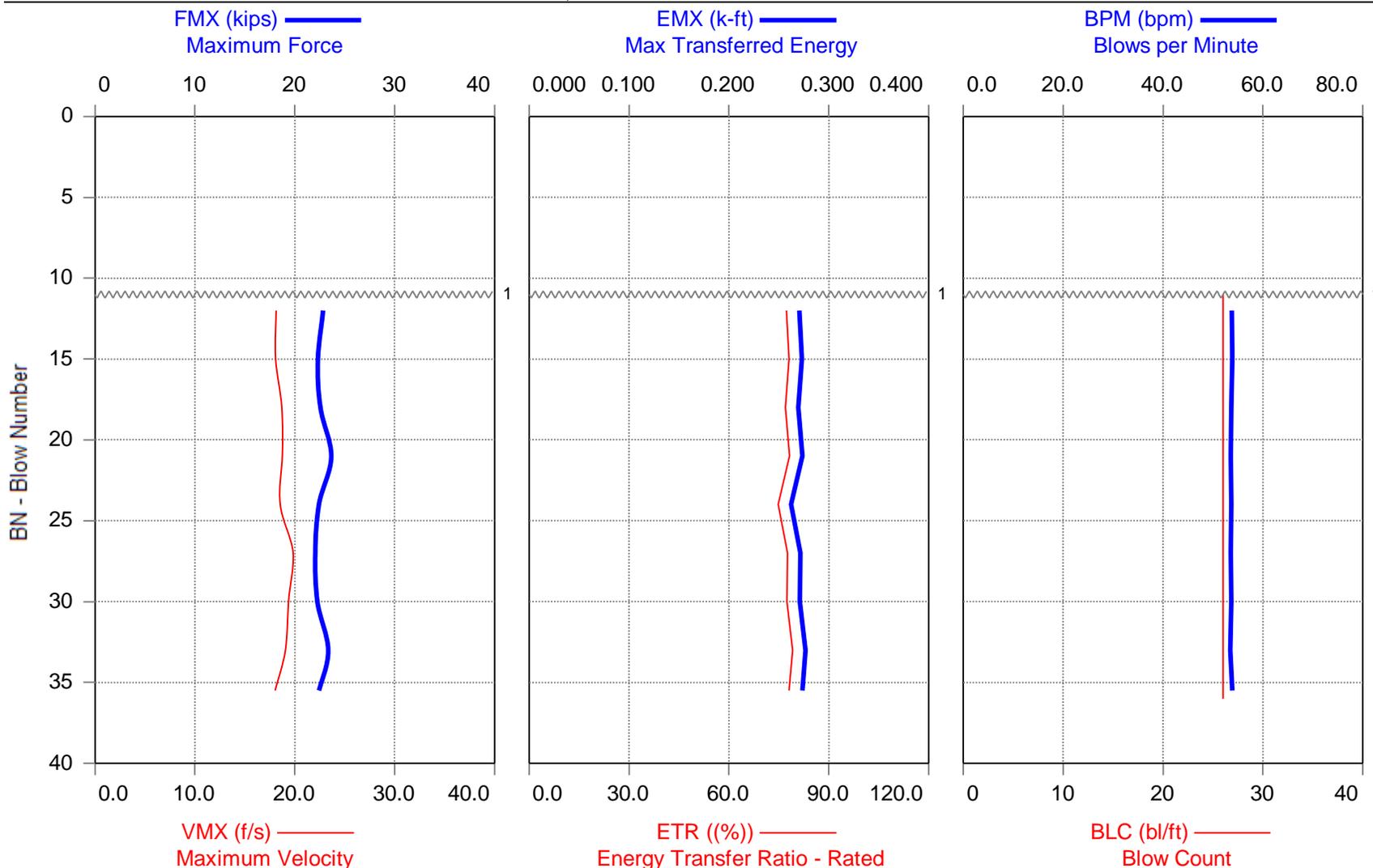
Smart Chip Programmed By J.M.W. on 19SEPT14 CRC Value 2D4A

## **Exhibit A-3 SPT Calibration Data Plots**



CME-55 CAL JUNE 2016 - B-1, 48.5 ft to 50 ft

**CME-55, SERIAL# 359485**



1 - Blows 1-10 = Seating Blows, Blow 11 = First Blow of N value

CME-55 CAL JUNE 2016 - B-1, 48.5 ft to 50 ft  
OP: CF

CME-55, SERIAL# 359485  
Date: 14-June-2016

AR: 1.18 in<sup>2</sup>  
LE: 53.83 ft  
WS: 16,807.9 f/s

SP: 0.492 k/ft<sup>3</sup>  
EM: 30,000 ksi  
JC: 0.00 []

FMX: Maximum Force  
VMX: Maximum Velocity  
EMX: Max Transferred Energy  
ETR: Energy Transfer Ratio - Rated

BPM: Blows per Minute  
DMX: Maximum Displacement  
CSX: Max Measured Compr. Stress  
DFN: Final Displacement

BL#	Depth ft	BLC bl/ft	FMX kips	VMX f/s	EMX k-ft	ETR (%)	BPM bpm	DMX in	CSX ksi	DFN in
11	49.04	26	23	18.2	0.267	76.4	54.0	0.63	19.5	0.46
12	49.08	26	23	18.1	0.269	76.8	53.6	0.63	19.3	0.46
13	49.12	26	23	18.1	0.275	78.5	53.6	0.63	19.3	0.46
14	49.15	26	22	18.1	0.277	79.3	53.3	0.62	19.1	0.46
15	49.19	26	23	18.1	0.273	78.0	53.8	0.61	19.1	0.46
16	49.23	26	22	18.0	0.269	77.0	54.4	0.60	18.6	0.46
17	49.27	26	23	19.4	0.278	79.5	53.3	0.59	19.7	0.46
18	49.31	26	22	18.1	0.268	76.6	53.4	0.56	18.8	0.46
19	49.35	26	22	18.6	0.261	74.7	54.4	0.57	18.9	0.46
20	49.38	26	25	19.3	0.280	79.9	52.9	0.58	21.2	0.46
21	49.42	26	22	18.1	0.267	76.3	54.4	0.60	18.8	0.46
22	49.46	26	24	18.9	0.275	78.5	53.5	0.60	20.1	0.46
23	49.50	26	23	19.3	0.266	75.9	53.4	0.58	19.4	0.46
24	49.54	26	22	18.2	0.269	76.9	53.5	0.60	19.0	0.46
25	49.58	26	22	18.1	0.251	71.7	54.2	0.54	18.6	0.46
26	49.62	26	22	19.7	0.269	76.8	53.4	0.59	18.9	0.46
27	49.65	26	21	20.4	0.272	77.8	53.5	0.59	17.7	0.46
28	49.69	26	23	19.3	0.274	78.2	53.9	0.58	19.4	0.46
29	49.73	26	23	19.1	0.274	78.2	53.5	0.60	19.4	0.46
30	49.77	26	21	20.5	0.265	75.7	53.6	0.58	18.0	0.46
31	49.81	26	23	18.5	0.275	78.4	54.0	0.60	19.3	0.46
32	49.85	26	23	19.3	0.275	78.6	53.0	0.60	19.4	0.46
33	49.88	26	24	19.1	0.274	78.2	54.3	0.57	19.9	0.46
34	49.92	26	24	18.7	0.281	80.4	52.9	0.60	20.0	0.46
35	49.96	26	22	17.8	0.271	77.4	54.3	0.59	18.7	0.46
36	50.00	26	23	18.2	0.276	78.8	53.5	0.60	19.3	0.46
Average			23	18.7	0.271	77.5	53.7	0.59	19.2	0.46
Std. Dev.			1	0.7	0.006	1.8	0.4	0.02	0.7	0.00
Maximum			25	20.5	0.281	80.4	54.4	0.63	21.2	0.46
Minimum			21	17.8	0.251	71.7	52.9	0.54	17.7	0.46

Total number of blows analyzed: 26

BL# Sensors

11-36 F3: [AWJ 1] 211.5 (1.00); F4: [AWJ 2] 211.8 (1.00); A3: [K1737] 342.0 (1.00);  
A4: [K1732] 360.0 (1.00)

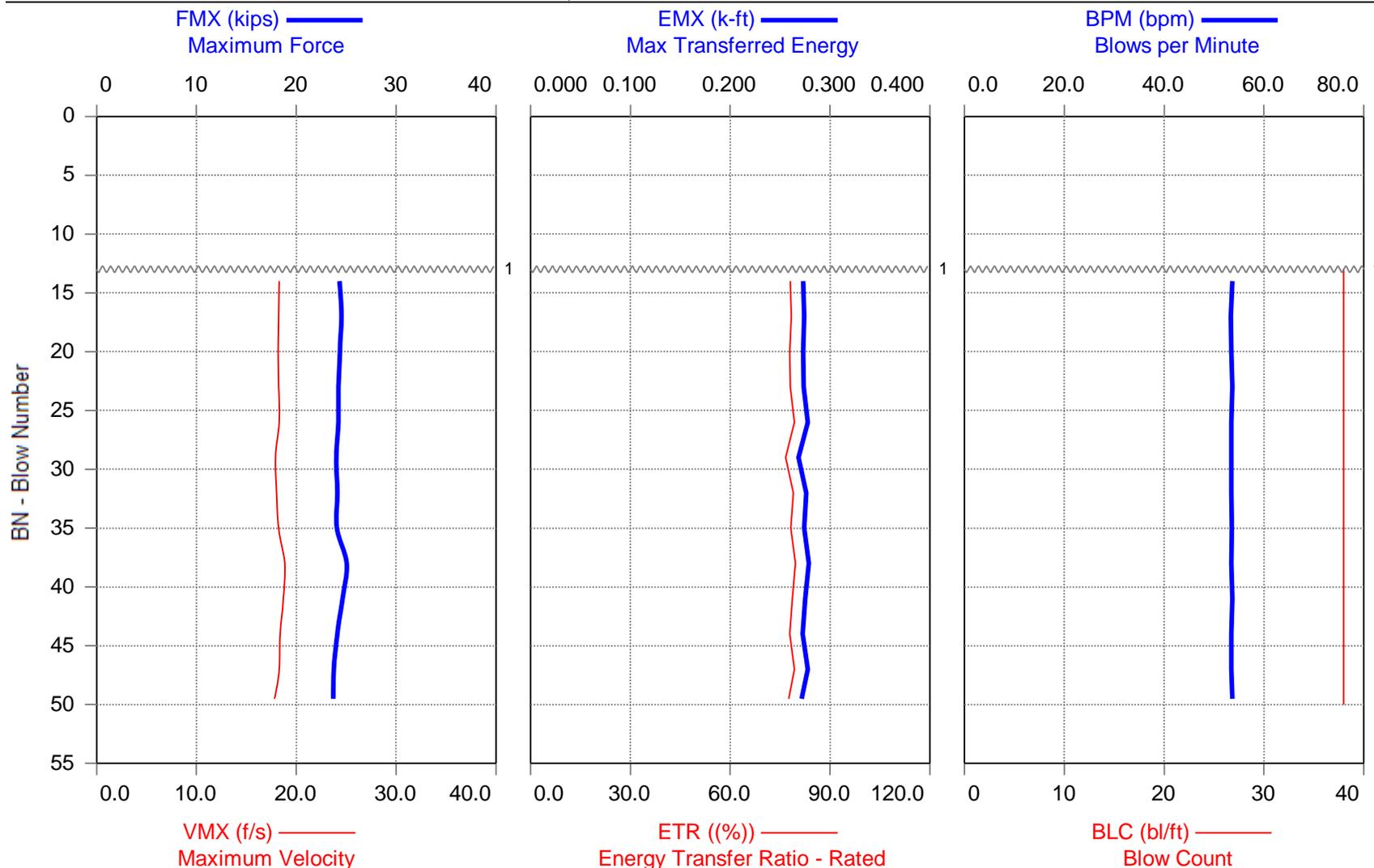
BL# Comments

11 Blows 1-10 = Seating Blows, Blow 11 = First Blow of N value



CME-55 CAL JUNE 2016 - B-1, 45.5 ft to 47 ft

**CME-55, SERIAL# 359485**



1 - Blows 1-12 = Seating Blows, Blow 13 = First blow of N value

CME-55 CAL JUNE 2016 - B-1, 45.5 ft to 47 ft  
OP: CF

CME-55, SERIAL# 359485  
Date: 14-June-2016

AR: 1.18 in<sup>2</sup>  
LE: 50.83 ft  
WS: 16,807.9 f/s

SP: 0.492 k/ft<sup>3</sup>  
EM: 30,000 ksi  
JC: 0.00 []

FMX: Maximum Force  
VMX: Maximum Velocity  
EMX: Max Transferred Energy  
ETR: Energy Transfer Ratio - Rated

BPM: Blows per Minute  
DMX: Maximum Displacement  
CSX: Max Measured Compr. Stress  
DFN: Final Displacement

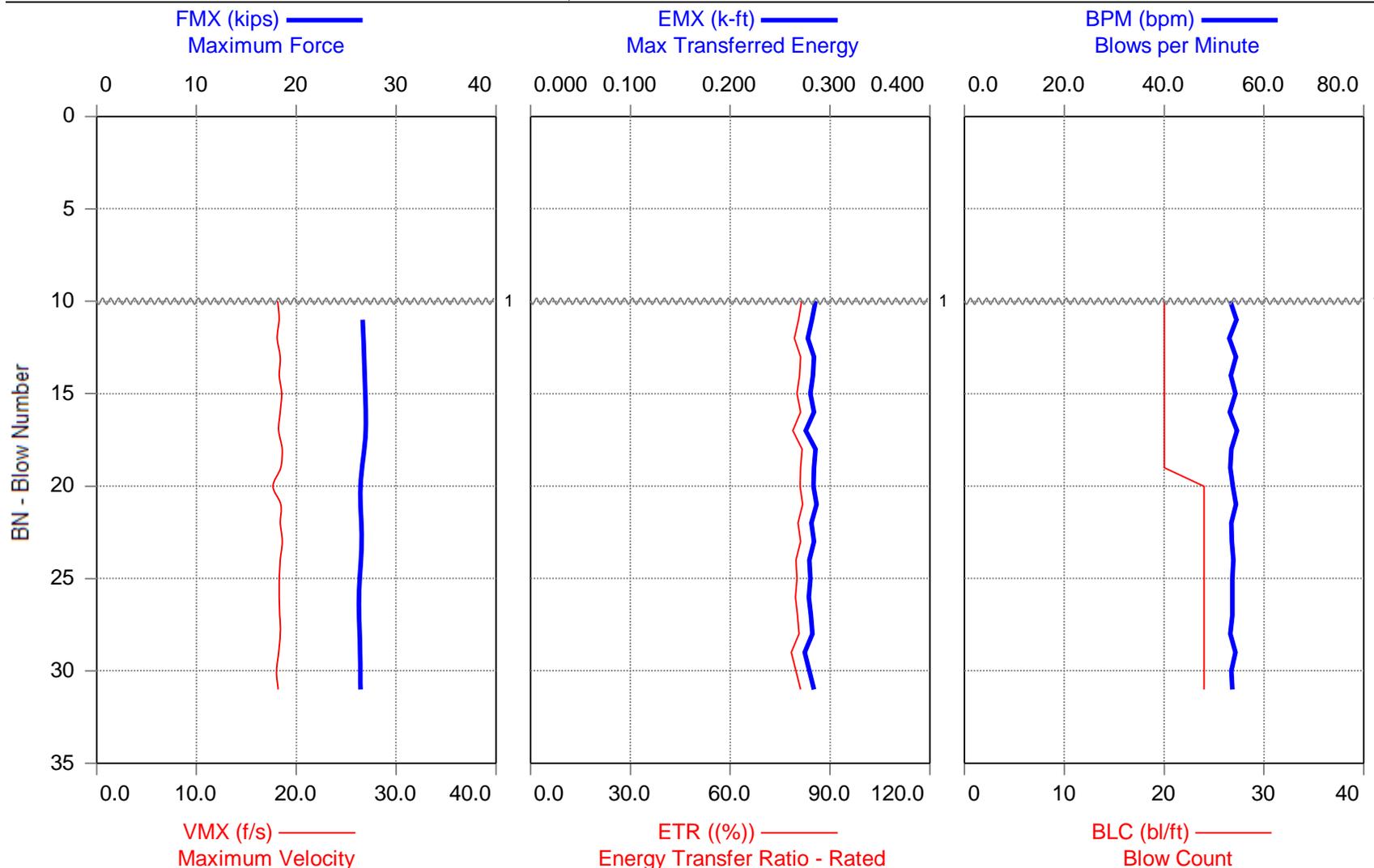
BL#	Depth ft	BLC bl/ft	FMX kips	VMX f/s	EMX k-ft	ETR (%)	BPM bpm	DMX in	CSX ksi	DFN in
13	46.03	38	24	17.8	0.263	75.2	54.2	0.48	20.1	0.32
14	46.05	38	26	19.3	0.288	82.2	53.1	0.51	21.9	0.31
15	46.08	38	23	17.8	0.269	76.7	53.8	0.50	19.9	0.32
16	46.11	38	25	18.3	0.274	78.3	53.3	0.50	21.1	0.31
17	46.13	38	24	18.1	0.274	78.2	53.2	0.50	20.6	0.32
18	46.16	38	24	18.3	0.275	78.6	53.5	0.49	20.6	0.32
19	46.18	38	24	17.9	0.270	77.1	53.6	0.49	20.2	0.32
20	46.21	38	23	17.5	0.265	75.8	54.2	0.49	19.7	0.31
21	46.24	38	26	19.1	0.283	80.9	52.7	0.50	22.0	0.31
22	46.26	38	23	17.4	0.266	76.0	54.0	0.48	19.5	0.32
23	46.29	38	25	18.6	0.276	78.9	53.7	0.49	21.0	0.31
24	46.32	38	25	18.7	0.278	79.5	53.4	0.49	21.2	0.31
25	46.34	38	23	17.7	0.269	76.9	53.9	0.48	19.6	0.32
26	46.37	38	24	18.6	0.276	78.8	52.5	0.49	20.5	0.32
27	46.39	38	25	18.5	0.289	82.5	54.1	0.54	21.4	0.32
28	46.42	38	25	18.5	0.275	78.5	53.4	0.49	21.2	0.32
29	46.45	38	23	17.3	0.265	75.6	53.2	0.48	19.8	0.32
30	46.47	38	24	17.9	0.266	76.0	53.9	0.49	20.0	0.32
31	46.50	38	25	18.4	0.274	78.3	53.7	0.48	21.2	0.31
32	46.53	38	24	17.8	0.273	78.0	53.0	0.48	20.2	0.31
33	46.55	38	23	17.8	0.282	80.6	53.5	0.53	19.9	0.32
34	46.58	38	26	18.9	0.279	79.8	53.2	0.50	21.7	0.32
35	46.61	38	23	17.7	0.266	76.0	54.9	0.48	19.7	0.32
36	46.63	38	23	18.1	0.276	79.0	52.7	0.50	19.7	0.32
37	46.66	38	26	18.7	0.274	78.3	53.7	0.49	21.9	0.31
38	46.68	38	25	19.5	0.286	81.7	53.7	0.50	21.5	0.32
39	46.71	38	24	18.3	0.276	78.8	53.1	0.49	20.2	0.32
40	46.74	38	26	18.8	0.274	78.2	53.8	0.48	21.7	0.32
41	46.76	38	25	19.3	0.282	80.7	53.5	0.49	21.4	0.32
42	46.79	38	23	18.1	0.270	77.0	53.7	0.48	19.6	0.32
43	46.82	38	24	18.6	0.274	78.4	53.2	0.49	20.5	0.32
44	46.84	38	23	17.7	0.270	77.1	53.2	0.49	19.4	0.31
45	46.87	38	25	18.8	0.274	78.2	53.9	0.50	21.4	0.32
46	46.89	38	23	18.0	0.277	79.1	53.5	0.50	19.6	0.32
47	46.92	38	25	19.1	0.284	81.2	53.1	0.51	21.3	0.32
48	46.95	38	23	17.8	0.272	77.7	53.9	0.49	19.5	0.31
49	46.97	38	25	18.4	0.277	79.0	53.6	0.50	21.1	0.32
50	47.00	38	23	17.3	0.267	76.2	53.7	0.48	19.1	0.32
	Average		24	18.3	0.274	78.4	53.5	0.49	20.6	0.32
	Std. Dev.		1	0.6	0.006	1.8	0.5	0.01	0.8	0.00
	Maximum		26	19.5	0.289	82.5	54.9	0.54	22.0	0.32
	Minimum		23	17.3	0.263	75.2	52.5	0.48	19.1	0.31

Total number of blows analyzed: 38



CME-55 CAL JUNE 2016 - B-1, 40.5 ft to 42 ft

**CME-55, SERIAL# 359485**



1 - Blows 1-9 = Seating blows, Blow 10 = First blow of N value

CME-55 CAL JUNE 2016 - B-1, 40.5 ft to 42 ft  
OP: CF

CME-55, SERIAL# 359485  
Date: 14-June-2016

AR: 1.18 in<sup>2</sup> SP: 0.492 k/ft<sup>3</sup>  
LE: 45.83 ft EM: 30,000 ksi  
WS: 16,807.9 f/s JC: 0.00 []

FMX: Maximum Force BPM: Blows per Minute  
VMX: Maximum Velocity DMX: Maximum Displacement  
EMX: Max Transferred Energy CSX: Max Measured Compr. Stress  
ETR: Energy Transfer Ratio - Rated DFN: Final Displacement

BL#	Depth ft	BLC bl/ft	FMX kips	VMX f/s	EMX k-ft	ETR (%)	BPM bpm	DMX in	CSX ksi	DFN in
10	41.05	20	27	18.2	0.285	81.5	53.2	0.81	22.5	0.60
11	41.10	20	27	18.3	0.282	80.5	54.5	0.79	23.0	0.60
12	41.15	20	26	18.1	0.278	79.3	53.0	0.75	22.2	0.60
13	41.20	20	27	18.4	0.284	81.1	54.4	0.76	22.8	0.60
14	41.25	20	27	18.3	0.283	80.8	53.3	0.71	22.6	0.60
15	41.30	20	27	18.5	0.280	80.1	54.3	0.71	22.8	0.60
16	41.35	20	27	18.4	0.284	81.2	53.1	0.68	22.8	0.60
17	41.40	20	27	18.2	0.276	78.8	54.6	0.64	22.7	0.60
18	41.45	20	27	18.6	0.286	81.6	53.4	0.65	23.1	0.60
19	41.50	20	27	18.4	0.284	81.1	53.2	0.64	22.9	0.60
20	41.54	24	26	17.7	0.284	81.0	53.8	0.63	22.2	0.50
21	41.58	24	26	18.5	0.286	81.8	54.4	0.62	22.1	0.50
22	41.63	24	27	18.4	0.281	80.4	53.4	0.61	22.8	0.50
23	41.67	24	27	18.6	0.284	81.1	53.6	0.61	22.8	0.50
24	41.71	24	26	18.4	0.279	79.7	53.9	0.60	21.9	0.50
25	41.75	24	26	18.3	0.280	80.1	53.7	0.60	22.2	0.50
26	41.79	24	26	18.3	0.279	79.6	53.7	0.59	22.2	0.50
27	41.83	24	26	18.4	0.281	80.3	53.7	0.59	22.4	0.50
28	41.88	24	27	18.4	0.283	80.7	53.2	0.59	22.7	0.50
29	41.92	24	26	18.2	0.274	78.4	54.3	0.57	22.4	0.50
30	41.96	24	26	18.0	0.279	79.8	53.5	0.59	22.0	0.50
31	42.00	24	26	18.2	0.284	81.2	53.7	0.59	22.4	0.50
Average			27	18.3	0.282	80.5	53.7	0.65	22.5	0.55
Std. Dev.			0	0.2	0.003	0.9	0.5	0.07	0.3	0.05
Maximum			27	18.6	0.286	81.8	54.6	0.81	23.1	0.60
Minimum			26	17.7	0.274	78.4	53.0	0.57	21.9	0.50

Total number of blows analyzed: 22

BL# Sensors

10-31 F3: [AWJ 1] 211.5 (1.00); F4: [AWJ 2] 211.8 (1.00); A3: [K1737] 342.0 (1.00);  
A4: [K1732] 360.0 (1.00)

BL# Comments

10 Blows 1-9 = Seating blows, Blow 10 = First blow of N value

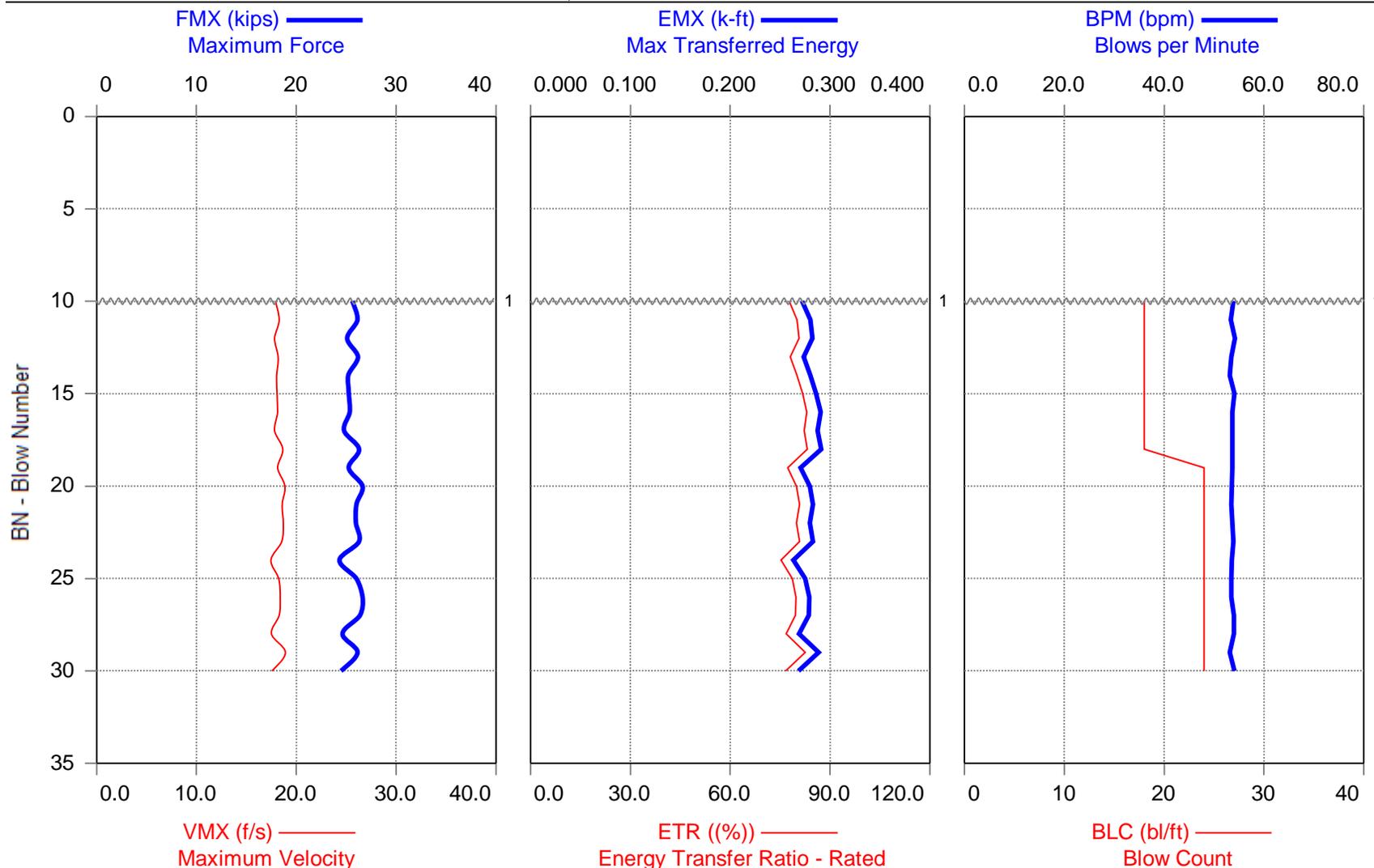
Time Summary

Drive 26 seconds 4:41 PM - 4:42 PM BN 7 - 31



CME-55 CAL JUNE 2016 - B-1, 43.5 ft to 45 ft

**CME-55, SERIAL# 359485**



1 - Blows 1-9 = Seating Blows, Blow 10 = First blow of N value



**Exhibit A-4    Field Log**

# Terracon

## SPT HAMMER CALIBRATION FIELD WORKSHEET

ARRIVAL TIME: 0:15  
 DEPART TIME: 5:15  
 TOTAL TRAVEL: —  
 TOTAL TIME: — 3 hrs  
 CLIENT REP: Ken Zou  
 MILEAGE: —

PROJECT NAME: None  
 PROJECT NO.: None  
 BORING NO.: B-1 (Test)  
 CLIENT: Terracon

DATE: 6/14/2016  
 TERRACON REP: Ken Zou  
 PDA MODEL/SN: PAX 3766Z  
 DRILLING CONT.: Terracon

### DRILL RIG DATA

Type/Transport: ATV-Track  
 Manufacturer: CME  
 Model No.: SS  
 Serial No.: 359485  
 Year Built: Aug 2008  
 Modifications: None  
 Maint. Schedule: As-Required

### SPT HAMMER DATA

Type: Auto  
 Manufacturer: CME  
 Lifting Mechanism: Chain  
 Model No.: —  
 Serial No.: —  
 Hammer Weight: 140 lbs  
 Hammer Operator(s): Grig Fednychowski

### PDA INPUT DATA

Operator: **OP** RSZ  
 Project No./Location: **PJ** Columbia Office  
 Rig Model & SN: **PN** CME-SS  
 Hammer Type, LM, Rods: **PD** Auto  
 Drill Rod Area (in<sup>2</sup>): **AR** 1.18

Elastic Modulus (ksi): **EM** 30,000 ksi  
 Specific Weight (kips/ft<sup>3</sup>): **SP** 0.492  
 Wave Speed (ft/sec): **WS** 16,808  
 Increment Length (ft): **LI** —  
 Sampling Freq. (kHz): **FR** 50 kHz

### TRANSDUCER INFORMATION

Gage	SN	Calibration
F1:	<u>267AWS1</u>	<u>211.59</u>
F2:	<u>267AWS2</u>	<u>211.77</u>
A1:	<u>K1737</u>	<u>342</u>
A2:	<u>K1732</u>	<u>360</u>

### NOTES:

Sampler 34' (283')  
 Rod 1'  
Total 3.83'

### SPT TESTING INFORMATION

Start Time	Soil	Depth (ft)		LE (ft)	Rods & Lengths	PDA Blows		SPT Blows			
		Start	End			Start	End	1st 6"	2nd 6"	3rd 6"	4th 6"
2:47	SP	23.5	25	28.83	5(5')	0	50	13	19	22	
2:57	SP	28.5	30	33.83	6(5')	0	38	10	14	17	
					"RAIN Delay"						
3:12	SP	33.5	35	38.83	7(5')	0	38	10	12	14	
4:26	SP	38.5	40	43.83	8(5')	0	42	10	13	16	
4:40	SP	40.5	42	45.83	8(5')+1(2')	0	27	9	10	12	
4:51	SP	43.5	45	48.83	9(5')	0	29	9	9	12	

PICTURE NUMBERS AND INFO:

# Terracon

## SPT HAMMER CALIBRATION FIELD WORKSHEET

ARRIVAL TIME: \_\_\_\_\_  
 DEPART TIME: \_\_\_\_\_  
 TOTAL TRAVEL: \_\_\_\_\_  
 TOTAL TIME: \_\_\_\_\_  
 CLIENT REP: \_\_\_\_\_  
 MILEAGE: \_\_\_\_\_

PROJECT NAME: \_\_\_\_\_  
 PROJECT NO.: \_\_\_\_\_  
 BORING NO.: \_\_\_\_\_  
 CLIENT: \_\_\_\_\_

DATE: \_\_\_\_\_  
 TERRACON REP: \_\_\_\_\_  
 PDA MODEL/SN: \_\_\_\_\_  
 DRILLING CONT.: \_\_\_\_\_

### DRILL RIG DATA

Type/Transport: \_\_\_\_\_  
 Manufacturer: \_\_\_\_\_  
 Model No.: \_\_\_\_\_  
 Serial No.: \_\_\_\_\_  
 Year Built: \_\_\_\_\_  
 Modifications: \_\_\_\_\_  
 Maint. Schedule: \_\_\_\_\_

### SPT HAMMER DATA

Type: \_\_\_\_\_  
 Manufacturer: \_\_\_\_\_  
 Lifting Mechanism: \_\_\_\_\_  
 Model No.: \_\_\_\_\_  
 Serial No.: \_\_\_\_\_  
 Hammer Weight: \_\_\_\_\_  
 Hammer Operator(s): \_\_\_\_\_

### PDA INPUT DATA

Operator: **OP** \_\_\_\_\_ Elastic Modulus (ksi): **EM** \_\_\_\_\_  
 Project No./Location: **PJ** \_\_\_\_\_ Specific Weight (kips/ft<sup>3</sup>): **SP** \_\_\_\_\_  
 Rig Model & SN: **PN** \_\_\_\_\_ Wave Speed (ft/sec): **WS** \_\_\_\_\_  
 Hammer Type, LM, Rods: **PD** \_\_\_\_\_ Increment Length (ft): **LI** \_\_\_\_\_  
 Drill Rod Area (in<sup>2</sup>): **AR** \_\_\_\_\_ Sampling Freq. (kHz): **FR** \_\_\_\_\_

### TRANSDUCER INFORMATION

Gage	SN	Calibration
F1:	_____	_____
F2:	_____	_____
A1:	_____	_____
A2:	_____	_____

NOTES:

### SPT TESTING INFORMATION

Start Time	Soil	Depth (ft)		LE (ft)	Rods & Lengths	PDA Blows		SPT Blows			
		Start	End			Start	End	1st 6"	2nd 6"	3rd 6"	4th 6"
5:00	SP	45.5	47	50.83	9(5') + 1(2')	0	2750	12	19	19	
	SP	48.5	50	53.83	10(5')	0	34	10	13	13	

PICTURE NUMBERS AND INFO:

First 4 tests had problems - accelerometers installed incorrectly (one opposite of other) also LE & LP incorrectly inputted. Equal 4 should be correct.