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3 DAYS BEFORE DIGGING IN SOUTH CAROLINA

SOUTH CAROLINA 811 (SC811) WWW.SC811.COM ALL UTILITIES MAY NOT BE A MEMBER OF SC811

ASSET ID _____1753___

TRAFFIC DATA

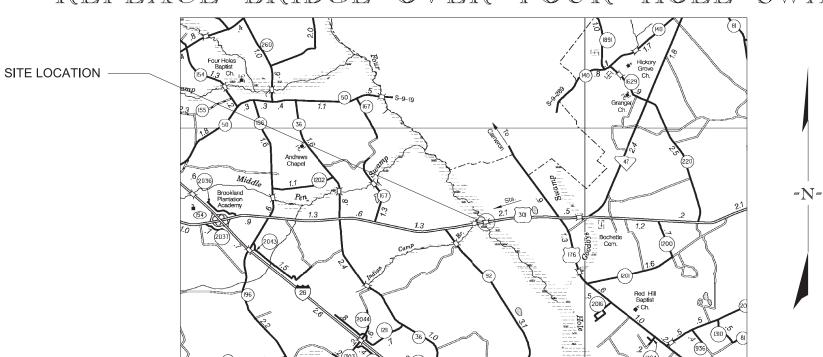
_____2033 ADT _____17500 V.P.D.

2013 ADT 11500 V.P.D.

- APPROACH SLAB DETAILS
 COMPRESSION SEAL EXPANSION JOINT DETAILS

PROPOSED PLANS FOR

ORANGEBURG COUNTY PROJECT ID: 0040308 US ROUTE 301 SOUTHBOUND (FIVE CHOP ROAD) REPLACE BRIDGE OVER FOUR HOLE SWAMP



Submit Shop Plans to:

Preconstruction Support Engineer Attn: Logistics Coordinator - Shop Plans 955 Park Street - Room 409 Columbia, SC 29201

Approximate Location of Bridge is 33°-27'-27" N Latitude 80°-38'-55" W Longitude _____

	FOR CONS	TRUCTION
	INITIAL	DATE
RPG - HYDROLOGY		
RPG - STRUCTURES		
RPG - GEOTECHNICAL		
PRECONSTRUCTION SUPPORT - STRUCTURES		
RPG - DESIGN MANAGER		
RPG - PROGRAM MANAGER		

LAYOUT

NET LENGTH OF ROADWAY	0.000	MILES
NET LENGTH OF BRIDGES	0.055	MILES
NET LENGTH OF PROJECT	0.055	MILES
LENGTH OF EXCEPTIONS	0.000	MILES
GROSS LENGTH OF PROJECT	0.055	MILES

NOTE: EXCEPT AS MAY OTHERWISE BE SPECIFIED ON THE PLANS OR IN THE SPECIAL PROVISIONS, ALL MATERIALS AND WORKMANSHIP ON THIS PROJECT SHALL CONFORM TO THE SOUTH CAROLINA DEPARTMENT OF TRANSPORTATION STANDARD SPECIFICATIONS FOR HIGHWAY CONSTRUCTION (2007 EDITION) AND THE STANDARD DRAWINGS FOR ROAD CONSTRUCTION IN EFFECT AT THE TIME OF LETTING.

WED DR.

NOT FOR CONSTRUCTION

FOR CONST

ENGINEER OF RECORD

 BRIDGE PLANS ID
 SHEET NO.

 0040308-B01
 2

	SUMMARY OF ESTIMATED QUANTITIES						
ITEM NO.	BID ITEM	UNIT	QUANTITY				
1075001	MONITORING OF CONSTRUCTION-RELATED EARTHBORNE VIBRATIONS	LS	NEC.				
2028100	REMOVAL & DISPOSAL OF EXISTING BRIDGE	LS	NEC.				
2033025	BORROW EXCAVATION - (AASHTO TYPE A-1 SAND) ●	TON	1110.000				
2043000	WET EXCAVATION FOR BRIDGES*	CY	3150.000				
2045040	COFFERDAM - TYPE 4 (30,001 - 40,000 C.F.)	EΑ	6.000				
2103000	FLOWABLE FILL	CY	1682.000				
6750278	FURNISH & INSTALL 2.0" SCHEDULE 80 PVC CONDUIT	LF	1340.000				
7011400	CONC. FOR STRUCTURES - CLASS 4000	CY	1015.100				
7011600	CONC. FOR STRUCTURES - CLASS 5000	CY	316.300				
7020300	COMPRESSION SEAL JOINT	LF	94.500				
7023200	GROOVED SURFACE FINISH	SY	1368.000				
7031200	REINF. STEEL FOR STRUCTURES (BRIDGE)	LB	281511.000				
7031220	HOOP REINFORCING STEEL FOR STRUCTURES (BRIDGE)	LB	18408.000				
7051000	CONCRETE BRIDGE BARRIER PARAPET	LF	619.300				
7051910	CONCRETE BRIDGE BARRIER PARAPET TRANSITION	EΑ	3.000				
7110001	DYNAMIC PILE ANAL.TEST SET-UP	EΑ	16.000				
7110010	PILE DRIVING SET-UP	EΑ	42.000				
7112220	STEEL H BEARING PILING (HP 14 X 73)*	LF	375.000				
7112222	STEEL H BEARING INDEX PILING (HP 14 X 73)*	LF	79.000				
7113480	STEEL PIPE PILING (48″ DIAMETER) [®]	LF	2520.000				
7113482	STEEL PIPE INDEX PILING (48″ DIAMETER) [®]	LF	642.000				
7243150	ELASTOMERIC BEARING ASSEMBLY (FLAT SLAB)	EΑ	10.000				
8041010	RIP-RAP (CLASS-A)	TON	630.000				
8048105	GEOTEXTILE FOR EROSION CONTROL UNDER RIP RAP (CLASS 1) TYPE	B SY	822.000				
8990566	CLASS 5000 CONCRETE WITH FIBER (HIGH SLUMP)*	CY	238.200				

Notes

- For use as Class A-1-a loose sand backfill inside Steel Pipe Piles. See Interior Bent Geotechnical Notes, Sh. 22.
- *Provide HP14x73 Steel Piling that conforms to the latest AASHTO Specifications for M270 Steel with a minimum yield strength of 50 ksi.
- Provide 48" Dia.Steel Pipe Piling that conforms to the latest ASTM Specifications for A252 Grade 3 Modified Steel with a minimum yield strength of 50 ksi.
- *Wet Excavation to include cofferdam excavation (See Cofferdam Backfill detail, Sh. 22) and soil extracted from inside of steel pipe piles to facilitate driving of pile through very dense layers.
- *See Special Provisions.

TABULATION OF ESTIMATED BRIDGE QUANTITIES

ITEM	NO.	CONC. FOR STRUCTURES CLASS 4000	CONC. FOR STRUCTURES CLASS 5000		HOOP REINF. STEEL FOR STRUCTURES (BRIDGE)	BARRIER	BARRIER PARAPET	DYNAMIC PILE ANAL. TEST SET-UP	PILE DRIVING SET-UP	STEEL PILING (HP14X73)	STEEL INDEX PILING (HP14X73)	STEEL PIPE PILING (48" DIA.)	INDEX	ELASTOMERIC BEARING ASSEMBLY (FLAT SLAB)	5000 WITH FIBER (HIGH
		CY	CY	LB	LB	LF	EA	EA	EA	LF	LF	LF	LF	EA	CY
End Bents 1 & 8	2		37.4	8,093				4	12	375	79				
Interior Bents 2 thru 7	6		278.9	77,240	18,408			12	30			2,520	642		238.2
132' Span Superstructure	2	852.7		161,966		527.5								8	
30' Span Superstructure	1	84.2		15,964		59.8								2	
Approach Slabs	2	78.2		18.248		32.0	3								
TOTALS		1015.1	316.3	281,511	18,408	619.3	3	16	42	375	79	2,520	642	10	238.2

NOT FOR CONSTRUCTION

SOUTH CAROLINA DEPARTMENT OF TRANSPORTATION

SUMMARY
OF ESTIMATED
QUANTITIES

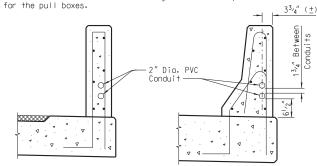
ORANGEBURG ROUTE US 301

OUNTY

1000 C 7:00:00 Colonian Colonian C 200:00 E

Furnish Schedule 80 PVC rigid nonmetallic conduits in accordance with NEMA TC-2 and UL Standard 651 and furnish fittings in accordance with NEMA TC-3 and UL Standard 514B. Furnish conduit and fittings with UL labels: conduit - on each 10 foot length: fittings - stamped or molded on each fitting. Connect conduit and fittings using solvent cement in coordance with monufacturer's resonanced too. in accordance with manufacturer's recommendations.

Furnish and install NEMA Type 4X non-metallic or galvanized steel pull boxes sized in accordance with NEC requirements and the maximum limits shown. Provide gasketed weatherproof covers



SECTION THRU

BARRIER PARAPET

DETAILS OF CONDUIT IN BARRIER PARAPET

(Typ. ea. side of bridge

Use Schedule 80 PVC nonmetallic pipe for conduit.

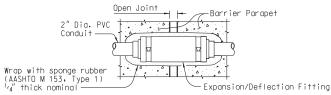
SECTION THRU

BARRIER TRANSITION

Extend conduits 6 inches beyond each end of the barrier parapet transition and cap with watertight covers.

Provide expansion fittings and/or expansion/deflection fittings at all open joints in the barrier parapet.

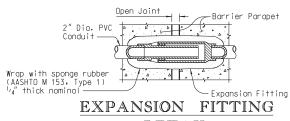
Include all costs for furnishing and installing conduit, expansion/deflection and/or expansion fittings, and any incidentals required in the unit price bid for 2.0" Schedule 80 PVC Conduit.



EXPANSION / DEFLECTION

FITTING DETAIL

(For open joints located at End Bents 1 & 8)



DETAIL

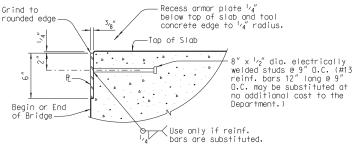
(For open joints located at Interior Bents 4 & 7)

WATER ELEVATIONS

The water elevations shown in the plans are for information only and the actual water elevation during construction may vary depending on weather conditions and seasonal fluctuations.

ORIENTATION IN RELATION TO STATIONING

Left and right sides, where referred to in these plans, are in relation to direction of stationing.



ARMOR PLATE DETAIL AT END BENTS

Install $^{3}\!v_{8}^{\prime\prime}$ thick plates, as detailed above, at the beginning and end of the bridge.

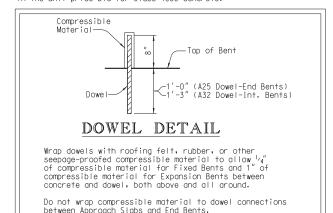
Provide steel for the armor plates that conforms to the latest AASHTO M 270 Grade 50W (ASTM A 709 Gr. 50W) steel and neither the plates nor the anchor studs need to be painted.

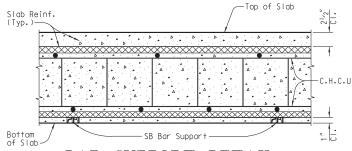
Provide fabricated plates that conform to the crown and grade of the roadway and extend from autter line to autter line. The plates may be fabricated in reasonable lengths and connected at the job site with full penetration butt welds ground flush along the top face of

If necessary, longitudinal reinforcing bars of the slab may be shifted laterally to clear anchor studs.

Holes, $^9\eta_6{''}$ dia., spaced approximately 2'-0" on center may be provided in the lower portion of the plates to bolt the plates to

Include all costs of material and workmanship to fabricate, furnish. and install the armor plates and anchor studs complete and in place, in the unit price bid for Class 4000 concrete.





BAR SUPPORT DETAIL

Section Parallel to C Roadway

For bar supports that contact forms or floor surfaces, use plastic bar supports that conform to the requirements of the Standard Specifications. Protect the plastic bar supports from exposure to sunlight until placed in the form. Where removable forms are used, do not use continuous legs or rails that are in contact with the forms.

For supports that do not contact forms or floor surfaces, use wire bar supports that conform to the requirements of the Standard Specifications. In applications where galvanized bars are used, use galvanized wire supports.

MATERIAL AND WORKMANSHIP

Provide all material and workmanship in accordance with the South Carolina Department of Transportation 2007 Standard Specifications for Highway Construction, unless otherwise specified on the Plans or in the Special Provisions.

COMPLETION DATES

On inside face of right side barrier parapet/railing at beginning of bridge and on left side barrier parapet/roiling at end of bridge, place year of completion adjacent to guardrail attachment. Place this completion date so that it will not be covered by the guardrail connector when it is installed. Recess numbers in the concrete using numbers fabricated from reusable/durable material that is approved by the RCE. Provide numbers in accordance with SCDOT Standard Drawing No. 702–305–00.

REINFORCING STEEL

Embricate reinforcing bars in accordance with the current C.R.S.L. Manual of Standard Practice except for ties, stirrups, and welded hoops.

Provide all ties and stirrups with 135° hooks that have extensions no less than the larger of ten bar diameters or six inches. This 135° hook requirement does not apply to stirrups extending from prestressed

The fabrication tolerance for out-to-out dimension of welded hoop diameter is ± 1/2 inch.

Do not use lap splices in column and shaft reinforcing steel.

CONCRETE

Provide the class of concrete as noted in the contract documents. For cast-in-place structural elements, use Class 4000 concrete where the class of concrete is not specified in the contract documents.

Payment for concrete in slab is based on theoretical plan quantity. No adjustment is made for variation in camber.

Chamfer all exposed edges 3,4" unless otherwise noted.

The minimum acceptable concrete cover for reinforcing steel is $^{1}\mathbf{2}^{"}$ less than the plan dimensions when required by reinforcing bar fabrication

Cast shear keys on bent caps monolithic with the cap unless indicated otherwise in these plans. Construct the top of each shear key level.

GRINDING & TEXTURING CONCRETE DECKS

For bridge stage construction projects, grind and texture the bridge decks as necessary near the stage longitudinal construction joints in order to meet the longitudinal and transverse rideability and rolling straightedge requirements of the Contract.

Prior to casting any closure pour, grinding, or texturing, make profile line surveys (2 to 6 as determined by the RCE) of each stage of the bridge decks. Make one of these profile line surveys for each stage bridge decks. Make one of these profile line surveys for each stage along the edge of the deck adjacent to the closure pour. Compare the surveys within each stage and compare the surveys of each stage to surveys of the adjacent stage to aid in determining the amount of grinding and texturing needed to meet the rideability and rolling straightedge requirements. Submit all grinding and texturing procedures, plotted survey profiles, and proposed grinding depths to the RCE for approval. Maintain a final cover of 2" minimum over the bridge deck reinforcing steel.

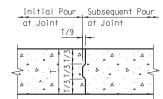
performed on the same bridge, use identical stations for survey shots in order to facilitate survey comparisons. All costs for performing, evaluating, and submitting the surveys are considered incidental to the Contract and no additional compensation is allowed for the performance of this work.

Payment for arinding and texturing concrete bridge decks at the junction of new and existing bridge deck slabs is determined in accordance with Subsection 702.6 of the Standard Specifications. No payment is made for grinding and texturing of new bridge decks to correct irregularities

ALLOWANCE FOR DEAD LOAD DEFLECTION AND SETTLEMENT

In setting falsework for reinforced concrete spans, make an allowance for the deflection of the falsework. for any settlment of the falsework. for the instantaneous dead load deflection of the span, and for the long-time dead load deflection of the span such that on removal of the falsework the top of the structure shall conform to theoretical finished grade plus the allowance for long-time deflection.

For instantaneous and long-time dead load deflection, use a camber of $^{1}\mbox{8}^{\prime}$ for concrete flat slab spans 22 feet in length, $^{3}\mbox{1}_{6}^{\prime\prime}$ for concrete flat slab spans 30 feet in length, and $^{3}\mbox{8}^{\prime}$ for concrete flat slab spans 40 feet and 44 feet in length, unless otherwise directed by the RCE. Adjust these cambers as necessary to allow for falsework deflection, falsework settlement and vertical curve ordinates.



CONST. JT. DETAIL

Before making subsequent pour, wait either a minimum of 96 hours after placement of the initial pour or until the initial pour concrete has attained a minimum of 75% of the specified 28-day compressive strength as verified by testing extra cylinders.

COORDINATION OF PLANS, SPECIFICATIONS, AND SPECIAL PROVISIONS

0040308-B0

Generally, in case of discrepancy, this General Notes and Details for Flat Slabs sheet governs over the Standard Specifications but the remainder of the plans govern over notes on this sheet and Special Provisions govern over all. See Subsection 105.4 of the Standard

DRIVEN PILE FOUNDATIONS

Where piles occur in fill, place fill before driving piles.

Where prestressed concrete piles are to be driven through fill. where prestressed concrete piles are 10 be driven in ough 1111.

For square prestressed concrete piles bore holes having a minimum diameter of 1.25 times the nominal pile size. Include all cost of pre-boring fills for pile installation in the unit price bid for the niles.

EXCAVATION FOR END BENTS

Include all cost of excavation necessary to construct end bents and to remove material under superstructure to an elevation twelve inches below tops of end bent caps, in the unit price bid for class of concrete specified in the Plans.

If a concrete footing is used for the end bent, the excavation below that included for the cap and berm in the above paragraph is paid for at the unit price bid for excavation. Include excavation above this in the unit price bid for class of concrete specified

BEARINGS

Provide a suitable trowel finish to the top surface of concrete caps where concrete slabs bear. See Subsection 702.4.13 of the Standard Specifications.

SPECIFICATIONS

AASHTO 2012 LRFD Bridge Design Specifications, 6th Edition, with Interim Revisions through 2013.

ANSI/AASHTO/AWS D1.5 Bridge Welding Code (latest edition), with additions and revisions as stated in the Standard Specifications.

DESIGN DATA

Load and Resistance Factor Design (LRFD) method

Live Load: AASHTO HL-93 loading

The top 1/4" of all concrete slabs is considered as a wearing surface and is not included in the slab depth used for the calculation of section properties.

An extra dead load of $0.015~\mathrm{KSF}$ is incorporated into the design of this structure as an allowance for a future wearing surface.

Seismic design is in accordance with the 2008 SCDOT "Seismic Design Specifications for Highway Bridges". Version 2.0, with the following parameters:

Seismic Design Category: C

Analysis Method: Multimode Spectral with Pushover

Operational Classification: II

Site Class: D

Design Acceleration Coefficients:

PGA (FEE Sps (FEE Spi (FEE): 0.39	g Sp	GA (SEE): os (SEE): on (SEE):	0.87
----------------------------------	---------	------	-------------------------------------	------

Values determined from Three Point Method

FINAL FINISH OF EXPOSED CONCRETE SURFACES

Addly the final surface finish on the $\mbox{bridge}(s)$ only to the following checked and designated bridge areas:

A) Entire surface of all barrier rails, parapet walls, approach slab curbs, concrete utitlity supports, and wing walls; outside vertical edge of bridge deck slabs and sidewalks.

☐ B) Outside face of exterior prestressed girders.

☐ C) Entire surface of designated substructure units, except top of bent caps and piers.

> ☐ All Units □ Designated Units:

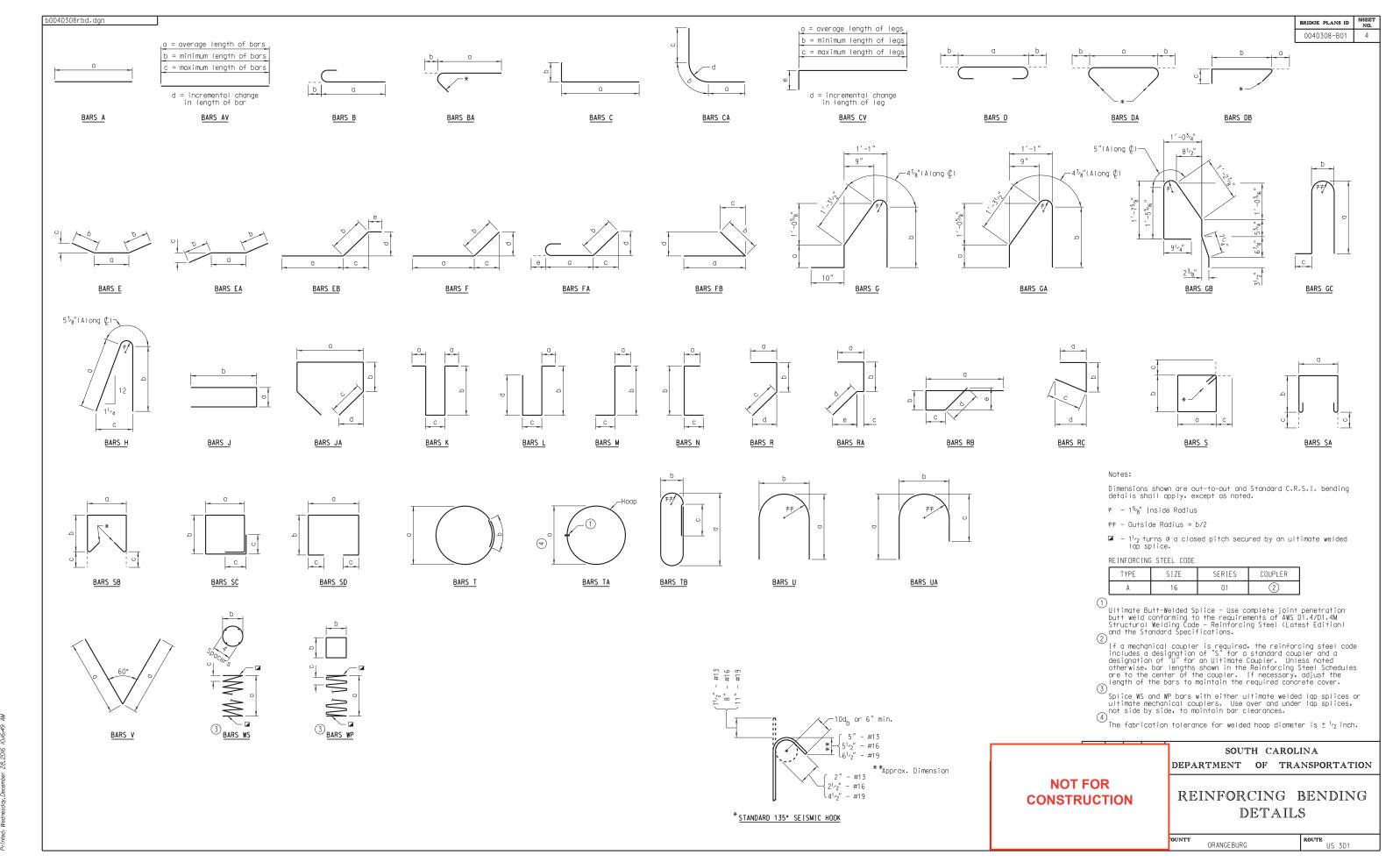
□ D) No final surface required.

NOT FOR CONSTRUCTION

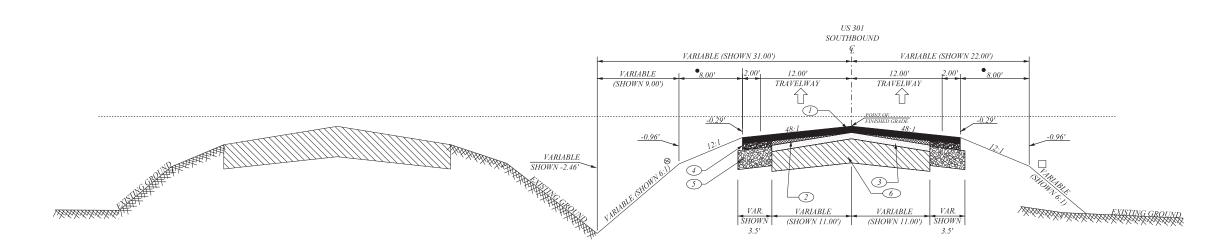
SOUTH CAROLINA DEPARTMENT OF TRANSPORTATION

> GENERAL NOTES AND DETAILS FOR FLAT SLABS

ORANGE BURG



TYPICAL SECTION OF IMPROVEMENT SOUTH CAROLINA DEPARTMENT OF TRANSPORTATION COLUMBIA, S.C.



USE THIS TYPICAL SECTION ON US ROUTE 301 SOUTHBOUND FROM STATION 5941+40.00 TO 5960+00.00

DESIGN SPEED

MPH

US ROUTE 301 RURAL PRINCIPAL ARTERIAL

FOR INFORMATION ONLY

⊗ NOTES:

THIS SLOPE MAY BE VARIED WHEN A DEEPER DITCH IS NECESSARY
FOR DRAINAGE PURPOSES, USING A MINIMUM SLOPE OF 12:1 AND A
MAXIMUM SLOPE OF 4:1. WHERE A DEEPER DITCH THAN PROVIDED
BY A 4:1 IS NECESSARY, THE DITCH SHALL BE PLACED FARTHER FROM
THE & CONTINUING THE 4:1 SLOPE TO PROVIDE FOR THE NECESSARY
DEPTH. SEE PROFILE FOR THE SPECIAL DITCH GRADES.

☐ FILL SLOPES

6:1----0' TO 5' FILL

4:1----5' TO 10' FILL

2:1-----OVER 10' FILL

IF 2:1 SLOPE IS USED, WIDEN SHOULDER 3.5' FOR GUARDRAIL

PH FROM STA. TO STA. 50 5941+40.00 5960+00.00 EXCEPTIONS TO DESIGN SPEED CONSTRUCTION

SOUTH CAROLINA ENT OF TRANSPORTATION SIGN COLUMBIA, S.C.

PICAL SECTION

CALE I"H=NTS RTE./RD.

PAVEMENT LEGEND

HOT MIX ASPHALT SURFACE COURSE TYPE B (200 LBS/SY)

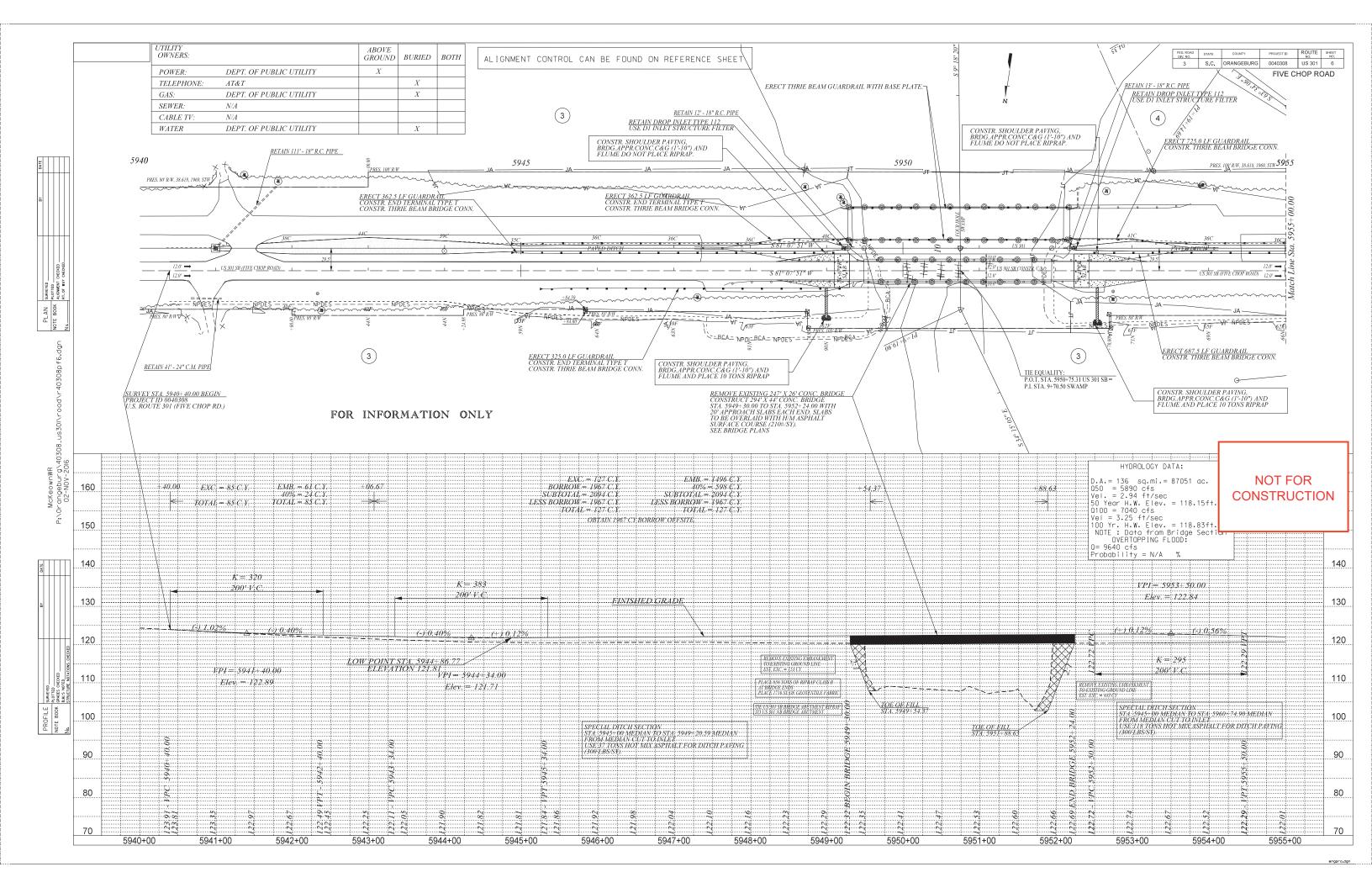
HOT MIX ASPHALT INTERMEDIATE COURSE TYPE B FOR BUILDUP AND LEVELING

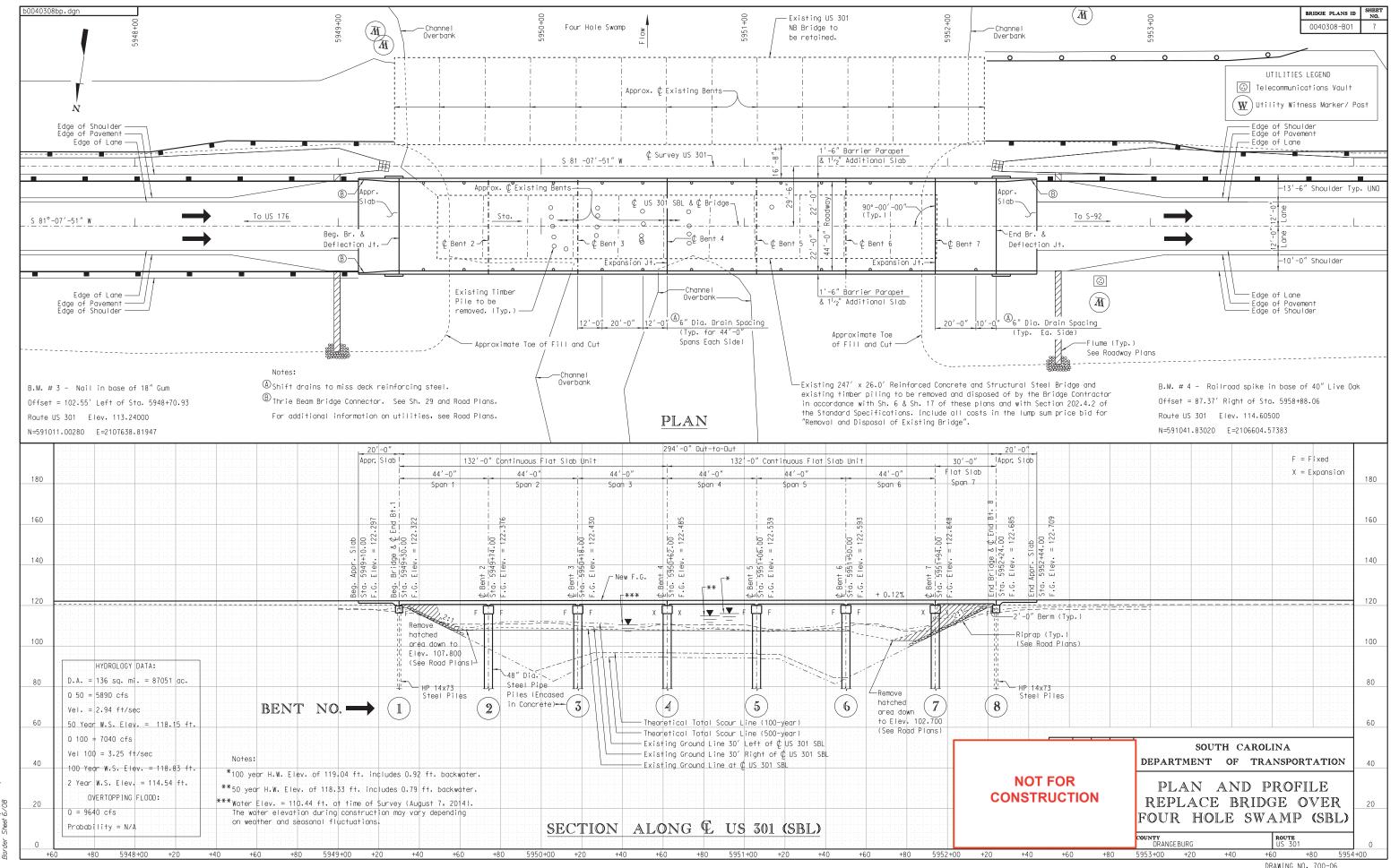
HOT MIX ASPHALT INTERMEDIATE COURSE TYPE B FOR BUILDUP AND LEVELING
 MILL EXISTING SURFACE 2" & REPLACE WITH HMA SURFACE TYPE B (200 LBS/SY)

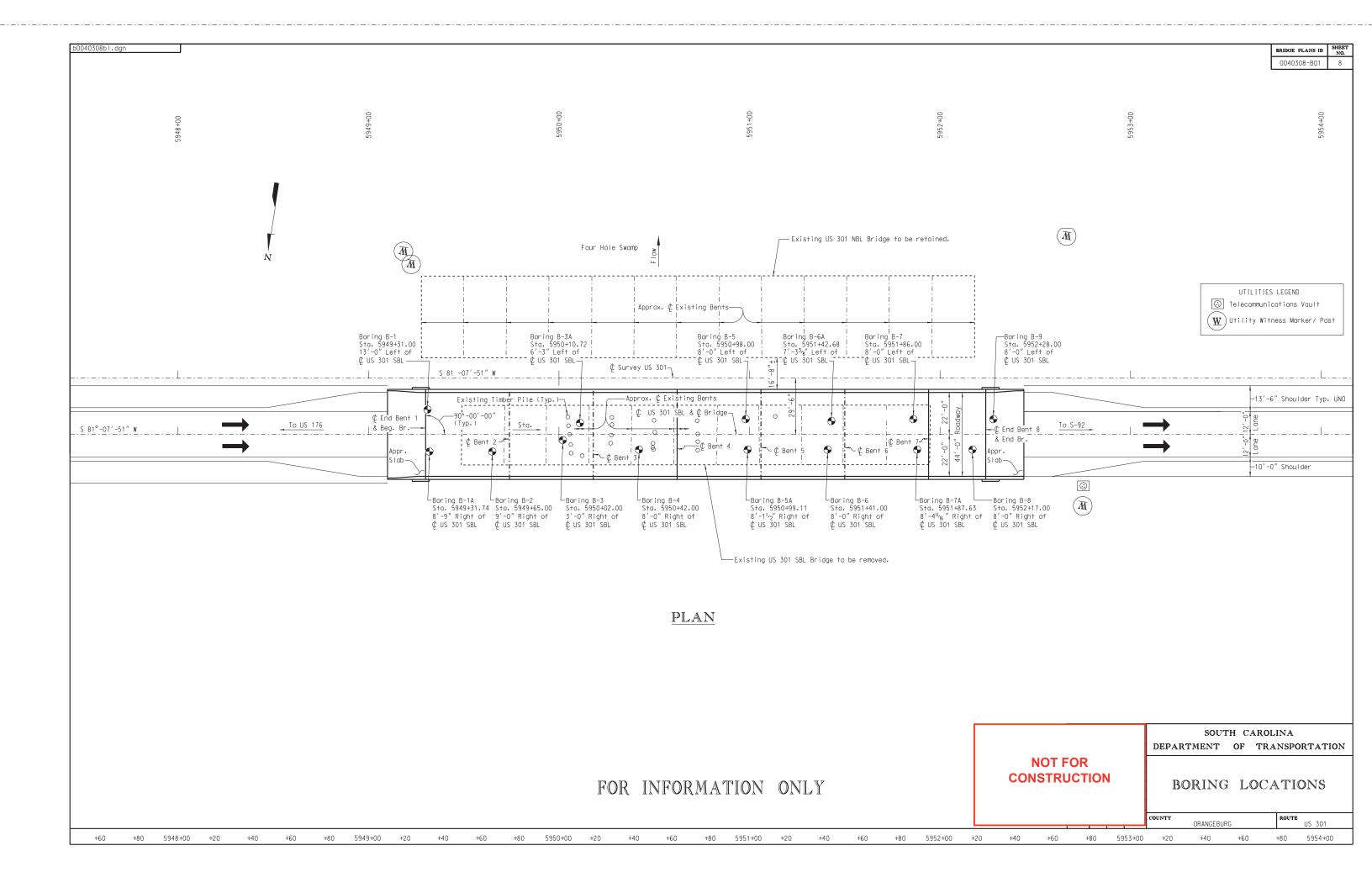
HOT MIX ASPHALT INTERMEDIATE COURSE TYPE B (200 LBS/SY)

BHOT MIX ASPHALT BASE COURSE TYPE A (600 LBS/SY)

6 EXISTING ASPHALT PAVEMENT - RETAIN







SCENT Soil Test Boring Log SCENT Soil Test Boring Log Scil Test Boring Log | File No.: | 38.0309 | Project No. | PM|; | BR38(019) | County: | Orangeburg | Eng/Geo.: | R. DeLost Site Description: | Birdy Replacement over Four Hols Swamp | Route: | US 301 | Boring No.: | Birdy Replacement over Four Hols Swamp | Route: | US 301 | Boring No.: | Birdy Replacement over Four Hols Swamp | Route: | US 301 | Boring No.: | Birdy Replacement over Four Hols Swamp | Route: | US 301 | Boring No.: | Birdy Replacement Over Four Hols Swamp | Route: | US 301 | Route: Very stiff to hard, moist, green, gray & tan, strongly reactive, med. to strongly cemented, sandy SILT (MLA-4).

LL=NP, PL=NP, PI=NP, NMC=33.9, %8/200=55.3 Very loose to loose, dry to wet, orange, tan, black, brown & gray, sub-angular, non-reactive, f. to med. grain sitty SAND (SM/A-2-4). 20 SS-1 3 2 2 4 X OA 60 SS-2 3 4 4 8 8 80 SS-3 3 2 2 4 8 80 SS-4 1 1 1 1 2 9 SX-A 51.0 SS-13 8 9 23 31 X No Casing Refusal & Boring Terminated @ 102.5' (Elev. 17.4). 56.0 SS-14 6 10 17 27 Bulk Sample #1 taken at 1' to 5' deep as per boring plan. Alluvium:

Very loose, moist, tan, brown & gray, non-reactive, clayey SAND (SC/A-2-4). LL=25, Pl=17, Pl=8, NMC=17.5, %#200=32.3 61.0 SS-15 10 14 18 32 66.0 SS-16 9 17 28 45 SS-6 10 11 12 23 XA O 1.0 SS-17 9 21 46 67 SS-8 8 16 21 37 76.0 SS-18 12 18 27 45 LL=37, PL=31, PI=6, NMC=38.1, %#200=28.5 Medium dense to very dense, moist towet, green & gray, sub-angular, strongly reactive strongly cemented, f. grain, silty SAND (SMA-2-4) LL=NP, PL=NP, PI=NP, NMC=23.5, %#200=24.5 96.0 SS-10 16 50/0.4 50/0.4 86.0 SS-20 19 34 50 84 SS-11 5 5 12 17 × SS-21 8 19 22 41 Dense, moist, dark green, black & gray, weakly reactive, poorly graded SAND with silt (SP-SM/A-1-b). 46.0 SS-12 6 9 16 25 SS-22 19 28 50 78 SCIPET Soil Test Boring Log SCEET Soil Test Boring Log SCIPET Soil Test Boring Log | File No. | 34-00282 | Project No. | Projec | File No.: | 384/09/82 | Project No. (PRI): | 0.040308 | County: | Orangeburg | Eng./Geo.: | B. Living Site Description: | Burgos Replacement Over Four Hole Swamp | Route: | US301 | Soring No.: | B-1A | Boring Location: | 5949-91.71 | Offset: | 8.7 R | Alignment: | Propose | Boring No.: | B-1A | Boring Location: | 5949-91.71 | Offset: | 8.7 R | Alignment: | Propose | Elev: | 119.91 | Latitude: | 33.4575 | Longitude: | 80.6472 | Data Started: | 124/2014 | Soring No.: | File No. 13-8-0222 | Project No. Pilh3: | 0.040338 | County: Orangeburg | Eng./Geo.: B. Site Description: Bridge Replacement Over Four Hele Swamp | Routet: US |
Site Description: Bridge Replacement Over Four Hele Swamp | Routet: US |
Boring No.: Bridge Replacement Over Four Hele Swamp | Routet: US |
Elev: 119.9 ft | Lettude: 33.4575 | Longitude: |-80.6472 | Date Started: 1242 |
Elev: 119.9 ft | Lettude: 33.4575 | Longitude: |-80.6472 | Date Started: 1242 |
Elev: 120 ft | Soil Deplith: 120 ft | Core Depth: 160 | End. Political Configuration |
Drill Machine: CME 55 | Drill Method: | Mud Rolay | Hammer Type: Safely Hammer Sperigy Ratios: Core Size: | Driller: Carolina Driling | Groundwater: TOB | 9.7 n. 244R. ● SPT N VALUE ● | \$\frac{1}{6}\tilde{\text{E}} \\ \frac{1}{6}\tilde{\text{E}} SS-12: MC=46%, LL=40, PL=38, PI=2, FC=49.3% FC=49.3%
Very stiff to hard, wet, green gray, Sandy
SILT (ML), slightly micaceous
(contains lenses of sand with strong
cementation)
(contains trace shell fragments)
SS-13: MC=35.3%, LL=29, PL=27, PI=2,
FC=56% 53.5-SS-14 7 13 16 2t 58.5 SS-15 10 18 24 42 33-14: MC=36.7%, LL=32, PL=31, PI=1, FC=66.3% 3.5 SS-26 12 17 18 35 63.5-SS-16 15 18 23 41 SS-6 2 4 5 9 **●**×-€× ▲ Loose, wet, gray, fine to medium grained Clayer SAND (SC), slightly micaceous SS-6: MC=20.5%, LL=25, PL=13, Pl=12, FC=42.3% Ver dense, wet, dark gray, fine to medium grained, poorly graded SAND with silt (SP-SM), micaceous SS-17 14 15 21 3f X 🖎 18.5 SS-7 7 16 9 25 ● Boring Terminated at 120 Feet COASTAL PLAIN DEPOSIT - Medium dense, wet, gray, medium grained, poorly graded SAND (SP), slightly micaceous (low recovery) 73.5 SS-18 19 22 29 51 Very dense, wet, green gray, fine to medium grained, Silty SAND (SM), slightly micaceous SS-20 30 50/3* 10) 33.5 SS-10 7 50/4" 100 6.5 Very dense, wet, dark green, fine to
medium grained, Silty SAND (SM), slightly
micaceous Very stiff, wet, green gray, Sandy SILT (ML), slightly micaceous 88.5 SS-21 17 32 50/5 10) 38.5 SS-11 7 9 13 22 ●※ ○ ▲ SS-11: MC=37%, LL=28, PL=26, PI=2, FC=57.7% 43.5 SS-12 11 14 50/5 100 Ж 🖎 Very dense, wet, green gray, fine to coars grained, Silty SAND (SM), slightly 98.5 SS-23 37 50/5.5* 10) 48.5 SS-13 11 10 11 21 ◆ж○ ▲ Continus

DRILLING METHOD

RW - Rotary Wash

CFA - Continuous Flight Augers

DC - Orlving Casing

CFA - Continuous Flight Augers

RC - Rock Core SAMPLER TYPE

NQ - Rock Core, 1-7/8*

CU - Cuttings

8"

CT - Continuous Tube SOUTH CAROLINA DEPARTMENT OF TRANSPORTATION **NOT FOR** FOR INFORMATION ONLY CONSTRUCTION BORING LOGS (1 OF 8)

0040308-B01

ROUTE US 301

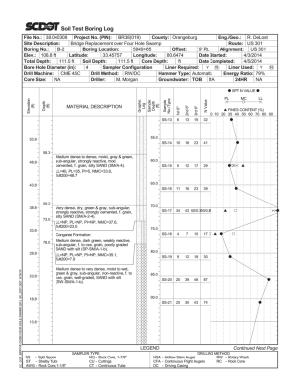
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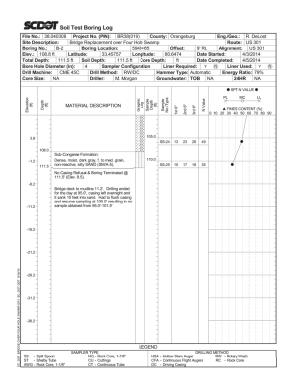
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BRIDGE PLANS ID

0040308-B01





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DEPARTMENT OF TRANSPORTATION

BORING LOGS (2 OF 8)

COUNTY ORANGEBURG ROUTE US 301

0040308-B01 SCENT Soil Test Boring Log SCENT Soil Test Boring Log SCENT Soil Test Boring Log | File No. | 38 A0030 | Project No. P(PN) | ER38(019) | County; | Orangeburg | Eng./Geo. | R. DeLos Site Description: | Bridge Replacement over Four Hole Swamp | Route: US 301 | Boring No.: | Bridge Replacement over Four Hole Swamp | Route: US 301 | Boring No.: | Bridge Replacement over Four Hole Swamp | Route: US 301 | Elev: 108.8 ft | Latitude: | 33 A5751 | Longitude: | 80.64752 | Date Started: | 42/114 | Core Depth: | 101.5 ft | Core Depth | File No.: | 38.0/0308| | Project No. | (PN): | BR38(019) | County: | Crangeburg | Eng./Geo.: | R. DeLost |
Site Description: | Bridge Replacement over Four Hole Swamp | Russian | Street | Street | Street |
Site Description: | Bridge Replacement over Four Hole Swamp | Russian | Street | Street |
Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | Street | St | File No.: | 38.0030 | Project No. Phys. | BR38(019) | County: | Orangeburg | Eng/Geo.: | R. DeLost Site Description: | Biograp Replacement over Four Hols Swamp | Routse: | US 301 | Boring No.: | B - 3 | Boring Location: | 596+02 | Offset: | 3º RL | Alignment: | US 301 | Elev: | 108.8 ft | Latitude: | 33.45751 | Longitude: | 80.64752 | Date Started: | 42/114 | Croal Degitio: | 101.5 ft | Soil Depth: | 101.5 ft | Core Degiti: | 10.5 ft | Date Complete: | 42/214 | Doro Hole Diameter (in): | 4 | Sampler Configuration | Limer Required: | 4 | Sampler Configuration | Drill Machine: | CME 455 | Drill Method: | RW070 | Hammer Type: Alutomatic | Energy Ratio: 79% | Core State: | NA | Driller: | M. Morgan | Groundwater: | TOB | 3.3 ft | 24HR | 3.3 f | Section | Sec Sub-Congaree Formation:

101.5 Sub-Congaree Formation:

Medium dense, moist, dark gray,
non-reactive, mod. cemented, siliy SAND (SMA-S),
(LL=44, PL=44, Pl=NP, NMC=38.9,
%#2001=42.6 20 40 8S-1 1 2 3 5 60 8S-2 1 3 9 12 20 8S-3 3 6 12 18 80 80 84 7 8 4 12 55.0 SS-14 10 8 7 15 No Casing Refusal & Boring Terminated @ 101.5' (Elev. 18.8). .0 SS-5 3 10 32 42 X0× ▲ 8.8- Congaree Formation:

Very locse, wet, dark green, weakly reactive,

I. grain, sitty SAND (SM/A-2-4).

L=NP, PL=NP, PI=NP, NMC=35.9,

%200=28.0 Hard, moist, green, gray & tan, strongly reactive, f. to cse. grain, sandy SILT 13.3 (ML/A-4). LL=36, PL=29, PI=7, NMC=30.2, %#200=51.9 SS-16 0 0 0 0 0 Hard, moist, green, gray & tan, strongly reactive, f. to cse. grain, sandy SILT (ML/A-4). LL=NA, PL=NA, PI=NA, NMC=NA, %#200=55.2 SS-17 0 0 0 0 • 5.0 SS-18 0 0 0 0 • 30.0 SS-9 4 6 11 17 35.0 SS-10 6 6 7 13 × • • SS-20 14 20 26 46 SS-11 16 10 8 18 • 45.0 SS-12 5 6 7 13 • SS-22 12 20 28 48 SCENT Soil Test Boring Log SCORT Soil Test Boring Log SCIPET Soil Test Boring Log | File No. | 34-00028 | Project No. | 19-004 | File No. | 3-448952 | Project No. | [PN] | 0.044308 | County: Orangeburg | Eng./Geo: B. Livingst |
Site Description: Bridge Replacement Over Four Hole Swamp | Strip Replacement Over Four Hole Strip Replacement Over Hole Strip Replacement Over Hole Strip Replacement Over Hole Strip Replacement | Strip Replacement Over Hole Strip Replacement | Strip Replacement Over Hole Strip Replacement | Strip | File No.: | 34-0822 | Project No.|FIM|: | 0040308 | County: | Orangeburg | Eng./Geo.: | B. Living |
Site Description: | Bridge Replacement Over Four Hele Swamp | Route: US301 |
Boring No.: | B-3A | Boring Location: | 596+10-72 | Offset: | 6.25 | L. Alignment: | Propose |
Elev.: | 120.3 ft | Latitude: | 33.4575 | Longitude: | -80.6475 | Date Started: | 12/8/2014 |
Total Depth: | 31.2 ft | Soil Depth: | 120 ft | Core Depth: | 120 ft ● SPT N VALUE ● SS-31 23 29 40 69 SS-12 6 6 10 16 • ×× O • SS-32 34 50/5" 100 61.2 SS-13 13 21 20 41 63.2 SS-14 11 19 28 47 65.2 SS-15 15 24 32 56 11.2 13.2 SS-1WOR/24* 0 • 15.2 SS-2 1 1 2 3 • 67.2 SS-16 15 19 50/5.5 100 Very dense, wet, dark gray, fine to medium grained, poorly graded SAND with silt (SP-SM), micaceous SS-34: MC=30.3%, LL=NP, PL=NP, PI=NP, FC=5% Loose, wet, gray and white, medium to 17.2 coarse grained, poorly graded SAND (SP) 2.3 Very soft to soft, vet, dark green, Sandy Elastic SILT (MH), slightly micaceous S-16: MC-316: ML (11-15), Ful-133, Hu-2; FC-60: 17: MC-376: 9%, LL-113, PL=102, PL=11; FC-647: MC-376: 9%, LL-113, PL=102, PL=11; FC-647: MC-376: 9%, LL-111; PL=101, MC-376: 9%, LL-111; PL=101, SS-34 13 29 39 68 X▲ □ 5.2 SS-2WOR/24" 0 • Very hard, wet, black, Sandy Elastic SILT (MH), micaceous SS-22: MC=336.3%, LL=111, PL=101, PI=10, FC=62.8% 88-6 7 18 22 40 X **X ●** ▲ SS-22 WONOH/12" 0 ♦ 79.2 Very soft to soft, wet, dark green, fine to medium grained, Silty SAND (SM), slightly micaceous SS-23: MC=316.1%, LL=99, PL=92, PL=97, FC=41% 83.2 SS-24 WOH 1 2 3 • ▲ 85.2 SS-25 WOH 2 1 3 • A 85.2 SS-26 4 6 13 19 35.3 85.2 SS-24: MC=305.5%, LL=90, PL=86, PI=4, FC=39.7% SS-25: MC=266.5%, LL=75, PL=66, PI=9, FC=32.8% 89.2 SS-27 WOH 1 8 9 X • 39.7 SS-9 8 12 15 27 (contains shell fragments)
SS-12: MC=43.6%, LL=35, PL=29, Pl=6, FC=63.3% SS-28: MC=25%, LL=NP, PL=NP, PI=NP, FC=19.9% Dense, wet, dark green, fine to coarse grained, Silty SAND (SM), slightly 49.7 SS-11 10 12 15 27 EEGEND 7 SS-30 23 28 28 56 Continue

HSA - Hollow Stem Auger

CFA - Continuous Flight Augers

DC - Driving Casing

CFA - Continuous Flight Augers

RC - Rock Core COntinue

DRILLING METHOD

HSA - Hollow Stem Auger RW - Rotary Wash

CFA - Continuous Flight Augers RC - Rock Core

DC - Dividen Casien. SOUTH CAROLINA DEPARTMENT OF TRANSPORTATION **NOT FOR** FOR INFORMATION ONLY CONSTRUCTION

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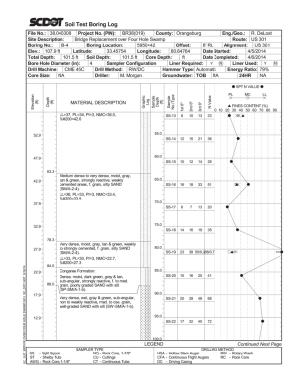
BORING LOGS (3 OF 8)

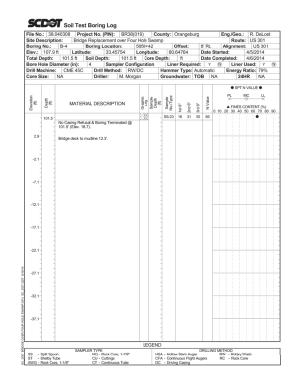
COUNTY ORANGEBURG ROUTE US 301

BRIDGE PLANS ID

0040308-B01

| File No. | 38.040306 | Project No. (PN): BFS8(019) | County: Orangeburg | Eng./Geo. | R. Duicust | Site Description: Discount | Si





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DEPARTMENT OF TRANSPORTATION

BORING LOGS (4 OF 8)

COUNTY
ORANGEBURG

ROUTE US 301

File No. 36,040308	File No.; 18 200,0038 Project No. (PR): BR38(019) County; Crangeburg Eng/Geo.; R. DeLost	File No. 38.040008 Project No. (PR); BR38(019) County; Orangeburg Eng./Geo: R. DeLost	
	SS-17 10 18 22 41 SS-17 10 18 22 41 SS-17 10 18 22 41 SS-18 10 SS-1	SS - Self Spoon SAMPLER TYPE LEGEND SS - Self Spoon NO - Rook Core, 1-167 OT - Continues Tube SS - Self Spoon NO - Rook Core, 1-167 OT - Continues Tube DC - Diving Caleng File Not: 30-4009022 Project Not, PRIN; 0040209 County Orangeburg Eng. Geno. B. Livingston Rook Core Livingston Continues Tube Diving Caleng File Not: 30-4009022 Project Not, PRIN; 0040209 County Orangeburg Eng. Geno. B. Livingston Rook Core Livingston Continues Tube Diving Caleng Rook USS/01 Rook County Diving Caleng Rook USS/01 Rook USS/01 Rook County Diving Caleng Diving Caleng Rook USS/01 Rook USS/01	
### MATERIAL DESCRIPTION Section Section	### SECOND CONTINUES OF PRINTS OF PR	MATERIAL DESCRIPTION	
	FOR INFORMATION ONLY	NOT FOR CONSTRUCTION	SOUTH CAROLINA DEPARTMENT OF TRANSPORTATIO BORING LOGS (5 OF 8)

ROUTE US 301

ORANGEBURG

Printed: Wednesday, December 28, 2016 10:14:03 4

SCDOT Soil Test Boring Log	SCEST Soil Test Boring Log		
File No.: 38.040308 Project No. (PIN): ER38(019) County: Crangeburg Eng./Geo.: R. DeLost Site Description: Bridge Replacement over Four Hole Swamp Route: US 301 Boring No.: B.6 Boring Location: S051+41 Offset: 67 Et. Alignment: US 301	File No. 120 240200 Businest No. (DBD) DD2000400 County County County		
Step Description: Program Replacement over You' note Swarmp	Site Description: Bridge Replacement over Duri Hole Swamp Bourt		
Bore Hole Diameter (In): 4 Sampler Configuration Liner Required: Y & Liner Used: Y & Drill Machine: CMF 45C Drill Method: RW/RCDC Hammer Type: Automatic Finerry Ratio: 79%	Total Depth: 35.2 ft Soil Depth: 15.2 ft Core Depth: 20 ft Date Completed: 4/8/2014		
	Core Size: NQ2 Driller: M. Morgan Groundwater: TOB NA 24HR NA		
● SPT N VALUE ● 5	9 87 N VALUE ● 8 8 8 8 9 P. MC LL X → X		
Section Sect	## 2		
Albuharr. Lose, web brown, tan & gray, sub-angular, 3.4 weekly reachine, med to cise, grain, sily \$5.1 3 4 3 7 \$	sandstone, fossiliferous (fracs. & trc. mega		
102.8 5.8 Medium dense, wet, brown, tan & gray, 6.0	sizheb med. strong 26 6-265; 27+ 0" B, T-MW, No. PH-1, SR 51		
sub-argular, no-reactive, most 10 csic grain, 85-3 8 11 17 28 34 0 8.0	0.0 Boring Terminated (@ 35.2 (Elev. 85.0). Bridge deck to musline 12.4.		
Modium dense and brown to 8 arm SS-5 1 1 2 3 • 4	47.8		
13.3 sub-angular, non-reactive, med. to cse. grain, poorly graded SAND (SPIA-1-b).			
Loose, wet, brown, tan & gray, sub-angular,	42.8		
non-reactive, med. to case grain, poorly	37.8		
Ns/200=2.1 Very loose, wet, gray & brown, sub-angular, NQ-2 REC%=66, RQD%=16			
82.8 25.2 mon-reactive, med. to cae, grain, poorly grain discovered by the process of the proces	32.8		
Very dense, wet, gray & green, sub-argular,			
77.8 Sweldy reactive, med. to ice, gain, silly	27.8		
man 25.2 Grawton tanut green scat black-dk	22.8		
Drown, I. to med, grain wivout, case, friga, think to think to think to the total case, friga, think to think to the total case, friga, think to the total case, frigate, the total case, the total case of the total case, the total ca			
weathered wisemen competely weathered v. (67.8 — (continued value) for the continued v. (67.8 — (continued value) for the continued v. (continued value) for the continued v. (continued v. (continu	17.8		
23 0"-10" B, T-MW, No, PI-Wa, SR			
George Company Company (Company Company Compan	DI 12.8		
VC discontinuity spacing, pods of carcireous LEGEND Continued Next Page	LEGEND		
SAMPLER TYPE SAMPLER TYPE DRILLING METHOD	SS - Spill Spoon No Rock Core, 1-7/6" HSA - Hollow Stem Auger DittLINNS METHOD DISTURNS METHOD		
ST - Shelty Tube CU - Cuttings CFA - Continuous Flight Augers RC - Rock Core AWG - Rock Core, 1-1/8" CT - Continuous Tibe DC - Driving Casing	ST - Shelly Tabe CU - Cuttings CFA - Continuous Flight Augens RC - Rock Core SL AWG - Rock Cose, 1-18° CT - Continuous Tube DC - Driving Casing		
CCDOT	CORAT	CCDOT	
	File No.: 3840308.2 Project No. (PIN): 0040308 County: Orangeburg Eng./Geo.: 8. Livingston	Soil Test Boring Log File No.: 38-40398.2 Project No. (Pill): 0040308 County: Orangeburg Eng./Geo.: B. Livingston	
Site Description: Bridge Replacement Over Four Hole Swamp Route: US301 Boring No.: B-6A Boring Location: 5951+42.88 Offset: 7.28 L. Alignment: Proposed Belve: 120.3 ft. Latitude: 33.475 Longitude: 40.6478 Date Started: 1207/2014 Total Depth: 131.7 ft. Soil Depth: 120 ft. Core Depth: ft. Date Completed: 1217/2014	Site Description: Bridge Replacement Over Four Hole Swamp Route: US301 Boring No.: 8-64 Boring Location: 5951+42.68 Offset: 7.2 \(\) L Alignment: Proposed	Site Description: Bridge Replacement Over Four Hele Swamp Route: US301	
Elev.: 120.3 ft Latitude: 33.4575 Longitude: -80.6478 Date Started: 12/7/2014 Total Depth: 131.7 ft Soil Depth: 120 ft Core Depth: ft Date Completed: 12/7/2014	Site Description: Bridge Replacement Over Four Hole Swamp Boring No.: 8-6A Boring Location: 5951+42-68 Offset: 7.2L Alignment Proposed	File No.: 39-400982 Project No. (PNI): 0040308 County: Orangeburg Eng./Geo.: B. Livingston Site Description: Birdge Replacement Over Four Hele Swamp Route: US301 Boring No.: 18-64 Boring Location: 1895-42.68 Offset: 7.28 L. Alignment: Proposed Elev.: 120.5 ft Latitude: 33.4575 Longitude: 30.6178 Date Started: 127/2014 Total Degits: 13.7 ft Soil Depth: 17 ft Soil Depth: 17 ft Soil Depth: 17 ft Soil Depth: 18 Soil De	
Bore Hole Diameter (In): 4 Sampler Configuration Liner Required: Y	Bore Holo Dismeter (in): 4 Sampler Configuration Drill Machine CME 55 Drill Method: Mud Rotary Core Size: Driller: Carolina Drilling Groundwater: TOB 8.6 ft 24MR	Born Hole Diameter (in): 4 Sampler Configuration Liner Required: Y 6 Liner Required: Y 7 Structure (in the Configuration Liner Required: Y 7 Structure (in the Configuration Liner Required: Y 8 Liner Required: X 9 Liner Required: Y 8 Liner Require	
One Size. Dillier. Carollia Dilling Globinarate. OD S.O.I. Zerric	Cute Size. Dillier. Calculus Dillilling Grountwater. Cut Size Petrix ■ SPTIN VALUE ●	Core size. Drimer. Calonina Drimity Groundwater. TOD 5.0 ft 24mm	
Second	Second to the	United the second of the seco	
0.0 Annis Contract (%) 0.0 Annis of the first of the firs	A PINES CONTENT (S) Set 10 10 10 10 10 10 10 1	## A FINES CONTENT (%) FC=11.5% FC=2.15	
	65.3	163 - 1062 - SS-28505.5' 100X A Q	
115.3	SS-12 10 16 24 4€ × • A		
110.3 9.6 W Water	60.3 -	10.3 - 10.2 - 55.29 30 40 505 100	
11.7 ALLUVIAL - Very soft, wet, brown, Sandy 11.7 SILT MILE 13.7 SI-MOH/18'3 0 •		113.5 Hard, wet, black, Sandy Lean CLAY (CL), micaelous 115.2	
105.3 Contains wood 15.7 SS-2 3 3 4 7 COLORS to medium dense, wet, light gray and	55.3	SS-30, MC=40,1%, LL=40, PL=19, Pl=21,	
white, medium to coate; went gain gard and white, medium to coate grained, porty graded SARD (SP) graded SAR	08.2 - Heart to very hand, wet, green gray, SILT 70.2 - Heart to very hand, with small (RILL, slightly) microscous 70.2 - Grountine Insense of commented sands with 1 2 - SS-15 14 32 505° 100 N-O	18.5 V—COON. 19.5 V—COON. 3.5 V—COON. 19.5 V—COON. 19.	
1003	- moderate to strong cemeratalion (- (contains small shelf tragements) 73,7 SS-16 15 19 25 44	FC=17.8%	
COASTAL PLAN DEPOSIT - Medium COASTAL PLAN DEPOSIT - Medium 2.25 Coastal Plan Deposit - Medium SS-0 0 0 0 12 Coastal Plan Deposit - Medium SS-0 0 0 0 12 Coastal Plan Deposit - Medium SS-0 0 0 0 12 Coastal Plan Deposit - Medium SS-0 0 0 0 12 Coastal Plan Deposit - Medium SS-0 0 0 0 12 Coastal Plan Deposit - Medium SS-0 0 0 0 12 Coastal Plan Deposit - Medium SS-0 0 0 0 12 Coastal Plan Deposit - Medium SS-0 0 0 0 12 Coastal Plan Deposit - Medium SS-0 0 0 0 12 Coastal Plan Deposit - Medium SS-0 0 0 0 12 Coastal Plan Deposit - Medium SS-0 0 0 0 12 Coastal Plan Deposit - Medium SS-0 0 0 0 12 Coastal Plan Deposit - Medium SS-0 0 0 0 12 Coastal Plan Deposit - Medium SS-0 0 0 0 12 Coastal Plan Deposit - Medium SS-0 0 0 0 12 Coastal Plan Deposit - Medium SS-0 0 0 0 12 Coastal Plan Deposit - Medium SS-0 0 0 0 12 Coastal Plan Deposit - Medium SS-0 0 0 0 0 12 Coastal Plan Deposit - Medium SS-0 0 0 0 0 12 Coastal Plan Deposit - Medium SS-0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	45.3 - SS-15: MC=41.2%, LL=38, PL=29, Pl=9, 75,7 SS-17 19 28 50/5.5 10)	4.7 127.0 Very hard, wet, black, Sandy Elestic St., T	
Very dense, velt, green gray, fine grained, Sily SAND (SM), slightly microsis (contains sands with strong cementation)	FC=70.9% 77.7 79.9 18 22 28 55	-9,7- (MH), micaceous	
90.3 (contains shell fragments)	81.7 SS-20 16 25 504* 100	131.7 SS-33 16 23 50/5' 100 Boring Terminated at 131.7'	
360	83.7 SS-21 28 33 505.5 100 83.7 SS-22 19 28 32 66	-14.7 - Groundwater Encountered at 9.6' at Time of Boring	
85.3 -	87.7 88-23 27 50/5" 10)	5.50	
39.0 Very stiff to very hard, wet, green gray, Sandy SILT (ML), stightly microscous SS-9 13 13 16 29	93.3 69.7 69.7 Medium dense, wet, dark green, fine to medium grained, Clayery SAND (SC). 99.17 55.25 10 14 14 21	5 -19.7 -	
- (contains lenses of cemented sands with - moderate to strong cementation)	8 SS-25 MC=31.5%, LL=49, PL=22, Pl=27,	8 24.7	
75.3 (contains small shell fragments) SR.11 - MATS A. 114, 11 = 31, P1 = 39, P1=3, P5=3, P5=3	25.3 VEV_C16		
SS-12: MC=39.9%, LL=32, PL=31, Pl=1, FC=68.2%	alt (BP-SM), micrococus (contains 2" - 5" black all tearns) - 5-5-2" MC-023 M, LL+RP, PL+RP (PI+NP) - 55-27 31 505.5" 100	-29.7	
LEGEND Continued Next Page	LEGEND Continued Next Page	LEGEND SAMPLET TYPE DRILLING METHOD	
Sample TYPE SS - Spill Spoon No. Flock Core, 17/8" SS - Spill Spoon No. Flock Core, 17/8" SS - Spill Spoon No. Flock Core, 17/8" SS - Spill Spoon S	3 SS - Spit Spoon SAMPLER TYPE 5 SS - Spit Spoon Mo-Rook Core, 1-785* HSA - Hollow Stem Auger RW - Rotary Wash 6 ST - Shethy Tube CJ - Clariflage CFA - Continuous Tube 9 ARMS - Rook Core, 1-167* C - Continuous Tube 1 CFA -	SAMPLER TYPE SS - Spill Spoon ST - Sheby Tube CU - Cuttings AND-Rock Core, 1-7/6" CH - Continuous Flight Augers CPA - CONTIN	
CITY - NAME COLORS (1998 COLORS (1998) COLOR	et www.roox.com; i-iie ci - commonse isser toc - Uniting Calling	a Larro-nook core, i-ue til - commone i tote 122 - Umring Caleng	
			SOUTH CAROLINA
			DEPARTMENT OF TRANSPORTATION
			DEFACTMENT OF TRANSPORTATION
	EUD INTEUDMATEUN UNIT W	NOT FOR	
	FOR INFORMATION ONLY	CONSTRUCTION	BORING LOGS (6 OF 8)
			DOUTHO PORS (O OL 9)

ROUTE US 301

ORANGEBURG

Printed: Wednesday, December 28, 2016 10:14:27

ROUTE US 301

COUNTY

ORANGEBURG

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SCENT Soil Test Boring Log

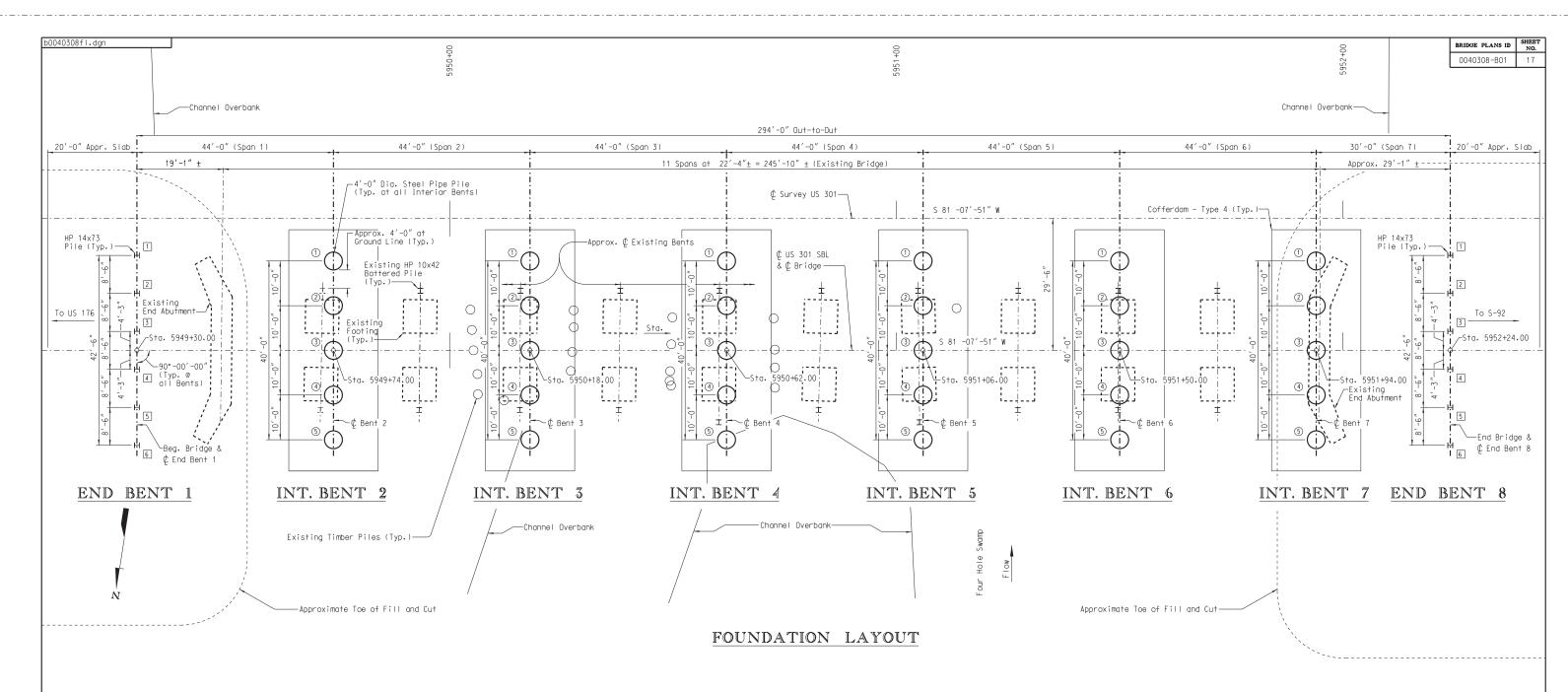
SCDOT Soil Test Boring Log	SCENT Soil Test Boring Log	SCPOT Soil Test Boring Log	
Fish Not. 36.040308	File No.: 38J.403039 Project No. (PRIN): BR38(019) County; Carageburg Eng. Geo.: R. DeLost Site Description: Bridge Replacement over Four Hole Swamp Route: US 301 Boring No.: B-8	File No.: 30.040008 Project No. (PRI)* BR38(015) County: Orangeburg Eng.JGoo: R. DeLost	
SE S	Core Size: NG2 Driller: M. Morgan Groundwater: TOB 12 ft. 24 ft. 10.4 ft.	SSTINUALE	
3.5 gray, sub-emplair, con-exactive, 11 ozes. 40 SS-1 4 7 6 13 X C 11 S	## 15 - 17 - 18 - 18 - 18 - 18 - 18 - 18 - 18	101.4 10 Cash plateat 8 Boring Terminated @ 10/14 (Elev. 16.0) 10 Cash not clash sample at 15.0' due to bore backfilling wiesen ratury, well-told on mud ratury of withing. Max formular 10 Indiana	
Lam. from 6 agry, sub-angular, ron ic 133 - yearded SAAC (GRPA+ 6), 105.0-	55.0	5.0	
graded SAM (SPIA-14),	38-14 10 15 25 44 40 15 25 44 44 10 15 25 45 44 44 10 15 25 45 45 45 45 45 45 45 45 45 45 45 45 45	-5.0	
90.0 30.4 SANG (SRANA) 30.3 35.6 ± 30.03 30.3 RECNI-6F, REDNI-66 30.4 Segin corrupt 30.4 Seg	35-16 15 20 24 44	-15.0 8	
	20.0 Dense, we did not general & gray, sub-angular, we will will be sub-angular, we will be sub-angular, we will be sub-angular, with sub-angular, we sub-angular, with sub-angular, we sub-angular,	3 20.0	
EGEND Continued Next Page S Subject Spoon MG - Road Core, 1-10" ST - Shally Tube CT - Continuous Tibe DC - Dinning Fight Augurs RC - Road Core RC - Road Core RC - Road Core RC - Road Core CT - Continuous Tibe DC - Dinning Castrig AMIG - Road Core, 1-10" CT - Continuous Tibe DC - Dinning Castrig AMIG - Road Core, 1-10" CT - Continuous Tibe DC - Dinning Castrig AMIG - Road Core, 1-10" CT - Continuous Tibe DC - Dinning Castrig AMIG - Road Core, 1-10" CT - Continuous Tibe DC - Dinning Castrig AMIG - Road Core, 1-10" CT - Continuous Tibe DC - Dinning Castrig AMIG - Road Core, 1-10" CT - Continuous Tibe DC - Dinning Castrig AMIG - Road Core, 1-10" CT - Continuous Tibe DC - Dinning Castrig AMIG - Road Core, 1-10" CT - Continuous Tibe DC - Dinning Castrig AMIG - Road Core, 1-10" CT - Continuous Tibe DC - Dinning Castrig AMIG - Road Core, 1-10" CT - Continuous Tibe DC - Dinning Castrig AMIG - Road Core, 1-10" CT - Continuous Tibe DC - Dinning Castrig AMIG - Road Core, 1-10" CT - Continuous Tibe DC - Dinning Castrig AMIG - Road Core, 1-10" CT - Continuous Tibe DC - Dinning Castrig AMIG - Road Core, 1-10" CT - Continuous Tibe DC - Dinning Castrig AMIG - Road Core, 1-10" CT - Continuous Tibe DC - Dinning Castrig AMIG - Road Core, 1-10" CT - Continuous Tibe DC - Dinning Castrig AMIG - Road Core, 1-10" CT - Continuous Tibe DC - Dinning Castrig AMIG - Road Core, 1-10" CT - Continuous Tibe DC - Dinning Castrig CT - Continuous Tibe DC - Dinning	SAMPLER TYPE SAMPLER TYPE ST - Stelly Table GT - Confincious Tube GT - Confincious Tube	LEGEND SS - Salt Spoon SAMPLET TYPE SS - Salt Spoon HD - Rock Core, 1-78" ST - Shelty Nate CFA - Continuous Tight August CFA - Continuous Tight Augu	
Scip Soil Test Boring Log File No.: 38.040308 Project No. (PN): ER38(019) County: Orangeburg Eng./Geo.: R. DeLost Site Description: Bridge Regiscement over Four Hole Powner Route: US 301 Boring No.: 59 Boring Location: 5952*28 Offset: 8' Lt. Alignment: US 301 Elev: 120.0	File No.: 38.340308 Project No. (PIN): BR38(019) County: Orangeburg Eng/Geo.: R. DeLost	File No.: 38.040308 Project No. (PIN): BR38(019) County: Orangeburg Eng./Geo.: R. DeLost	
Bore Nolo Diameter (iii): 4 Sampler Configuration Liner Required: Y Ø Liner Used: Y Ø	Bone Hole Dismeter (iii): 4 Sampler Configuration Liner Required: 7 ® Liner Used: 1 Y ® Configuration Drill Machine: CME 45C Drill Method: RW/DC Hammer Type: Autorutic Energy Ratio: 79% Core Size: NA Driller: M. Morgan Groundwater: TOB 5.9 ft. 244R 12.6 ft. ### SPT N VALUE ** ### MC LINER SPT N VALUE **	Bore Hole Diameter (n) : 4 Sampler Configuration Liner Required; Y 8 Liner Used: Y 8	
Second S	## 36 BE MATERIAL DESCRIPTION \$3 \$3 \$5 \$5 \$5 \$5 \$5 \$5	SE BE MATERIAL DESCRIPTION SE SE SE SE SE SE SE S	
7.5	60.0	50	
15.5 Very locate, vett, gray 6 lain, sub-angular 200	50.0 S\$-17 10 12 15 21 \$	40	
SNA() (SWIN-16) SNA() (SWI	40.0 85.0 85.0 8 20 23 45	-10.0 -15.0	
Dense, molic, geen & gay, silroyly	8.0.0 Congratee Formation: 1. Cone, wit, dark green & gray, sub-angular, 3.0.0 - Loose, wit, dark green & gray, sub-angular, 3.0.0 - Second Construction and one grain, poorly 2.0.0 Second Construction and Grad-Staff-A-10 Second Construc	5	
Lu41, PL40, Pl+1, NMC-41.7, 550 550	Modium dranes, gays, sub-angules. Modium dranes, gays, sub-angules. Modium dranes, gays, sub-angules. Modium dranes, gays, sub-angules. Modium dranes, gays, sub-angules. Modium dranes, gays, ga	SS - Salt Spoon SAMPLER TYPE SS - Salt Spoon HD - Real Core, 1-78" (SS - 1-105c) Sam Aug. CRILLING NETH-CO. ST - Shely Table CJ - Collingo CSA - Collinous Fight August SC - Roak Core CSA - Collingo CSA - Collinous Fight August SC - Roak Core CSA - Collinous Fight August SC - Roak Core CSA - Collinous Fight August SC - Roak Core	
			SOUTH CAROLINA
	FOR INFORMATION ONLY	NOT FOR CONSTRUCTION	DEPARTMENT OF TRANSPORTATION
		CONSTRUCTION	BORING LOGS (8 OF 8)

ROUTE US 301

ORANGEBURG

Printed: Wednesday, December 28, 2016 10:14:38





Notes:

No more than two cofferdams are allowed to be in the channel at any point in time during construction. Maximum size of cofferdams is limited to 22^{\prime} x 56^{\prime} in plan to conform with environmental permit.

Bridge plans for the original portion of the existing bridge have not been located. The original substructure is assumed to be supported by footings, based on details provided in plans for the widened portions of the existing bridge. Whether the footings are spread footings or supported on piles is unknown. Also, exact dimensions for the footings are unknown. Therefore, the footings shown in the Foundation Layout are representative and do not necessarily show all potential conflicts between the existing foundations and the new foundations. While best effort has been made to locate potential conflicts between the existing foundations and the new foundations, other conflicts may occur that are not indicated in the Foundation Layout.

Completely remove portions of the existing foundations that interfere with the installation of the new steel pipe piles. Remove all other portions of existing foundations including existing piling from previous bridge(s) according to Section 202.4.2 of the Standard Specifications or as directed by the RCE. Include all costs for this work in the lump sum price bid for "Removal and Disposal of Existing Bridge".

#Indicates HP Pile Number.

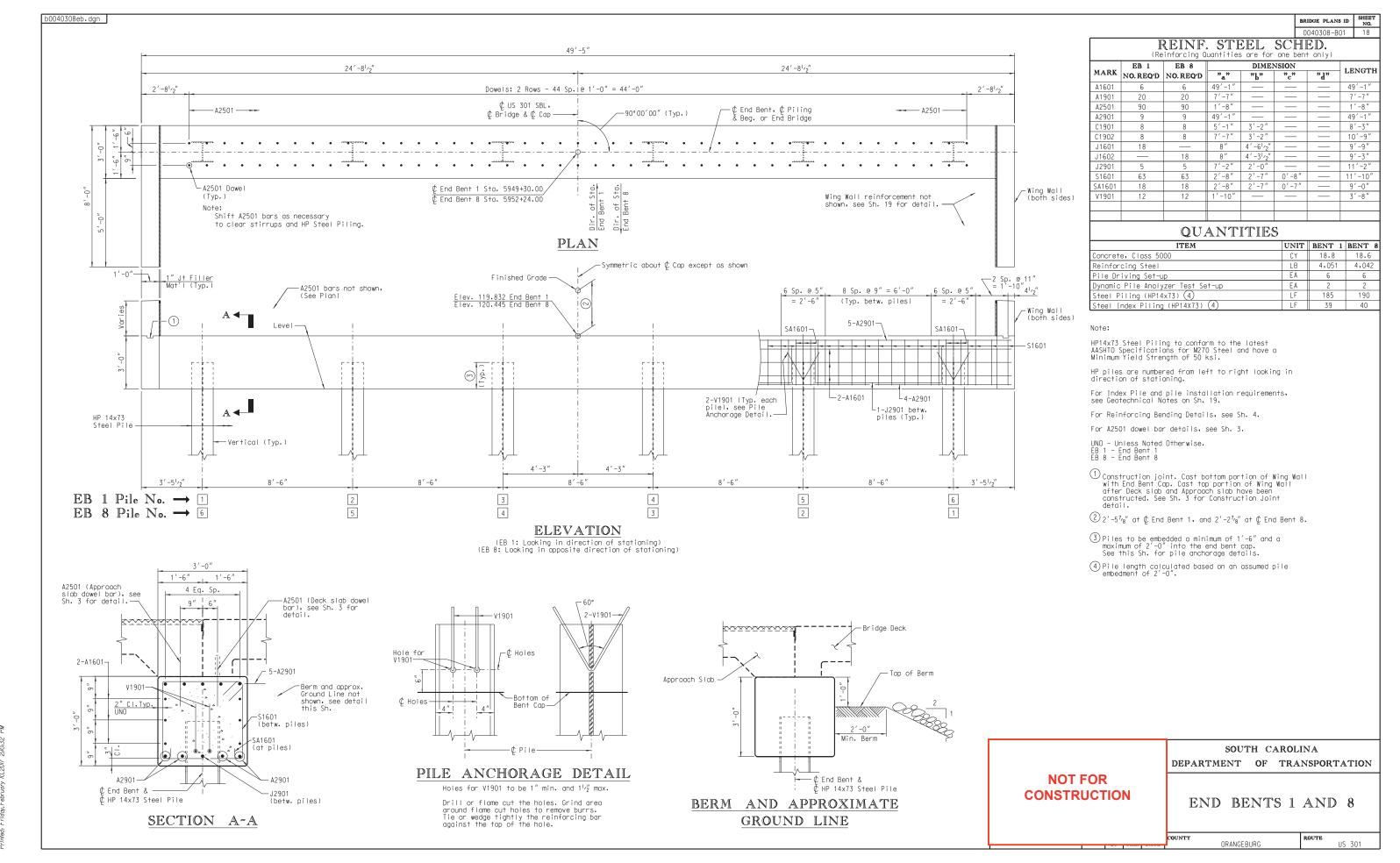
Indicates Steel Pipe Pile Number.

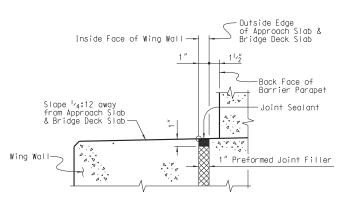
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FOUNDATION LAYOUT

COUNTY ORANGEBURG ROUTE US 301





SECTION SHOWING TOP OF WING WALL

Note: UNO - Unless Noted Otherwise EB 1 - End Bent 1 EB 8 - End Bent 8

- Construction joint. Cast bottom portion of Wing Wall with End Bent Cap. Cast top portion of Wing Wall after Deck slab and Approach slab have been constructed. See Sh. 4 for Construction Joint detail.
- \bigodot Level in longitudinal direction. Slope in transverse direction, see "Section Showing Top of Wing Wall" for detail.
- 3 EB 1: 1'-11³/₄" @ Outside Face EB 8: 1'-8³/₄" @ Outside Face
- 4 End Bent 1: 2 Sp. @ 8" = 1'-4". End Bent 8: 2 Sp. @ $6^{1}/_{2}$ " = 1'-1".
- (5) Space C1901 with A1901 (Inside Face) in bottom portion of Wing Walls (below construction joint).

WING WALL PLAN

Bent Cap reinforcement not shown

Outside Face \(\(\(\)_{3-A1901} \)

90°00′00″ (Typ.)

7-A1901 \ Inside Face

(5)_{4-C1901-}

-4-C1902

-Bot, of Bent Cap & Wing Wall, level (Typ.)

1" Preformed Joint
Filler not shown, see
"Section Showing Top of
Wing Wall" for detail.

A1901 (each face)

Elev. 116.832 End Bent 1

Elev. 116.832 End Bent 1

Elev. 117.445 End Bent 8

SECTION A-A

b0040308eb.dan

WING WALL ELEVATION

GEOTECHNICAL NOTES

PILE BEARING END BENTS 1 and 8				
Factored Axial Compression Load	105 Tons			
Geotechnical Resistance Factor	0.65			
Nominal Resistance	162 Tons			
Estimated loss of Resistance due to Scour	0 Tons			
Estimated loss of Resistance due to Downdrag	0 Tons			
Required Driving Resistance	162 Tons			

Method of controlling installation of piles and verifying their capacity: Dynamic Testing with PDA and CAPWAP analysis

GOVERNING CONDITIONS					
Loading Type	Loading Direction				
Static	Axial (Compression)				

The following estimated parameters were used for performing a driveability analysis:

DRIVEABILITY PARAMETERS					
Skin Quake (QS)	0.10 in	% Skin Friction	54%		
Toe Quake (QT)	0.10 in	Distribution Shape No.	0.00		
Skin Damping (SD)	0.05 s/ft	Pile Penetration	100%		
Toe Damping (TD)	0.15 s/ft	Bearing Graph	Proportional		

Note: GRLWEAP (2010-6) was used to perform the wave equation analysis.

A pile hammer having a rated energy between 29 kip-feet and 65 kip-feet should be suitable for driven pile installation. However, the Contractor is responsible for selecting a hammer, based on a wave equation analysis that accurately reflects the Contractor's proposed pile driving system, which will properly install the piling.

The estimated pile tip elevation to achieve axial capacity (static) for the HP 14x73 steel H-pile for End Bents 1 and 8 is 79 feet-msl. The required minimum tip elevation to achieve critical depth (lateral stability) for the HP 14x73 steel H-pile is 90 feet-msl for End Bents 1 and 8. Piles must be installed as shown on plans.

Pile Driving Analyzer (PDA) testing shall be performed on the first production pile driven at End Bent 1 and End Bent 8. These piles shall include an additional two feet of HP14x73 steel H-pile length in order to accommodate the initial PDA testing. If a CAPWAP analysis determines that capacity has not been achieved, a restrike of one of the production piles may be required. The restrike shall be performed on the production pile exhibiting the lowest blows per foot. PDA testing shall also be performed on the restrike. The time between initial driving and restrike will be determined by the Engineer, but should be between a minimum of 3 days and a maximum of 7 days. Within seven days of completion of the PDA testing (on initial drive and/or restrike, if required), the results will be evaluated by the RPG3 GDS. Construction of the bent caps shall not proceed until the end bent piles have been accepted by the RPG3 GDS.

Reference the 2007 SCDOT Standard Specifications for Driven Pile Foundation (Section 711). Notes included in these plans are in addition to the requirements of the Standard Specifications.

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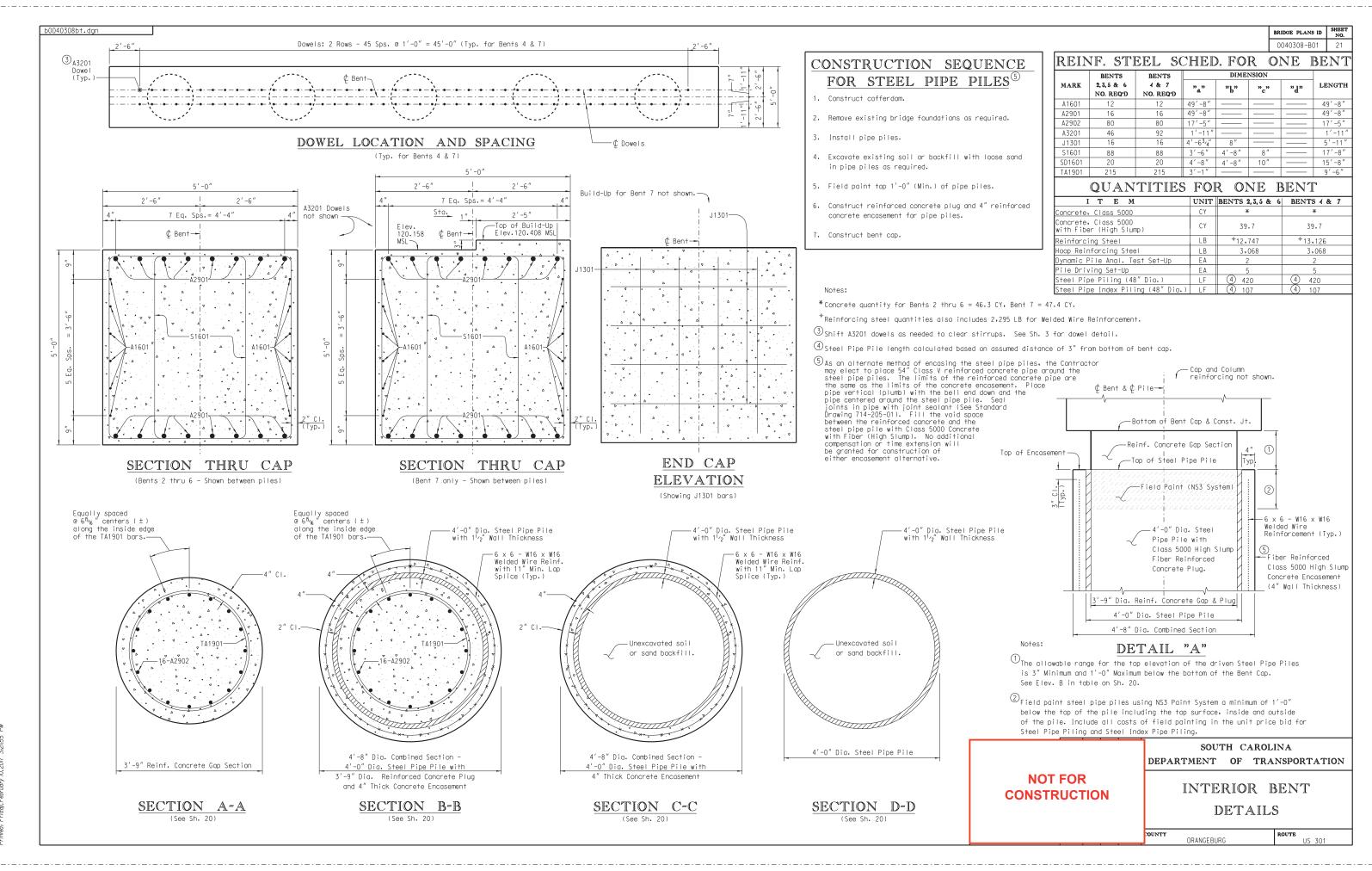
SOUTH CAROLINA
DEPARTMENT OF TRANSPORTATION

END BENT DETAILS

COUNTY

ROUTE

inted: Friday.February 10,2017 2;16;59 PI



48-inch PIPE PILE BEARING INTI	ERIOR BENTS	
Factored Axial Compression Load (Tons)	186	
Geotechnical Resistance Factor	0.65	
Required Nominal Resistance (Tons)	286	
Estimated Pile Tip Penetration (feet)	98	
Estimated Pile Tip Elevation (feet-msl)	10	
Unplugged Required Pile Driving Resistance (Tons)	1369	
Plugged Required Pile Driving Resistance (Tons)	2801	

Method of controlling installation of piles and verifying their capacity: Capacity will be verified by pile driving analyzer and CAPWAP analysis of index piles(s). A Pile Installation Chart developed from the analysis will be used to verify the capacity of production piles.

GOVERNIN	G CONDITIONS
Loading Type	Loading Direction
Static	Axial (Compression)

The following estimated parameters were used for performing a driveability analysis:

DRIVEABILITY PARAMETERS - UNPLUGGED CONDITIONS									
0.10 in	% Skin Friction	92%							
0.10 in	Distribution Shape No.	Variable							
0.05 s/ft	Pile Penetration %	89%							
0.15 s/ft	Bearing Graph	Proportional							
	0.10 in 0.10 in 0.05 s/ft	0.10 in % Skin Friction 0.10 in Distribution Shape No. 0.05 s/ft Pile Penetration %							

DRIVEABILITY PARAMETERS - PLUGGED CONDITIONS										
Skin Quake (QS)	0.10 in	% Skin Friction	66%							
Toe Quake (QT)	0.40 in	Distribution Shape No.	Variable							
Skin Damping (SD)	0.05 s/ft	Pile Penetration %	89%							
Toe Damping (TD)	0.15 s/ft	Bearing Graph	Proportional							
Note: GKLWEAP (2010-6) was u	ed to perform the wave o	quation analysis.								

Cofferdam Plan Notes

Contractor is responsible for cofferdam design. For all soils, buoyant unit weights shall be used in computations for soils below the water level. The designer shall consider all unbalanced water forces. The designer is responsible for determining a design water level. The designer shall use the following soil strength parameters for determining earth pressure coefficients.

CONT. DADANGTEDS FOR COFFERDAM DESIGN

Depth (ft)	IB2 (B-2)								
Deptn (It)	c (psf)	•	7 m (pcf)	K.	K.	K,			
0-5	-	31	115	0.485	0.320	3.124			
5-9	-	36	120	0.412	0.260	3.852			
9-11	-	36	115	0.412	0.260	3.852			
11-12		36	110	0.412	0.260	3.852			
12-19	1700	15	115	0.741	0.589	1.698			
19-74	-	36	115	0.412	0.260	3.852			
74+	-	36	120	0.412	0.260	3.852			

Depth (ft)	IB3 (B-3)								
	c (psf)	•	7 (pcf)	K.	K.	K _e			
0-5	-	31	120	0.485	0.320	3.124			
5-9	-	36	120	0.412	0.260	3.852			
'9-20	1700	15	110	0.741	0.589	1.698			
20-59	-	36	115	0.412	0.260	3.852			
59-78	-	24	120	0.593	0.422	2.371			
78+		36	120	0.412	0.260	3.852			

	IB3 (B-3A)								
Depth (ft)	c (psf)	•	y (pcf)	K.	K.	K,			
0-4	400	0	110	1.000	1.000	1.000			
4-13	-	32	120	0.470	0.307	3.255			
13-18	1700	0	110	1.000	1.000	1.000			
18-23	1780	15	115	0.741	0.589	1.698			
23-47	-	36	110	0.412	0.260	3.852			
47-59	2218	0	110	1.000	1.000	1.000			
59-62	-	26	110	0.562	0.390	2.561			
62-68	300	3	110	0.948	0.901	1.110			
68-70	-	26	115	0.562	0.390	2.561			
70-74	300	0	115	1.000	1.000	1.000			
74+	-	36	120	0.412	0.260	3.852			

A double-acting hydraulic pile driving hammer with monitoring and recording equipment capable of measuring continuously the hammer energy and rate of impact having a maximum rated energy between 66 kip-feet and 146 kip-feet should be suitable for driven pile installation under unplugged conditions. Larger hammers having a maximum rated energy between 292 kip-feet and 658 kip-feet may be suitable under plugged conditions; but, may require limiting the energy delivered. The Contractor is responsible for selecting a hammer(s), based on a wave equation analysis that accurately reflects the Contractor's proposed pile driving system, which will properly install the

The estimated pile tip elevation for the 48-inch steel pipe piles at Interior Bents 2 through 7 is 10 feet-msl in order to achieve penetration 20 feet beyond a potentially weak soil zone below the Santee Limestone Formation. For very hard or stiff soils (i.e., Santee Limestone Formation) the inside of the pipe pile may need to be augered out in order to drive the pile. No pre-augering will be allowed. The inside of the pipe pile should not be augered out deeper than the bottom of the Santee Limestone Formation which varies in elevation from 51 to 24 feet-msl based on the boring logs. The Contractor is responsible for verifying the bottom of the Santee Limestone formation by referring to the test-hole logs and the Table of Approximate Formation Elevations.

Approximate Formation Elevations

The state of the s										
Bent No.	IB-2	IB-3	IB-4	IB-5	IB-6	IB-7				
Offset direction	(L/R)	(L/R)	(L/R)	(L/R)	(L/R)	(L/R)				
Top of SLF Elevation	Unk/91	92/99	Unk/98	96/99	97/93	100/100				
Bottom of SLF Elevation & Top of WHF	Unk/36	51/50	Unk/24	42/32	31/Unk	Unk/38				
Bottom of WHF & Top of CF	Unk/14	7/9	Unk/6	10/6	Unk/7	Unk/14				
Pile Tip Elevation	10	10	10	10	10	10				

The elevations presented in this table are approximate. Actual field conditions may vary SLF = Santee Limestone Formation, WHF = Warley Hill Formation, CF = Congaree Formation

The final pipe pile tip elevation must not be shallower than 20 feet below the augered depth if no weak soil zone is encountered. If a weak soil zone (i.e., Warley Hill Formation) is encountered the final pipe pile tip elevation must not be shallower than 20 feet below the weak soil zone.

the material inside the pipe pile as the elevation of the bottom of the concrete plug as shown on the plans as Elevation C. If top elevation of material inside pipe pile is lower than the plans Elevation C, backfill with loose sand classified as A-1-a to the plans Elevation C. If top elevation of material inside pipe pile is higher than the plans Elevation C, remove material to the plans Elevation C. This soil shall be removed in order to construct the composite section at the top of the pile for connection to the pile

Perform Pile Driving Analyzer (PDA) on the first production pile driven at the Interior Bents 2 through Interior Bents 7. These piles shall include an additional two feet of 48-CAPWAP analysis determines that capacity has not been achieved, restrike one of the production piles. Perform the restrike on the production pile exhibiting the lowest blows per foot. On initial drive, piles shall be stopped at the highest allowable finished grade on the plans to accommodate a restrike while still remaining within an allowable plan finished grade elevation. Perform PDA testing during the restrike. Contact the Bridge Construction Office to determine the time between initial driving and restrike. Within seven days of completion of the PDA testing (on initial drive and/or restrike, if required), the results will be evaluated by the RPG3 GDS. Construction of the bent caps shall not proceed until the interior bent piles have been accepted by the RPG3 GDS. Payment for the restrike will be as indicated in the Standard Specifications

Reference the 2007 SCDOT Standard Specifications for Driven Pile Foundation (Section 711). Notes included in these plans are in addition to the requirements of the Standard Specifications.

Once the pipe pile is driven to the final bearing stratum, establish the final elevation of

See Sh. 20 --Top of Pile Combined Section -Dia. Steel Pipe Pile with 4" thick Concrete Encasement Cofferdam Wall - To be removed (Typ. -Existing Ground Line Class A Rip-Rap (1'-4" Layer) 5'-0" Min — Geotextile Class 1 Type B filter Encasement embedment, into this, layer. - Flowable Fill

COFFERDAM BACKFILL DETAIL (Bents 2 thru 7)

Reinforced Concrete Plug not shown.

After Piles are driven. Reinforced Concrete Plug and Encasement are installed and prior to removal of the Cofferdam. backfill with the following materials in the following sequence:

- At the bottom of the Cofferdam begin with backfilling with flowable fill to approximately 1'-4'' below the existing groundline surrounding the Cofferdam.
- 2. Place Geotextile Class 1 Type B filter over entire cured layer of flowable fill.
- 3. Place an approximate 1'-4" layer of Class A Rip-Rap over the Geotextile Class 1 Type B filter to the same elevation of the ground line surrounding the cofferdam.

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DEPARTMENT OF TRANSPORTATION INTERIOR BENT GEOTECHNICAL & COFFERDAM PLAN NOTES

SOUTH CAROLINA

Bottom of Cofferdam excavation (Varies)

ROUTE

Depth (ft)		IB4 (B-4)									
	c (psf)	•	y as (pcf)	K.	K.	K,					
0-10	-	32	120	0.470	0.307	3.255					
10-18	-	36	110	0.412	0.260	3.852					
18-84	-	36	115	0.412	0.260	3.852					
84+	-	36	120	0.412	0.260	3.852					

D41 (60	IB5 (B-5)								
Depth (ft)	c (psf)	•	y (pcf)	K.	K.	K,			
0-3	-	30	115	0.500	0.333	3.000			
3-6	-	38	120	0.384	0.238	4.204			
6-8		30	110	0.500	0.333	3.000			
8-10	-1	36	115	0.412	0.260	3.852			
10-38	-	36	115	0.412	0.260	3.852			
38-48	2125	15	110	0.741	0.589	1.698			
48-58		30	110	0.500	0.333	3.000			
58-63	8	36	115	0.412	0.260	3.852			
63-72	-	24	120	0.593	0.422	2.371			
72+		36	120	0.412	0.260	3.852			

Depth (ft)	IB5 (B-5A)									
	c (psf)		y (pcf)	K.	K.	K,				
0-6	-	35	115	0.426	0.271	3.690				
6-9	-	32	120	0.470	0.307	3.255				
9-21		36	115	0.412	0.260	3.852				
21-76	-	30	110	0.500	0.333	3.000				
76-101	-	36	115	0.412	0.260	3.852				
101-	4000	0	110	1.000	1.000	1.000				

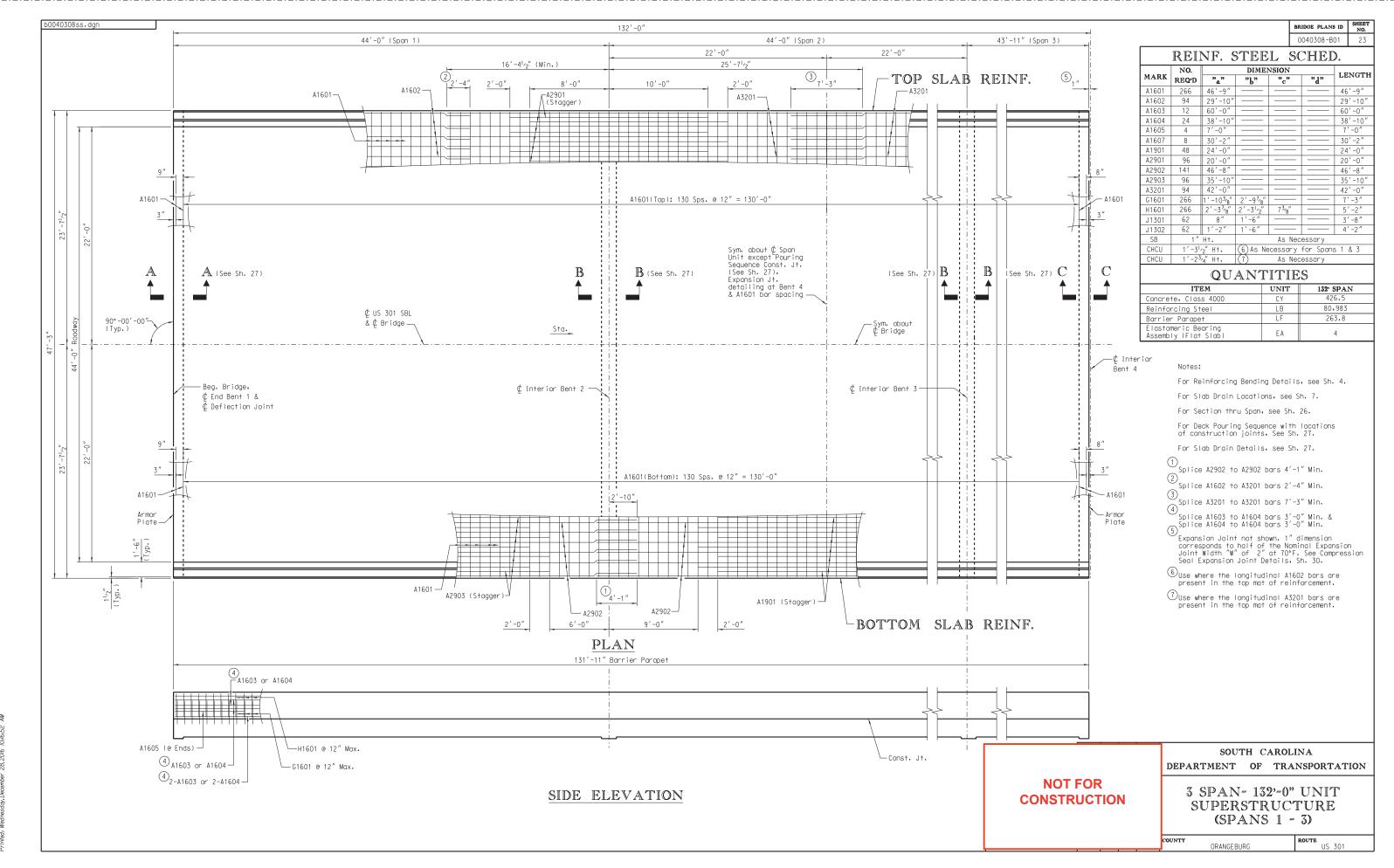
D 11 (8)	IB6 (B-6)								
Depth (ft)	c (psf)	osf) Y sat (po	y as (pcf)	K.	к.	K,			
0-3	~	34	115	0.441	0.283	3.537			
3-9		32	120	0.470	0.307	3.255			
9-13	-	30	120	0.500	0.333	3.000			
13+	-	36	115	0.412	0.260	3.852			

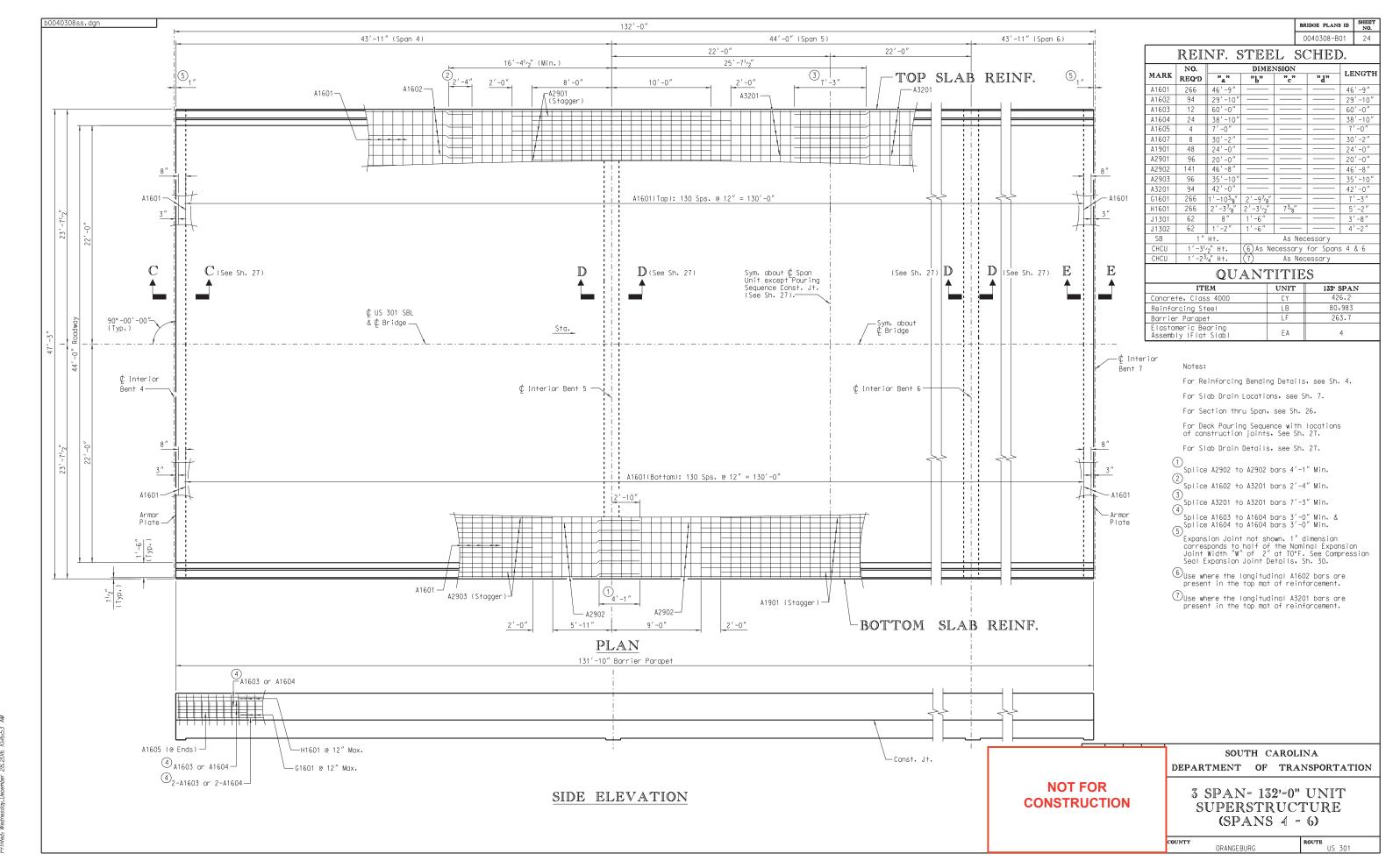
Depth (ft)			IB6	(B-6A)		
	c (psf)	•	y (pcf)	K.	K.	K _p
0-1	-	20	110	0.658	0.490	2.040
1-5	-	32	120	0.470	0.307	3.255
5-10	-	36	120	0.412	0.260	3.852
10-25	-	36	115	0.412	0.260	3.852
25-54	×	30	110	0.500	0.333	3.000
54-76	2440	15	110	0.741	0.589	1.698
76-79	-	36	115	0.412	0.260	3.852
79-	-	36	120	0.412	0.260	3.852

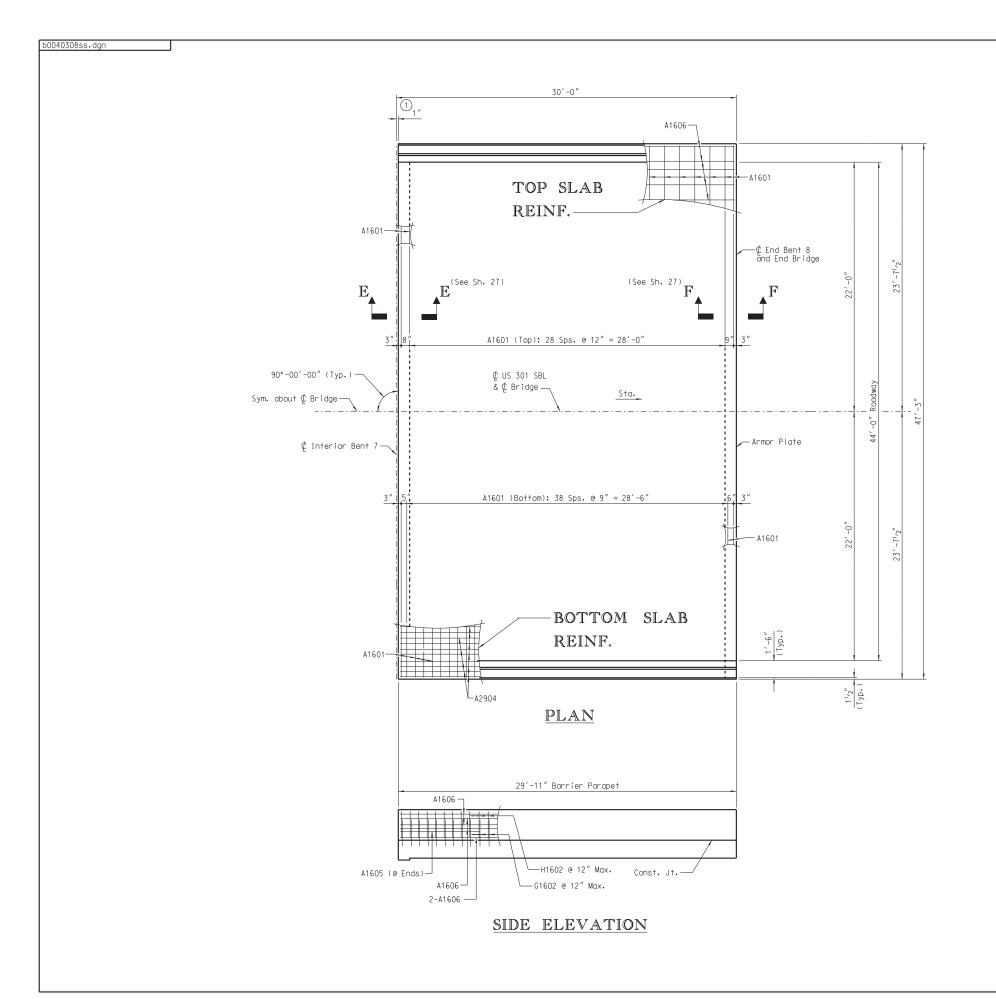
D (1 //0)	IB7 (B-7)					
Depth (ft)	c (psf)	•	y m (pcf)	K.	K.	K,
0-3	-	30	120	0.500	0.333	3.000
3-5	-	32	120	0.470	0.307	3.255
5-10	-	36	110	0.412	0.260	3.852
10+		36	115	0.412	0.260	3.852

D 4 (8)	IB7 (B-7A)					
Depth (ft)	c (psf)	•	y (pcf)	K.	K.	K,
0-3	-	24	110	0.593	0.422	2.371
3-7		29	120	0.515	0.347	2.882
7-21	-	36	115	0.412	0.260	3.852
21-47	-	30	110	0.500	0.333	3.000
47-61	-	34	110	0.441	0.283	3.537
61-69	2320	15	110	0.741	0.589	1.698
69-76		30	115	0.500	0.333	3.000
76		36	115	0.412	0.260	3.852

0040308-B01







 BRIDGE PLANS ID
 SHEET NO.

 0040308-B01
 25

| NO. | NO.

QUANTITIES

As Necessary

ITEM	UNIT	30' END SPAN
Concrete, Class 4000	CY	84.2
Reinforcing Steel	LB	15.964
Barrier Parapet	LF	59.8
Elastomeric Bearing Assembly (Flat Slab)	EA	2

Notes:

CHCU 121/2" Ht.

For Reinforcing Bending Details, see Sh. 4.

For Slab Drain Locations, see Sh. 7.

For Section thru Span, see Sh. 26.

For Deck Pouring Sequence, See Sh. 27.

For Slab Drain Details, see Sh. 27.

Expansion Joint not shown. 1" dimension corresponds to half of the Nominal Expansion Joint Width "W" of 2" at 70°F. See Compression Seal Expansion Joint Details, Sh. 30.

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SOUTH CAROLINA
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30'-0" END SPAN SUPERSTRUCTURE (SPAN 7)

ORANGEBURG ROUTE

ORANGEBURG US 301

-Sym₊ about¢Bridge

- A1602 or A3201

¢ US 301 SBL

& C Bridge——

Top - 42 Sps. @ 6" = 21'-0" (Alternate A1602 or A3201 and A2901 bars)

BRIDGE PLANS ID SHEET NO.

0040308-B01

A1603 or A1604 (Typ.)

10" Rad. -

0040308ss.dgn

Level (Typ.)—

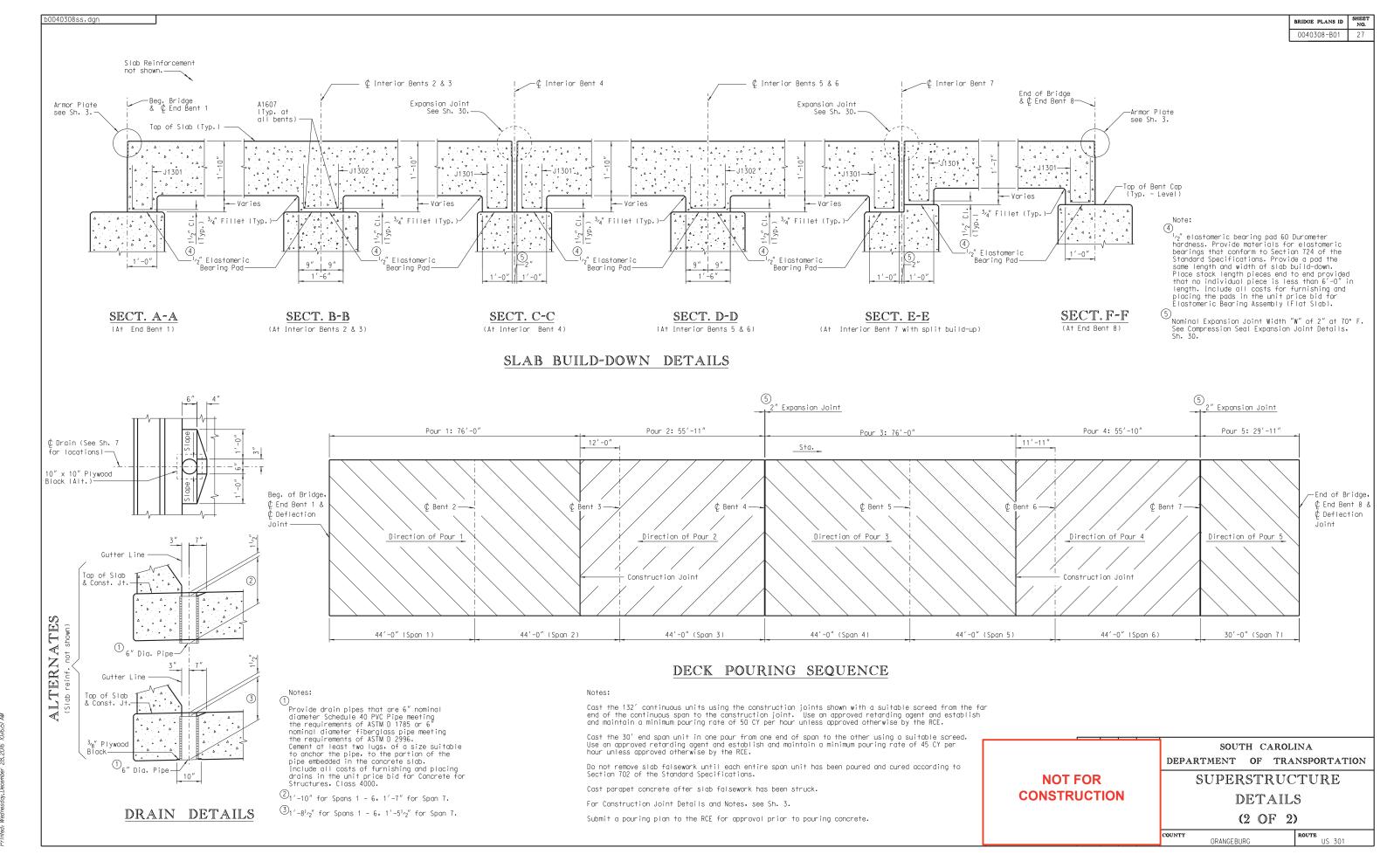
11/2" 1'-6"

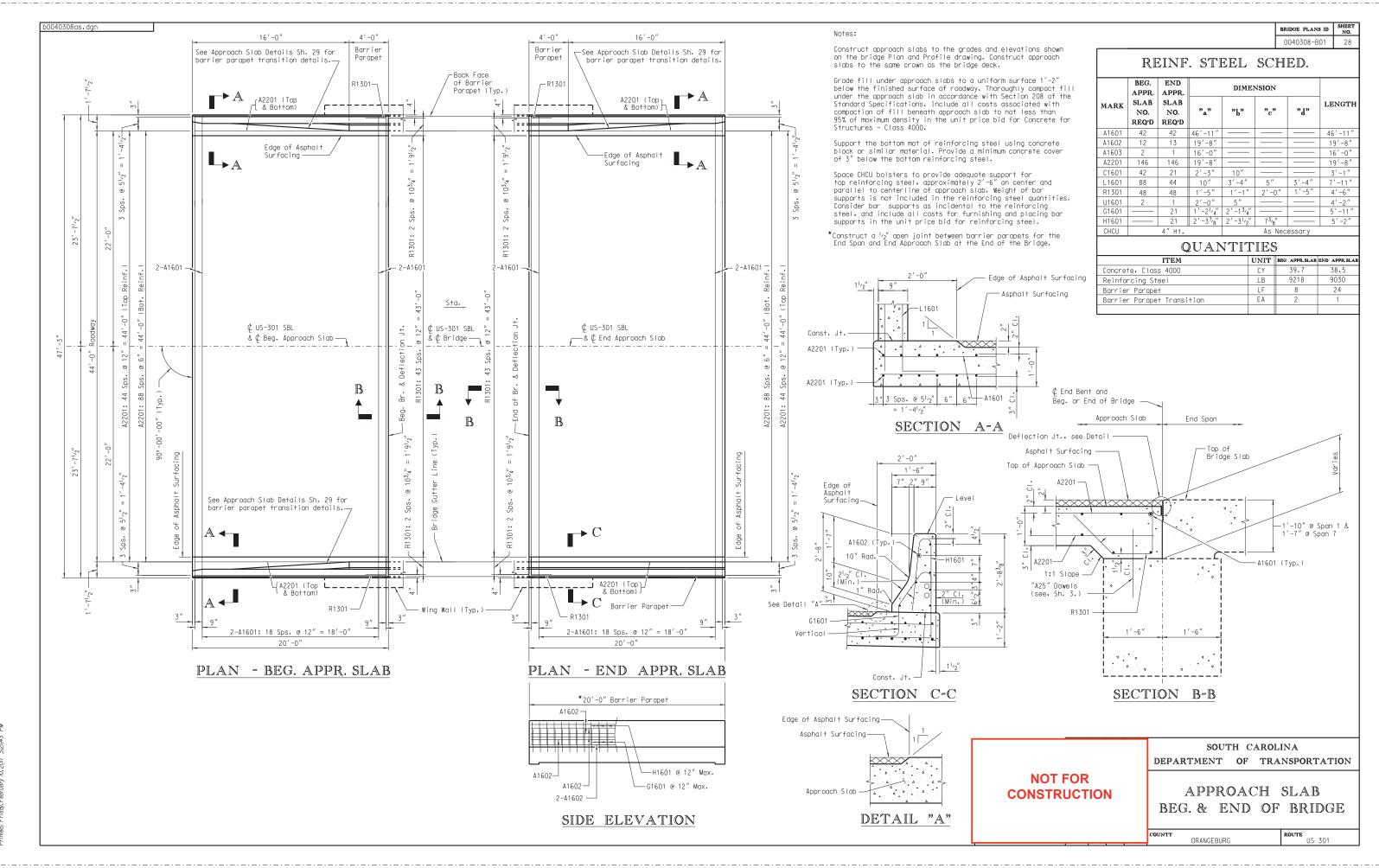
23'-71/2"

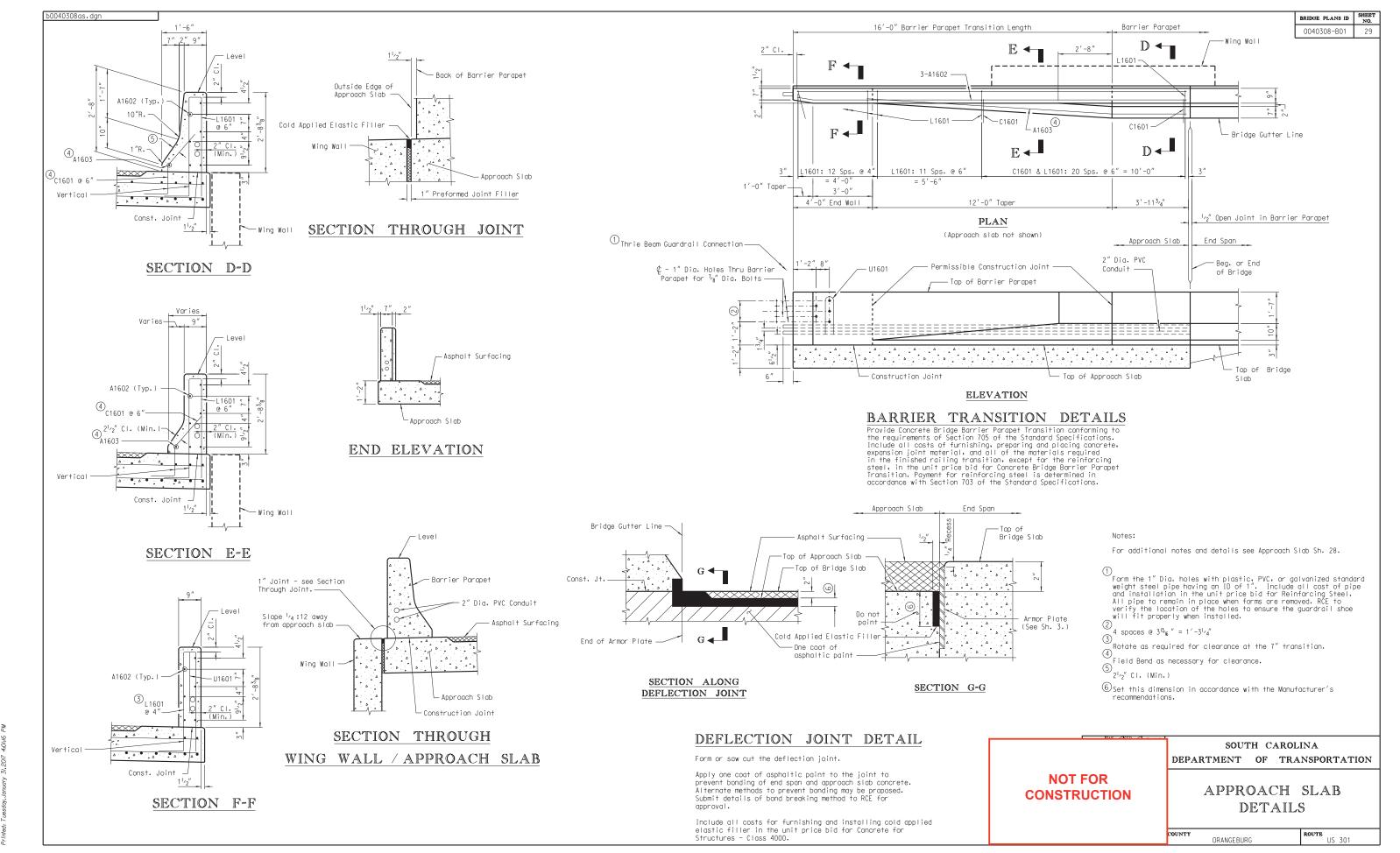
22'-0"

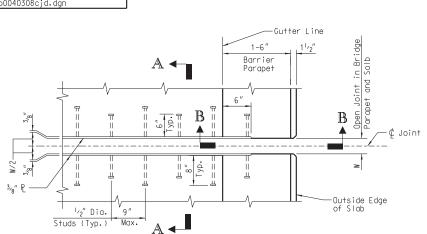
(See Sh. 27) \mathbb{A} , \mathbb{B} , \mathbb{C} , \mathbb{D} , \mathbb{E}

J1301 or J1302: 15 Sps. @ 12'' = 15'-0''



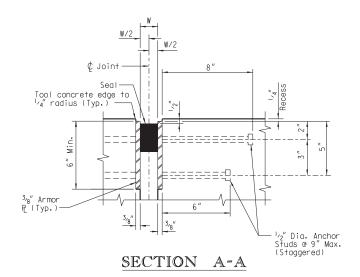






PART PLAN - EXPANSION JOINT

(Seal Not Shown)



3/4" Recess

SECTION B-B

Construction

See Detail for Seal Turns/Splices

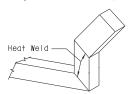
Top of Slab

Seal Installation:

Have the manufacturer's representative present for the first installation to insure proper installation. Follow the manufacturer's installation procedures and the instructions below.

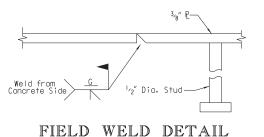
Begin seal installation at the low end of the joint, Apply mixed epoxy to Begin seal installation at the low end of the joint. Apply mixed epoxy to both sides of the seal and joint. Ensure epoxy completely fills the grooves in the sides of the seal. With gloved hands, compress the seal and install seal into the joint recessing the seal "4" below the top of the steel plate. If assistance is needed in installing the seal, use a blunt probe to push down on the seal. Do not push the seal at any angle that will stretch the seal material. Once seal installation has begun on a joint, do not stop until the installation is completed. Clean the excess epoxy from the surface of the seal material quickly and the problems in accordance with the seal. of the seal material quickly and thoroughly in accordance with the seal manufacturer's recommendations. Do not use solvents to clean or remove excess epoxy. Excess epoxy remaining on the joint seal may be cause for rejection of the joint.

Provide a watertight joint and seal. The joint will not be tested, but the RCE will observe the joint condition and performance until final inspection.



DETAIL FOR SEAL TURNS/SPLICES

- 1) Preheat the Teflon heating iron to 350° for approximately 30 minutes before welding the seal.
- 2) Using a sharp instrument such as a hacksaw, cut the seal to form the shape shown in Section B-B. This shape not necessary for welding seal at other approved splice locations.
- 3) Place the ends of seal to be welded against the Teflon heating iron at 350°F. Hold for a minimum of 10 seconds but no more than 20 seconds, depending on the ambient temperature. Then, quickly place these ends together tightly and hold for 20 seconds. Do not check the welded seal until the material has completely cooled.
- 4) If the edges do not seal completely, use a thin blade, such as a hacksaw blade to transfer heat into the edge to be sealed. Hold the heated blade between the edges of the material approximately 5 seconds, then remove and press the edge together quickly and hold for 10 to 20 seconds. Keep the blade on the heating iron under the Teflon cover between each use.



Provide adhesive that complies with the requirements in the Table below.

TEST	TEST METHOD	REQUIREMENT
Tensile Strength	ASTM D 638	3500 psi Min.
Compressive Strength	ASTM D 695	7000 psi Min.
Shore D Hardness	ASTM D 2240	75 Min.
Water Absorption	ASTM D 570	0.25% by Weight
Bond Strength	ASTM C 882	430 psi Min.

Provide seal that complies with the requirements in the Table below.

TEST	TEST METHOD	REQUIREMENT
Elongation at Break	ASTM D 3575, Suffix T	≥ 180%
Tensile Strength	ASTM D 3575, Suffix T	≥ 110 psi
Tear Resistance	ASTM D 3575, Suffix G	≥14 pli
Density	ASTM D 3575, Suffix W - Method A	2.0 pcf to 3.4 pcf
Water Absorption	ASTM D 3575, Suffix L	< 0.03 psf
Compression Set	ASTM D 3575, Suffix B, 2 hour recovery	< 15%

Notes:

0040308-B0 For each joint location as shown in the Joint Table below, provide seal For each joint location as shown in the Joint Table below, provide seal having a normal uncompressed width as shown in the Joint Table. Set the nominal joint width "W" to the value shown in the Joint Table at 70° F. Use the actual air temperature, measured in the shade and averaged over the preceding 24 hour period, as the setting temperature. At the time of construction, decrease the joint opening by Dim "A" for each 10°F that the setting temperature is above 70°F or increase the joint opening by Dim "A" for each 10°F that the setting temperature is below 70°F.

JOINT TABLE				
	NOMINAL		Seal	
	JOINT WIDTH		Uncompressed	
LOCATION	″W″ @ 70° F.	DIM "A"	Width	
Interior Bent 4	2"	1/8"	21/2"	
Interior Bent 7	2"	ν ₁₆ "	21/2"	

Ensure three copies of certifications are signed by an authorized agent of the manufacturer or supplier and submitted to the RCE prior to the installation of the seal. The required certifications are a copy of the manufacturer's test reports, or a statement by the supplier accompanied by the test results, certifying that the materials have been sampled, tested and inspected. Failure to provide the required certifications for seals and lubricant/adhesive is grounds for rejection of the materials.

Mark all seals with die markings that indicate the lot number and manufacturer. Mark each container of lubricant/adhesive with the manufacturer, lot number, and shelf life expiration date.

Provide preformed seals that are compatible with steel and concrete and resistant to abrasion, oxidation, oils, gasoline, salt, and other materials that may be spilled on or applied to the surface. Provide seal material that is resistant to weathering and ultra-violet rays. Provide a seal having a working movement range of 30% tension and 60% compression. Manufacture the seal from a low-density closed cell-cross-linked ethylene vinyl acetate polyethylene copolymer nitrogen blown material.

Manufacture seals with grooves along the bond surface running the length of the joint. The grooves shall be $^{1}/_{8}''$ wide by $^{1}/_{8}''$ deep and spaced between $^{1}/_{4}''$ and $^{1}/_{2}''$ apart. Provide seals with a minimum depth at least 70% of the uncompressed width and meeting the manufacturer's recommendations. Design the seal so that, when compressed, the center portion of the top does not extend upward above the original height of the seal by more than 1/4".

Shop mark the seal to indicate the top side of the seal in such a way as

Install seals in accordance with the manufacturer's instructions unless stipulated otherwise in these plans or the Special Provisions.

Provide a watertight seal along the entire length including the ends of the seal.

Provide a two component, 100% solid, modified epoxy adhesive meeting the requirements of ASTM C 881, Type I, Grade 2, Class B & C and in accordance with testing requirements shown on this sheet.

Provide adhesive that is workable to $40^{\circ}F$. For installation temperatures below $40^{\circ}F$ or for application on moist, hard to dry concrete surfaces, provide adhesive as specified by the manufacturer of the joint material.

Clean the armored joint opening in accordance with the manufacturer's recommendations. Bond the seal to the cleaned surface on the same day the cleaning is done.

Provide steel armor plates that conform to the requirements of the latest AASHTO M 270, Grade 50W (ASTM A 709, Gr. 50W) and are of weldable quality.

Provide $^3\eta_0''$ plates that conform to the crown of the finished roadway and have smooth edges. Fabricate the $^3\eta_0''$ plates in reasonable lengths and connect them at the job site using partial penetration groove welds. Grind welds at the exposed surfaces of plates flush. Perform welding of splices prior to bonding seals. If necessary to bolt the $^3\eta_0''$ plates to the forms, provide $^3\eta_0''$ Dia. holes at approximately 2' on center in the lower portion of the particles.

Field bend top slab reinforcing as required to clear anchor studs.

For payment purposes, measure along the centerline of the joint from the edge of slab to the edge of slab. Include all costs associated with furnishing labor, materials, fabrication, and installation of armor plates, cover plates, and seals complete and in place in the unit price bid per linear foot of Compression Seal Joint.

OUNTY

NOT FOR CONSTRUCTION

SOUTH CAROLINA DEPARTMENT OF TRANSPORTATION

> COMPRESSION SEAL EXPANSION JOINT DETAILS

ORANGEBURG

ROUTE US 301